PB83-175018

# Analysis of Long-Term No Emission Data from Pulverized Coal-Fired Utility Boilers Volume II. Appendices

KVB, Inc.
Irvine, CA

Prepared for

Industrial Environmental Research Lab.
Research Triangle Park, NC

Feb 83

U.S. Department of Commerce
National Technical Information Service
NTIS

PB83-175018

EPA-600/7-83-012b
February 1983

# ANALYSIS OF LONG-TERM NO EMISSION DATA FROM PULVERIZED COAL-FIRED UTILITY BOILERS

## VOLUME II. APPENDICES

by

S. S. Cherry

KVB, INC.
18006 Skypark Boulevard
Irvine, California 92714

EPA Contract No. 68-02-3175, Work Assignment #7

EPA Project Officer: Robert E. Hall

Industrial Environmental Research Laboratory
Office of Environmental Engineering and Technology
Research Triangle Park, NC 27711

Prepared for:

U.S. ENVIRONMENTAL PROTECTION AGENCY
Office of Research and Development
Washington, D.C. 20460

REPRODUCED BY
NATIONAL TECHNICAL
INFORMATION SERVICE
U.S. DEPARTMENT OF COMMERCE
SPRINGFIELD, VA. 22161

| TECHNICAL REPORT DATA (Please read Instructions on the reverse before completing) | |
|---|---|
| 1. REPORT NO. EPA-600/7-83-012b | 2. |
| 3. RECIPIENT'S ACCESSION NO. PB83 175018 | |
| 4. TITLE AND SUBTITLE Analysis of Long-term NO Emission Data from Pulverized Coal-fired Utility Boilers; Vol. II. Appendices | 5. REPORT DATE February 1983 |
| | 6. PERFORMING ORGANIZATION CODE |
| 7. AUTHOR(S) S.S. Cherry | 8. PERFORMING ORGANIZATION REPORT NO. |
| 9. PERFORMING ORGANIZATION NAME AND ADDRESS KVB, Inc. 18006 Skypark Boulevard Irvine, California 92714 | 10. PROGRAM ELEMENT NO. |
| | 11. CONTRACT/GRANT NO. 68-02-3175, Task 7 |
| 12. SPONSORING AGENCY NAME AND ADDRESS EPA, Office of Research and Development Industrial Environmental Research Laboratory Research Triangle Park, NC 27711 | 13. TYPE OF REPORT AND PERIOD COVERED Task Final; 5/81-5/82 |
| | 14. SPONSORING AGENCY CODE EPA/600/13 |
| 15. SUPPLEMENTARY NOTES IERL-RTP project officer is Robert E. Hall, Mail Drop 65, 919/541-2477. Volume I is the technical analysis. | |

16. ABSTRACT The report gives results of an analysis of long-term NO emission monitoring data from nine pulverized-coal-fired utility boilers. These data were in the form of hourly averaged NO, O2 (or CO2), and load: NO and O2/CO2 were measured with certified continuous emission analyzers. The analyses were compared to the emissions limitations in both the 1971 and 1978 New Source Performance Standards (NSPS). The comparison with the 1978 NSPS showed that seven of the nine boilers would have produced no periods of excess NO emissions on a 30-day rolling average basis. In addition, the same seven boilers would have complied with the 1978 NSPS NOx performance test requirements. Recommendations are made to more fully analyze the operation of two of these boilers to determine if their mode of operation could be adopted by other boilers. These boilers use permanently installed CO monitors to allow operation at the lowest practical excess air to achieve either low NO emissions or better fuel efficiency.

| 17. KEY WORDS AND DOCUMENT ANALYSIS | | |
|---|---|---|
| a. DESCRIPTORS | b. IDENTIFIERS/OPEN ENDED TERMS | c. COSATI Field/Group |
| Pollution<br>Nitrogen Oxide (NO)<br>Coal<br>Pulverized Fuels<br>Combustion<br>Boilers<br>Monitors<br>Analyzing | Pollution Control<br>Stationary Sources | 13B 14G<br>07B<br>21D 14B<br>21B<br>13A |
| 18. DISTRIBUTION STATEMENT Release to Public | 19. SECURITY CLASS (This Report) Unclassified | 21. NO. OF PAGES 445 |
| | 20. SECURITY CLASS (This page) Unclassified | 22. PRICE |

EPA Form 2220-1 (9-73)

NOTICE

This document has been reviewed in accordance with U.S. Environmental Protection Agency policy and approved for publication. Mention of trade names or commercial products does not constitute endorsement or recommendation for use.

CONTENTS


| | | Page |
|---|---|---|
| A. | Data Reduction Computer Program Listing | 1 |
| B. | Oklahoma Gas & Electric, Muskogee Station - Unit 4<br>Input Data - Initial Analysis | 12 |
| C. | Oklahoma Gas & Electric, Muskogee Station - Unit 4<br>Input Data - Revised Analysis | 62 |
| D. | Oklahoma Gas & Electric, Muskogee Station - Unit 5<br>Input Data - Initial Analysis | 104 |
| E. | Oklahoma Gas & Electric, Muskogee Station - Unit 5<br>Input Data - Revised Analysis | 148 |
| F. | Omaha Public Power District, Nebraska City Station - Unit 1<br>Input Data | 161 |
| G. | Iowa Power & Light, Council Bluffs Station - Unit 3<br>Input Data - Initial Analysis | 179 |
| H. | Iowa Power & Light, Council Bluffs Station - Unit 3<br>Input Data - Revised Analysis | 230 |
| I. | Pennsylvania Electric, Homer City Generating Station - Unit 3<br>Input Data | 264 |
| J. | Louisville Gas & Electric, Mill Creek Station - Unit 3<br>Input Data | 297 |
| K. | Proprietary Information - Unit A<br>Input Data | 327 |
| L. | Proprietary Information - Unit B<br>Input Data | 367 |
| M. | Public Service Company of New Mexico, San Juan Plant - Unit 1<br>Input Data | 409 |

The data reduction computer program (Appendix A) was written prior to receiving any of the utility data. As such, the column headings for example, were structured to be printed in terms of total oxides of nitrogen ($NO_x$). The monitor data subsequently received was in terms of nitric oxide (NO) only and not $NO_x$. The only exception is the 1971 NSPS performance test result which is in terms of total $NO_x$. It was decided to retain the $NO_x$ headings instead of reprogramming and rerunning all the cases.

# APPENDIX A

## DATA REDUCTION COMPUTER PROGRAM LISTING

```
*09/02/81-13:42(8,9)
C     THIS PROGRAM ACCEPTS UP TO 100 DAYS OF NOX, O2 AND LOAD. THE
C     INPUT IS PRE-EDITED TO DELETE INVALID DAYS - THOSE WITH LESS THAN
C     18 VALID HOURS. THE PROGRAM THEN CALCULATES--
C     (A)DAILY AVERAGES AND STD DEV OF NOX, O2 AND LOAD
C     (B)AVERAGE NOX AND O2 (AND STD DEV) VS. LOAD (IN 10 LOAD CELLS)
C     (C)LOAD PROBABILITY (10 CELLS)
C     (D)NOX PROBABILITY (10 CELLS)
C     (E)3-HR NOX AVERAGES FOR COMPARISON WITH 1971 NSPS
C     (F)30-DAY ROLLING AVERAGES FOR COMPARISON WITH 1978 NSPS
C     INPUT VARIABLES ARE--
C     NDAYS = NO. OF DAYS OF INPUT .LE. 100
C     ICOAL = COAL TYPE, -1 SUBBITUMINOUS, 0 BITUMINOUS
C                        +1 N+S DAKOTA, MONTANA LIGNITE
C                        +2 OTHER LIGNITE
C     PERFM = NOX MEASURED DURING PERFORMANCE TEST LB/10**6 BTU
C     IDAY(I) = SEQUENTIAL DAY NUMBER .LE. 0 MEANS INVALID DAY
C     NOX(I,J) = LB/10**6 BTU HOURLY AVERAGE
C     O2(I,J) = EXCESS OXYGEN PERCENT HOURLY AVERAGE
C     LOAD(I,J) = GROSS MEGAWATT(E) GENERATOR OUTPUT
      DIMENSION IDAY(100),NOX(100,24),O2(100,24),LOAD(100,24)
      DIMENSION DUM1(24),DUM2(24),DUM3(24),NOXMN(100),STDN(100)
      DIMENSION O2MN(100),STDO2(100),LDMN(100),STDLD(100),NN(100)
      DIMENSION VAL1(2400),VAL2(2400),VAL3(2400),BNDR(11),CNTR(10)
      DIMENSION NBIT(10),ENOX(10,2400),EO2(10,2400),AAN(10),SSN(10)
      DIMENSION ANO(10),SSO(10),PSUM(10),DALY(100),ROLAVE(100)
      REAL NOX,LOAD,NOXMN,LDMN
      CHARACTER*72 HDG
      WRITE(6,1)
    1 FORMAT(1H1)
      WRITE(6,2)
    2 FORMAT(1H0,34X,64H**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISS
     1ION MONITORING**)
C     READ AND WRITE 6 HEADING CARDS
      DO 3 I=1,6
      READ(5,4)HDG
    4 FORMAT( A72 , 8X)
      WRITE(6,5)HDG
    5 FORMAT(1H0, A72)
    3 CONTINUE
C     INITIALIZE ARRAYS
      DO 6 I=1,100
      IDAY(I)=0
      NOXMN(I)=0.
      STDN(I)=0.
      O2MN(I)=0.
      STDO2(I)=0.
      LDMN(I)=0.
      STDLD(I)=0.
      NN(I)=0
      DALY(I)=0.
      ROLAVE(I)=0.
    6 CONTINUE
      DO 7 I=1,100
      DO 8 J=1,24
      NOX(I,J)=0.
      O2(I,J)=0.
      LOAD(I,J)=0.
```

```
      8 CONTINUE                                                        820
      7 CONTINUE                                                        830
        DO 9 I=1,24                                                     840
        DUM1(I)=0.                                                      850
        DUM2(I)=0.                                                      860
        DUM3(I)=0.                                                      870
      9 CONTINUE                                                        880
        DO 10 I=1,2400                                                  890
        VAL1(I)=0.                                                      900
        VAL2(I)=0.                                                      910
        VAL3(I)=0.                                                      920
        DO 11 J=1,10                                                    930
        ENOX(J,I)=0.                                                    940
        FO2(J,I)=0.                                                     950
     11 CONTINUE                                                        960
     10 CONTINUE                                                        970
        DO 12 I=1,10                                                    980
        NRIT(I)=0                                                       990
        CNTR(I)=0.                                                     1000
        BNOR(I)=0.                                                     1010
        AAN(I)=0.                                                      1020
        SSN(I)=0.                                                      1030
        ANO(I)=0.                                                      1040
        SSO(I)=0.                                                      1050
        PSUM(I)=0.                                                     1060
     12 CONTINUE                                                       1070
        BNOR(11)=0.                                                    1080
C       READ INPUT DATA                                                1090
        READ(5,13) NDAYS, ICOAL, PERFN                                 1100
     13 FORMAT(2I6, F6.3  , 62X)                                       1110
        DO 18 I=1,NDAYS                                                1120
        READ(5,15)IDAY(I)                                              1130
     15 FORMAT(I6 , 74X)                                               1140
        IF(IDAY(I) .LE. 0) GO TO 18                                    1150
        READ(5,16) (NOX(I,J) , J=1,24)                                 1160
     16 FORMAT(12F6.3, 8X /12F6.3,8X)                                  1170
        READ(5,16) (O2(I,J), J=1,24)                                   1180
        READ(5,16) (LOAD(I,J), J=1,24)                                 1190
     18 CONTINUE                                                       1200
C       WRITE INPUT DATA                                               1210
        AVERT=629.591                                                  1220
        WRITE(6,1)                                                     1230
        WRITE(6,17)                                                    1240
     17 FORMAT(1H0,59X,10H**INPUT DATA**)                              1250
        DO 1A I=1,NDAYS                                                1260
        IF(IDAY(I).LE.0)GO TO 18                                       1270
        WRITE(6,19)IDAY(I)                                             1280
     19 FORMAT(1H0,61X,5HDAY = ,I4 / 1H0,89X,3HNOX,10X,3HNOX,8X,2HO2,  1290
     1AX,12HGROSS OUTPUT / 1H ,36X,4HHOUR,5X,12HLB/10**6 BTU,5X,       1300
     2AHMG/J,5X,7HPERCENT,10X,2HMW /1H ,36X,4H----,5X,12H------------,  1310
     35X,8H-----,5X,7H-------,5X,12H------------ )                     1320
        DO 20 J=1,24                                                   1330
        A=NOX(I,J)*AVERT                                               1340
        WRITE(6,21)J,NOX(I,J),A,O2(I,J),LOAD(I,J)                      1350
     21 FORMAT(1H ,37X,I2,8X,F6.3,8X,F5.0,6X,F4.1,11X,F4.0)            1360
     20 CONTINUE                                                       1370
     1A CONTINUE                                                       1380
C       CALCULATE DAILY MEANS AND STANDARD DEVIATIONS                  1390
        WRITE(6,22)                                                    1400
```

```
      22 FORMAT(1H1 /1H0,46X,39H**DAILY MEANS AND STANDARD DEVIATIONS**)      1200
         WRITE(6,23)                                                         1210
      23 FORMAT(1H0,10X,8HNOX MEAN,7X,8HNOX MEAN,5X,11HNOX STD DEV,6X,       1220
        111HNOX STD DEV,5X,7HO2 MEAN,5X,10HO2 STD DEV,5X,9HLOAD MEAN,       1230
        25X,12HLOAD STD DEV /1H ,8X,3HDAY,5X,12HLB/10**6 BTU,7X,8HNG/J,     1240
        37X,12HLB/10**6 BTU,8X,8HNG/J,9X,7HPERCENT,6X,7HPERCENT,10X,        1250
        82HMN,10X,2HMN /1H ,3X,8H-----,5X,12H------------,5X,8H--------,    1260
        55X,12H------------,5X,11H------------,5X,7H-------,5X,             1270
        610H----------,5X,9H---------,5X,12H------------)                   1280
         IVALID=0                                                            1290
         DO 24 I=1,NDAYS                                                     1300
         N=0                                                                 1310
C        CHECK FOR VALID DAY                                                 1320
         IF(IDAY(I).LE. 0)GO TO 24                                           1330
         IVALID=IVALID + 1                                                   1340
         DO 25 J=1,24                                                        1350
C        CHECK FOR VALID HOUR                                                1360
         IF(NOX(I,J).LE. 0.) GO TO 25                                        1370
         N=N+1                                                               1380
C        NN(I)=NO. VALID HOURS IN I-TH DAY                                   1390
         NN(I)=N                                                             1400
         DUM1(N)=NOX(I,J)                                                    1410
         DUM2(N)=O2(I,J)                                                     1420
         DUM3(N)=LOAD(I,J)                                                   1430
      25 CONTINUE                                                            1440
C        DUM1,DUM2,DUM3 CONTIGUOUS ARRAYS OF NOX,O2,LOAD                     1450
         CALL STAT(N,DUM1,A,B)
         NOXMN(I)=A
         STDN(I)=B
         CALL STAT(N,DUM2,A,B)
         O2MN(I)=A
         STDO2(I)=B
         CALL STAT(N,DUM3,A,B)
         LDMN(I)=A
         STDLD(I)=B
      24 CONTINUE                                                            1490
         DO 30 I=1,NDAYS                                                     1500
         IF(IDAY(I).LE.0)GO TO 30
         A=NOXMN(I)*AVERT                                                    1510
         B=STDN(I)*AVERT                                                     1520
         WRITE(6,26)IDAY(I),NOXMN(I),A,STDN(I),B,O2MN(I),STDO2(I),          1530
        1LDMN(I),STDLD(I)                                                    1540
      26 FORMAT(1H ,3X,I4,8X,F5.3,11X,F4.0,10X,F6.4,11X,F5.1,9X,F4.1,       1550
        19X,F5.2,10X,F4.0,11X,F5.1  )                                        1560
      30 CONTINUE                                                            1570
C        VAL1,VAL2,VAL3 ARE PACKED 1-DIMENSIONAL ARRAYS OF VALID             1580
C        NOX,O2 AND LOAD HOURLY AVERAGES                                     1590
C        NNN IS A COUNT ON NUMBER OF VALID HOURLY AVERAGES                   1600
         NNN=0                                                               1610
         DO 50 I=1,NDAYS                                                     1620
         DO 60 J=1,24                                                        1630
         IF(NOX(I,J) .LE. 0.0) GO TO 60                                      1640
         NNN=NNN+1                                                           1650
         VAL1(NNN)=NOX(I,J)                                                  1660
         VAL2(NNN)=O2(I,J)                                                   1670
         VAL3(NNN)=LOAD(I,J)                                                 1680
      60 CONTINUE                                                            1690
      50 CONTINUE                                                            1700
C        FIND LOAD MINIMUM AND MAXIMUM (A,B), THESE WILL BE USED TO SET-UP   1710
```

```
C     LOAD CELLS FOR SORTING NOX,O2 AND LOAD
      A=VAL3(1)
      B=VAL3(1)
      DO 710 I=2,NNN
      IF(VAL3(I).LT.A)A=VAL3(I)
      IF(VAL3(I).GT.B)B=VAL3(I)
  710 CONTINUE
      A=A-1.
      B=B+1.
C     DIVIDE LOAD RANGE INTO 10 CELLS
      C= (B-A)/10.
C     BNDR ARE BOUNDARIES OF LOAD CELLS
C     CNTR ARE CENTERS OF LOAD CELLS
      BNDR(1)=A
      BNDR(11)=B
      DO 80 I=2,10
      BNDR(I)=BNDR(I-1)+C
   80 CONTINUE
      CNTR(1)=A+C/2.
      CNTR(10)=B-C/2.
      DO 100 I=2,9
      CNTR(I)=CNTR(I-1)+C
  100 CONTINUE
C     NBIT(10) IS THE NUMBER OF NOX AND O2 PAIRS IN EACH LOAD CELL
C     SCAN VAL3(NNN)
      DO 110 I=1,NNN
      D=VAL3(I)
      IF((D.GE.BNDR( 1)).AND.(D.LT.BNDR( 2)))GO TO 120
      IF((D.GE.BNDR( 2)).AND.(D.LT.BNDR( 3)))GO TO 130
      IF((D.GE.BNDR( 3)).AND.(D.LT.BNDR( 4)))GO TO 140
      IF((D.GE.BNDR( 4)).AND.(D.LT.BNDR( 5)))GO TO 150
      IF((D.GE.BNDR( 5)).AND.(D.LT.BNDR( 6)))GO TO 160
      IF((D.GE.BNDR( 6)).AND.(D.LT.BNDR( 7)))GO TO 170
      IF((D.GE.BNDR( 7)).AND.(D.LT.BNDR( 8)))GO TO 180
      IF((D.GE.BNDR( 8)).AND.(D.LT.BNDR( 9)))GO TO 190
      IF((D.GE.BNDR( 9)).AND.(D.LT.BNDR(10)))GO TO 200
      IF((D.GE.BNDR(10)).AND.(D.LT.BNDR(11)))GO TO 210
C     ENOX AND EO2 ARE SORTED PAIRS OF NOX AND O2 IN EACH LOAD CELL
  120 NBIT(1)=NBIT(1)+1
      JJ=NBIT(1)
      ENOX(1,JJ) = VAL1(I)
      EO2(1,JJ) = VAL2(I)
      GO TO 110
  130 NBIT(2)=NBIT(2)+1
      JJ=NBIT(2)
      ENOX(2,JJ) = VAL1(I)
      EO2(2,JJ) = VAL2(I)
      GO TO 110
  140 NBIT(3)=NBIT(3)+1
      JJ=NBIT(3)
      ENOX(3,JJ) = VAL1(I)
      EO2(3,JJ) = VAL2(I)
      GO TO 110
  150 NBIT(4)=NBIT(4)+1
      JJ=NBIT(4)
      ENOX(4,JJ) = VAL1(I)
      EO2(4,JJ) = VAL2(I)
      GO TO 110
  160 NBIT(5)=NBIT(5)+1
```

```
      JJ=NAIT(5)                                                        .  2250
      ENOX(5,JJ)=VAL1(I)                                                .  2260
      EO2(5,JJ)=VAL2(I)
      GO TO 110                                                         .  2270
  170 NAIT(6)=NAIT(6)+1                                                 .  2280
      JJ=NAIT(6)                                                        .  2290
      ENOX(6,JJ) = VAL1(I)                                              .  2300
      EO2(6,JJ) = VAL2(I)                                               .  2310
      GO TO 110                                                         .  2320
  180 NAIT(7)=NAIT(7)+1                                                 .  2330
      JJ=NAIT(7)                                                        .  2340
      ENOX(7,JJ) = VAL1(I)                                              .  2350
      EO2(7,JJ) = VAL2(I)                                               .  2360
      GO TO 110                                                         .  2370
  190 NAIT(8)=NAIT(8)+1                                                 .  2380
      JJ=NAIT(8)                                                        .  2390
      ENOX(8,JJ) = VAL1(I)                                              .  2400
      EO2(8,JJ) = VAL2(I)                                               .  2410
      GO TO 110                                                         .  2420
  200 NAIT(9)=NAIT(9)+1                                                 .  2430
      JJ=NAIT(9)                                                        .  2440
      ENOX(9,JJ) = VAL1(I)                                              .  2450
      EO2(9,JJ) = VAL2(I)                                               .  2460
      GO TO 110                                                         .  2470
  210 NAIT(10)=NAIT(10)+1                                               .  2480
      JJ=NAIT(10)                                                       .  2490
      ENOX(10,JJ) = VAL1(I)                                             .  2500
      EO2(10,JJ) = VAL2(I)                                              .  2510
  110 CONTINUE                                                          .  2520
C     CALCULATE MEANS AND STD DEVS OF NOX AND O2 IN EACH LOAD CELL      .  2530
      DO 220 I=1,10                                                     .  2540
      K=NAIT(I)
      IF(K.LT.1)GO TO 220
      AAN(I)=0.
      SSN(I)=0.
      ANO(I)=0.
      SSO(I)=0.
      DO 225 J=1,K
      AAN(I)=AAN(I)+ENOX(I,J)
      ANO(I)=ANO(I)+EO2(I,J)
  225 CONTINUE
      AAN(I)=AAN(I)/FLOAT(K)
      ANO(I)=ANO(I)/FLOAT(K)
      DO 230 J=1,K
      IF(K.LT.2)GO TO 220
      SSN(I)=SSN(I)+(ENOX(I,J)-AAN(I))**2
      SSO(I)=SSO(I)+(EO2(I,J)-ANO(I))**2
  230 CONTINUE
      SSN(I)=SQRT(SSN(I)/(FLOAT(K-1)))
      SSO(I)=SQRT(SSO(I)/(FLOAT(K-1)))
  220 CONTINUE                                                          .  2590
      PSUM(1) = FLOAT(NAIT(1))                                          .  2600
      DO 240 I=2,10                                                     .  2610
      PSUM(I) = PSUM(I-1) + FLOAT(NAIT(I))                              .  2620
  240 CONTINUE                                                          .  2630
      DO 250 I=1,10                                                     .  2640
      PSUM(I) = PSUM(I)*100./FLOAT(NNN+1)                               .  2650
  250 CONTINUE                                                          .  2660
      WRITE(6,1)                                                        .  2670
```

```
      WRITE(6,260)                                                      .  2680
  260 FORMAT(1H0,38X,56H**NOX AND O2 SORTED BY LOAD CELL, AND LOAD PROBA .  2690
     1BILITY** / 1H0,54X,20HLOAD CELL DIMENSIONS /1H ,70X,5HLOWER,      .  2700
     212X,5HUPPER/1H ,36X,11HCELL NUMBER,5X,10HCENTER(MW),5X,           .  2710
     312HBOUNDARY(MW),5X,12HBOUNDARY(MW) /1H ,36X,11(1H=),5X,10(1H=),   .  2720
     45X,12(1H=),5X,12(1H=))                                            .  2730
      DO 270 I=1,10                                                     .  2740
      WRITE(6,280)I,CNTR(I),BNDR(I),BNDR(I+1)                           .  2750
  280 FORMAT(1H ,40X,I2,13X,F4.0,12X,F4.0,13X,F4.0)                     .  2760
  270 CONTINUE                                                          .  2770
      WRITE(6,290)                                                      .  2780
  290 FORMAT(1H0,54X,23HRESULTS OF LOAD SORTING / 1H0,5X,4HCELL,7X,     .  2790
     16HNO. OF,7X,8HNOX MEAN,7X,8HNOX MEAN,6X,11HNOX STD DEV,5X,       .  2800
     211HNOX STD DEV,5X,7HO2 MEAN,5X,10HO2 STD DEV,5X,10HLOAD PROB, /  .  2810
     31H ,4X,6HNUMBER,5X,7HENTRIES,5X,12HLB/10**6 BTU,7X,4HNG/J,7X,     .  2820
     412HLB/10**6 BTU,8X,4HNG/J,9X,7HPERCENT,6X,7HPERCENT,8X,           .  2830
     57HPERCENT /1H ,4X,6(1H=),5X,7(1H=),5X,12(1H=),5X,8(1H=),5X,       .  2840
     612(1H=),5X,11(1H=),5X,7(1H=),5X,10(1H=),5X,10(1H=))               .  2850
      DO 300 I=1,10                                                     .  2860
      A = AAN(I)*AVERT                                                  .  2870
      B = SSN(I)*AVERT                                                  .  2880
      WRITE(6,310)I,NBIT(I),AAN(I),A,SSN(I),B,AND(I),SSO(I),PSUM(I)     .  2890
  310 FORMAT(1H ,6X,I2,8X,I4,10X,F5.3,11X,F4.0,10X,F6.4,11X,F5.1,9X,    .  2900
     1F5.2,8X,F5.2,10X,F5.2)                                            .  2910
  300 CONTINUE                                                          .  2920
C     CALCULATE NOX PROBABILITY                                         .  2930
      A=VAL1(1)
      B=VAL1(1)
      DO 700 I=2,NNN
      IF(VAL1(I).LT.A)A=VAL1(I)
      IF(VAL1(I).GT.B)B=VAL1(I)
  700 CONTINUE
      A=A-.005
      B=B+.005                                                          .  2951
      C = (B-A)/10.                                                     .  2960
      BNDR(1)=A                                                         .  2970
      BNDR(11)=B                                                        .  2980
      DO 320 I=2,10                                                     .  2990
      BNDR(I)=BNDR(I-1)+C                                               .  3000
  320 CONTINUE                                                          .  3010
      CNTR(1)=A+C/2.                                                    .  3020
      CNTR(10)=B-C/2.                                                   .  3030
      DO 325 I=2,9                                                      .  3040
      CNTR(I)=CNTR(I-1)+C                                               .  3050
  325 CONTINUE                                                          .  3060
      DO 330 I=1,10                                                     .  3070
      NBIT(I)=0                                                         .  3080
  330 CONTINUE                                                          .  3090
      DO 335 I=1,NNN                                                    .  3100
      D = VAL1(I)                                                       .  3110
      IF((D.GE.BNDR( 1)).AND.(D.LT.BNDR( 2)))GO TO 340                  .  3120
      IF((D.GE.BNDR( 2)).AND.(D.LT.BNDR( 3)))GO TO 345                  .  3130
      IF((D.GE.BNDR( 3)).AND.(D.LT.BNDR( 4)))GO TO 350                  .  3140
      IF((D.GE.BNDR( 4)).AND.(D.LT.BNDR( 5)))GO TO 355                  .  3150
      IF((D.GE.BNDR( 5)).AND.(D.LT.BNDR( 6)))GO TO 360                  .  3160
      IF((D.GE.BNDR( 6)).AND.(D.LT.BNDR( 7)))GO TO 365                  .  3170
      IF((D.GE.BNDR( 7)).AND.(D.LT.BNDR( 8)))GO TO 370                  .  3180
      IF((D.GE.BNDR( 8)).AND.(D.LT.BNDR( 9)))GO TO 375                  .  3190
      IF((D.GE.BNDR( 9)).AND.(D.LT.BNDR(10)))GO TO 380                  .  3200
```

```
      IF((D.GE.BNDR(10)).AND.(D.LT.BNDR(11)))GO TO 385                  .  3210
      NBIT(1)=NBIT(1)+1                                                 .  3220
      GO TO 335                                                         .  3230
  345 NBIT(2)=NBIT(2)+1                                                 .  3240
      GO TO 335                                                         .  3250
  350 NBIT(3)=NBIT(3)+1                                                 .  3260
      GO TO 335                                                         .  3270
  355 NBIT(4)=NBIT(4)+1                                                 .  3280
      GO TO 335                                                         .  3290
  360 NBIT(5)=NBIT(5)+1                                                 .  3300
      GO TO 335                                                         .  3310
  365 NBIT(6)=NBIT(6)+1                                                 .  3320
      GO TO 335                                                         .  3330
  370 NBIT(7)=NBIT(7)+1                                                 .  3340
      GO TO 335                                                         .  3350
  375 NBIT(8)=NBIT(8)+1                                                 .  3360
      GO TO 335                                                         .  3370
  380 NBIT(9)=NBIT(9)+1                                                 .  3380
      GO TO 335                                                         .  3390
  385 NBIT(10)=NBIT(10)+1                                               .  3400
  335 CONTINUE                                                          .  3410
      PSUM(1)=FLOAT(NBIT(1))                                            .  3420
      DO 390 I=2,10                                                     .  3430
      PSUM(I)=PSUM(I-1)+FLOAT(NBIT(I))                                  .  3440
  390 CONTINUE                                                          .  3450
      DO 400 I=1,10                                                     .  3460
      PSUM(I)=PSUM(I)*100. /FLOAT(NNN+1)                                .  3470
  400 CONTINUE                                                          .  3480
      WRITE(6,1)                                                        .  3490
      WRITE(6,410)                                                      .  3500
  410 FORMAT(1H0,56X,19H**NOX PROBABILITY** /1H0,56X,19HNOX CELL DIMENSI .  3510
     1ONS /1H0,68X,5HLOWER,18X,5HUPPER/1H ,29X,4HCELL,12X,6HCENTER,     .  3520
     216X,8HBOUNDARY,15X,8HBOUNDARY /1H ,28X,6HNUMBER,5X,18HLB/10**6 BTU .  3530
     3  NG/J, 2(5X,18HLB/10**6 BTU  NG/J ) /1H ,28X,6(1H-), 3(5X,12(1H-) .  3540
     4,2X,4(1H-)))                                                      .  3550
      DO 420 I=1,10                                                     .  3560
      A=CNTR(I)*AVERT                                                   .  3570
      B=BNDR(I)*AVERT                                                   .  3580
      C=BNDR(I+1)*AVERT                                                 .  3590
      WRITE(6,430)I,CNTR(I),A,BNDR(I),B,BNDR(I+1),C                     .  3600
  430 FORMAT(1H ,30X,I2,10X,F5.3,6X,F4.0,8X,F5.3,6X,F4.0,8X,F5.3,6X,    .  3610
     1F4.0)                                                             .  3620
  420 CONTINUE                                                          .  3630
      WRITE(6,440)                                                      .  3640
  440 FORMAT(1H0,54X,23HNOX PROBABILITY RESULTS /1H0,78X,10HCUM. PROB./ .  3650
     11H ,44X,4HCELL,11X,9HNUMBER OF,11X,7HPERCENT/1H ,43X,6HNUMBER,    .  3660
     211X,7HENTRIES,11X,9HLESS THAN /1H ,43X,6(1H-),10X,9(1H-),10X,     .  3670
     310(1H-))                                                          .  3680
      DO 450 I=1,10                                                     .  3690
      WRITE(6,460)I,NBIT(I),PSUM(I)                                     .  3700
  460 FORMAT(1H ,45X,I2,14X,I4,15X,F5.2)                                .  3710
  450 CONTINUE                                                          .  3720
C     DETERMINE COMPLIANCE WITH RESPECT TO 1971 NSPS USING 3-HOUR       .  3730
C     AVERAGES. I1971 COUNTS NUMBER OF EXCESS EMISSION PERIODS.         .  3740
      ELIM = 0.7                                                        .  3750
      IF(ICOAL.EQ.1)ELIM=0.8                                            .  3760
      IF(ICOAL.EQ.2)ELIM=0.6                                            .  3770
      IELIM=1000.*ELIM                                                  .
      I1971=0                                                           .  3780
```

```
      M=NNN-2                                                          .  3790
      DO 470 I=1,M                                                     .  3800
      A=(VAL1(I)+VAL1(I+1)+VAL1(I+2))/3.                               .  3810
C     CHECK FOR EXCEEDANCE TO 2 DECIMAL PLACES
      IA=1000.*A
      IF(IA-IELIM.GT.4)I1971=I1971+1
  470 CONTINUE                                                         .  3830
      WRITE(6,1)                                                       .  3840
      WRITE(6,475)                                                     .  3850
  475 FORMAT(1H0,44X,44H**NOX COMPLIANCE WITH RESPECT TO 1971 NSPS** /  .  3860
     1 1H0,27X,78HFOR SUBBITUMINOUS COAL THE EMISSION LIMITATION IS 0.70  .  3870
     2LB/10**6 BTU (300 NG/J)  /1H0,29X,75HFOR BITUMINOUS COAL THE EMISS .  3880
     3ION LIMITATION IS 0.70 LB/10**6 BTU (300 NG/J) /1H0,17X,99HFOR LIG .  3890
     4NITE MINED IN THE DAKOTAS OR MONTANA THE EMISSION LIMITATION IS 0.  .  3900
     580 LB/10**6 BTU (340 NG/J) /1H0,27X,79HFOR OTHER LIGNITE COALS THE  .  3910
     6 EMISSION LIMITATION IS 0.60 LB/10**6 BTU (260 NG/J) )              .  3920
      IF(ICOAL .EQ. -1)WRITE(6,480)                                    .  3930
      IF(ICOAL .EQ.  0)WRITE(6,485)                                    .  3940
      IF(ICOAL .EQ.  1)WRITE(6,490)                                    .  3950
      IF(ICOAL .EQ.  2)WRITE(6,495)                                    .  3960
  480 FORMAT(1H0,42X,48HTHIS BOILER WAS OPERATED WITH SUBBITUMINOUS COAL .  3970
     1 )                                                               .  3980
  485 FORMAT(1H0,43X,45HTHIS BOILER WAS OPERATED WITH BITUMINOUS COAL )  .  3990
  490 FORMAT(1H0,29X,74HTHIS BOILER WAS OPERATED WITH LIGNITE COAL MINED .  4000
     1 IN THE DAKOTAS OR MONTANA )                                     .  4010
  495 FORMAT(1H0,23X,85HTHIS BOILER WAS OPERATED WITH LIGNITE COAL OTHER .  4020
     1 THAN MINED IN THE DAKOTAS OR MONTANA )                          .  4030
      AAA = PERFM*AVERT                                                .  4040
      WRITE(6,500)PERFM,AAA                                            .  4050
  500 FORMAT(1H0,25X,50HTHE NOX MEASURED DURING THE PERFORMANCE TEST WAS .  4060
     1    , F5.3, 16H  LB/10**6 BTU ( , F4.0, 6H NG/J) )                .  4070
      WRITE(6,510)I1971                                                .  4080
  510 FORMAT(1H0,9X,114HAN ANALYSIS OF 3-HOUR NOX ROLLING AVERAGES (EXCL
     1UDING PERIODS WHEN THE BOILER WAS OFF-LINE OR MONITOR INOPERATIVE)
     2 /1H0,28X,60HINDICATED THAT THE NOX EMISSION LIMITATION WAS EXCEED
     3ED ON    . I4,11H  OCCASIONS )
C     CALCULATE EXCESS EMISSIONS ON 3-HOUR BLOCK AVERAGE
      I1971=0
      N4=1
 2000 CONTINUE
      IF(N4.GT.NNN-2)GO TO 2010
      A=(VAL1(N4)+VAL1(N4+1)+VAL1(N4+2))/3.
      IA=1000.*A
      IF(IA-IELIM.GT.4)GO TO 2020
      N4=N4+1
      GO TO 2000
 2020 I1971=I1971+1
      N4=N4+3
      GO TO 2000
 2010 CONTINUE
      WRITE(6,2030)I1971
 2030 FORMAT(1H0,10X,112HAN ANALYSIS OF 3-HOUR NOX BLOCK AVERAGES (EXCLU
     1DING PERIODS WHEN THE BOILER WAS OFF-LINE OR MONITOR INOPERATIVE)/
     21H0,28X,60HINDICATED THAT THE NOX EMISSION LIMITATION WAS EXCEEDED
     3 ON    .  I4, 11H  OCCASIONS )
C     SEARCH NOX DAILY AVERAGES FOR PERIODS OF EXCESS EMISSIONS WITH    .  4130
C     RESPECT TO 1978 NSPS ON 30-DAY ROLLING AVERAGE BASIS             .  4140
      ELIM = 0.5                                                       .  4150
      IF(ICOAL .EQ. 0)ELIM=0.6                                         .  4160
```

```
      IF(ICOAL .EQ. 1)ELIM=0.8                                          .  4170
      IF(ICOAL .EQ. 2)ELIM=0.6                                          .  4180
      IELIM=1000.*ELIM
C     PACK VALID DAILY NOX AVERAGES INTO DALY(N)                        .  4190
      N = 0                                                             .  4200
      DO 520 I=1,NDAYS                                                  .  4210
      IF(IDAY(I).LE.0)GO TO 520                                         .  4220
      N=N+1                                                             .  4230
      DALY(N) = NOXMN(I)                                                .  4240
  520 CONTINUE                                                          .  4250
C     CALCULATE 30-DAY ROLLING AVERAGES ROLAVE                          .  4260
      I = 1                                                             .  4270
      J = 30                                                            .  4280
      SUM = 0.                                                          .  4290
      MM = N-29                                                         .  4300
C     MM = TOTAL NUMBER OF ROLLING AVERAGES                             .  4310
C     IF MM .LT. 1 SKIP ROLLING AVERAGE CALCULATION                     .  4311
      IF(MM.LT. 1) GO TO 900                                            .  4312
      DO 530 L=1,MM                                                     .  4320
      DO 540 K=I,J                                                      .  4330
      SUM = SUM + DALY(K)                                               .  4340
  540 CONTINUE                                                          .  4350
      ROLAVE(I) = SUM/30.                                               .  4360
      I=I+1                                                             .  4370
      J=J+1                                                             .  4380
      SUM=0.                                                            .  4390
  530 CONTINUE                                                          .  4400
C     I1978 COUNT ON EXCEEDANCES OF 1978 LIMITATION                     .  4410
      I1978 = 0                                                         .  4420
      DO 550 I=1,MM                                                     .  4430
C     CHECK FOR EXCEEDANCE TO 2 DECIMAL PLACES
      IROL=1000.*ROLAVE(I)
      IF(IROL-IELIM.GT.4)I1978=I1978+1
  550 CONTINUE                                                          .  4450
      WRITE(6,1)                                                        .  4460
      WRITE(6,555)                                                      .  4470
  555 FORMAT(1H0,44X,44H**NOX COMPLIANCE WITH RESPECT TO 1978 NSPS**  ) .  4480
      WRITE(6,560)                                                      .  4490
  560 FORMAT(1H0,49X,34H1978 NSPS NOX EMISSION LIMITATIONS /1H ,41X,    .  4500
     149HSUBBITUMINOUS COAL = 0.50 LB/10**6 BTU (210 NG/J) /1H ,43X,    .  4510
     246HBITUMINOUS COAL = 0.60 LB/10**6 BTU (260 NG/J)    /1H ,33X,    .  4520
     366HLIGNITE MINED IN DAKOTAS OR MONTANA = 0.80 LB/10**6 BTU (340 NG.  4530
     4/J) /1H ,43X,45HOTHER LIGNITES = 0.60 LB/10**6 BTU (260 NG/J) )   .  4540
      IPERFM=1000.*PERFM
      IF(IPERFM-IELIM .LT.5)WRITE(6,570)
      IF(IPERFM-IELIM .GE.5)WRITE(6,575)
  570 FORMAT(1H0,26X,79HTHIS BOILER, HAD IT BEEN SUBJECT TO 1978 NSPS, W.  4570
     1OULD HAVE MET PERFORMANCE LIMIT )                                 .  4580
  575 FORMAT(1H0,24X,83HTHIS BOILER, HAD IT BEEN SUBJECT TO 1978 NSPS, W.  4590
     1OULD NOT HAVE MET PERFORMANCE LIMIT )                             .  4600
      WRITE(6,580)I1978                                                 .  4610
  580 FORMAT(1H0,34X,47HANALYSIS OF 30-DAY ROLLING AVERAGES INDICATED  .  .  4620
     1I3, 13H  EXCEEDANCES )                                            .  4630
      AAAA=ELIM*AVERT                                                   .  4640
      WRITE(6,590)ELIM,AAAA                                             .  4650
  590 FORMAT(1H0,54X,23H30-DAY ROLLING AVERAGES /1H ,42X,20HEMISSION LIM.  4660
     1ITATION  ,F4.2 , 15H LB/10**6 BTU   ,F4.0, 5H NG/J )              .  4670
      WRITE(6,600)                                                      .  4680
  600 FORMAT(1H0,47X,10HSEQUENTIAL ,10X,18H30-DAY AVERAGE NOX /1H ,48X,  .  4690
```

```
      17HAVERAGE , 12X, 18HLB/10**6 BTU  NG/J /1H ,47X, 10(1H-), 10X,
     212(1H-), 2X, 4(1H-))
      DO 610 I=1,MM
      AAAA=ROLAVE(I)*AVERT
      WRITE(6,620)I,ROLAVE(I),AAAA
  610 CONTINUE
  620 FORMAT(1H ,51X,I2,16X,F5.3,7X,F4.0)
      GO TO 920
  900 WRITE(6,910)
  910 FORMAT(1H0,39X,54HINSUFFICIENT DATA TO CALCULATE 30-DAY ROLLING AV
     1ERAGES )
  920 CONTINUE
      END
```

```
      SUBROUTINE STAT(N,A,AVE,STD)
      DIMENSION A(N)
      AVE=0.
      DO 10 J=1,N
      AVE=AVE+A(J)
   10 CONTINUE
      AVE=AVE/FLOAT(N)
      STD=0.
      DO 20 J=1,N
      STD=STD+(A(J)-AVE)**2
   20 CONTINUE
      STD=SQRT(STD/(FLOAT(N)-1.))
      RETURN
      END
```

APPENDIX B

OKLAHOMA GAS & ELECTRIC

MUSKOGEE STATION - UNIT 4

Input Data - Initial Analysis

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

DATA SUBMITTED BY OKLAHOMA GAS AND ELECTRIC MUSKOGEE STATION

UNIT 4  SUBBITUMINOUS COAL  NOX MON. REL. ACC. = 10.9 PC

DAY 1 IS OCTOBER 15, 1980  DAY 94 IS JANUARY 16, 1981

550 MWE, COMBUSTION ENGINEERING BOILER WITH OVERFIRE AIR

COAL PROXIMATE 8815+-578TU/LB, 0.337+-0.037 PC SULFUR,

4.86+-0.371 PC ASH, 27.73+-0.36 PC MOISTURE

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 10.0 | 180. |
| 2 | .460 | 198. | 10.0 | 180. |
| 3 | .460 | 198. | 10.0 | 180. |
| 4 | .450 | 193. | 10.0 | 180. |
| 5 | .450 | 193. | 10.0 | 180. |
| 6 | .450 | 193. | 10.0 | 178. |
| 7 | .450 | 193. | 9.7 | 220. |
| 8 | .540 | 232. | 8.1 | 305. |
| 9 | .520 | 223. | 8.6 | 225. |
| 10 | .420 | 180. | 9.9 | 180. |
| 11 | .360 | 155. | 10.0 | 180. |
| 12 | .350 | 150. | 10.0 | 180. |
| 13 | .350 | 150. | 10.0 | 180. |
| 14 | .340 | 146. | 9.8 | 180. |
| 15 | .340 | 146. | 9.8 | 180. |
| 16 | .350 | 150. | 10.0 | 180. |
| 17 | .350 | 150. | 10.0 | 180. |
| 18 | .360 | 155. | 10.0 | 180. |
| 19 | .350 | 150. | 10.0 | 180. |
| 20 | .350 | 150. | 10.0 | 180. |
| 21 | .350 | 150. | 10.0 | 180. |
| 22 | .350 | 150. | 10.0 | 180. |
| 23 | .350 | 150. | 10.0 | 180. |
| 24 | .360 | 155. | 10.0 | 180. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 10.0 | 180. |
| 2 | .360 | 155. | 9.9 | 180. |
| 3 | .350 | 150. | 9.9 | 180. |
| 4 | .340 | 146. | 10.0 | 182. |
| 5 | .330 | 142. | 9.9 | 182. |
| 6 | .340 | 146. | 9.9 | 182. |
| 7 | .400 | 172. | 9.7 | 182. |
| 8 | .400 | 172. | 9.9 | 180. |
| 9 | .440 | 189. | 9.8 | 180. |
| 10 | .400 | 172. | 9.8 | 180. |
| 11 | .400 | 172. | 9.8 | 180. |
| 12 | .390 | 168. | 9.8 | 180. |
| 13 | .380 | 163. | 9.7 | 180. |
| 14 | .400 | 172. | 9.9 | 180. |
| 15 | .420 | 180. | 10.0 | 180. |
| 16 | .410 | 176. | 10.0 | 180. |
| 17 | .400 | 172. | 10.0 | 180. |
| 18 | .390 | 168. | 9.9 | 180. |
| 19 | .390 | 168. | 10.0 | 180. |
| 20 | .390 | 168. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 21 | .390 | 168. | 9.9 | 180. |
| 22 | .390 | 168. | 9.9 | 180. |
| 23 | .390 | 168. | 9.8 | 180. |
| 24 | .380 | 163. | 9.8 | 182. |

DAY = 3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 9.9 | 180. |
| 2 | .410 | 176. | 9.9 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .410 | 176. | 9.9 | 180. |
| 5 | .410 | 176. | 9.9 | 180. |
| 6 | .420 | 180. | 9.9 | 182. |
| 7 | .440 | 189. | 9.4 | 228. |
| 8 | .460 | 198. | 8.8 | 275. |
| 9 | .480 | 206. | 8.6 | 300. |
| 10 | .410 | 176. | 7.8 | 325. |
| 11 | .410 | 176. | 7.7 | 325. |
| 12 | .420 | 180. | 7.8 | 325. |
| 13 | .430 | 185. | 7.8 | 325. |
| 14 | .440 | 189. | 7.9 | 325. |
| 15 | .450 | 193. | 7.9 | 325. |
| 16 | .450 | 193. | 7.9 | 325. |
| 17 | .470 | 202. | 8.2 | 250. |
| 18 | .540 | 232. | 9.5 | 225. |
| 19 | .550 | 236. | 9.5 | 225. |
| 20 | .540 | 232. | 9.4 | 225. |
| 21 | .540 | 232. | 9.4 | 225. |
| 22 | .560 | 241. | 9.5 | 225. |
| 23 | .560 | 241. | 9.5 | 225. |
| 24 | .560 | 241. | 9.5 | 225. |

DAY = 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 9.6 | 195. |
| 2 | .390 | 168. | 10.0 | 180. |
| 3 | .380 | 163. | 10.0 | 180. |
| 4 | .390 | 168. | 10.0 | 180. |
| 5 | .400 | 172. | 10.0 | 180. |
| 6 | .400 | 172. | 10.0 | 180. |
| 7 | .400 | 172. | 10.0 | 180. |
| 8 | .390 | 168. | 10.0 | 180. |
| 9 | .360 | 155. | 10.0 | 180. |
| 10 | .390 | 168. | 10.0 | 180. |
| 11 | .380 | 163. | 10.0 | 180. |
| 12 | .380 | 163. | 10.0 | 180. |
| 13 | .370 | 159. | 10.0 | 180. |
| 14 | .380 | 163. | 10.0 | 180. |
| 15 | .370 | 159. | 10.0 | 180. |
| 16 | .380 | 163. | 10.0 | 180. |
| 17 | .370 | 159. | 10.0 | 180. |
| 18 | .360 | 155. | 10.0 | 180. |
| 19 | .360 | 155. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 20 | .380 | 163. | 10.0 | 180. |
| 21 | .380 | 163. | 10.0 | 180. |
| 22 | .390 | 168. | 10.0 | 180. |
| 23 | .400 | 172. | 10.0 | 180. |
| 24 | .410 | 176. | 10.0 | 180. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.0 | 180. |
| 2 | .400 | 172. | 10.0 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .430 | 185. | 10.0 | 180. |
| 5 | .420 | 180. | 10.0 | 180. |
| 6 | .430 | 185. | 10.1 | 180. |
| 7 | .430 | 185. | 10.1 | 180. |
| 8 | .440 | 189. | 10.1 | 185. |
| 9 | .430 | 185. | 10.0 | 185. |
| 10 | .430 | 185. | 10.1 | 180. |
| 11 | .430 | 185. | 10.1 | 180. |
| 12 | .440 | 189. | 10.1 | 180. |
| 13 | .420 | 180. | 10.1 | 180. |
| 14 | .430 | 185. | 10.1 | 180. |
| 15 | .400 | 172. | 10.1 | 180. |
| 16 | .410 | 176. | 10.1 | 180. |
| 17 | .400 | 172. | 10.1 | 180. |
| 18 | .410 | 176. | 10.1 | 180. |
| 19 | .410 | 176. | 10.1 | 180. |
| 20 | .400 | 172. | 10.1 | 180. |
| 21 | .400 | 172. | 10.1 | 180. |
| 22 | .410 | 176. | 10.1 | 180. |
| 23 | .400 | 172. | 10.1 | 180. |
| 24 | .400 | 172. | 10.1 | 180. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.1 | 180. |
| 2 | .400 | 172. | 10.1 | 180. |
| 3 | .410 | 176. | 10.1 | 180. |
| 4 | .410 | 176. | 10.1 | 180. |
| 5 | .410 | 176. | 10.0 | 180. |
| 6 | .420 | 180. | 10.1 | 180. |
| 7 | .450 | 193. | 9.5 | 240. |
| 8 | .510 | 219. | 7.9 | 325. |
| 9 | .530 | 228. | 7.9 | 325. |
| 10 | .520 | 223. | 7.9 | 325. |
| 11 | .510 | 219. | 7.8 | 330. |
| 12 | .510 | 219. | 7.9 | 330. |
| 13 | .500 | 215. | 7.9 | 330. |
| 14 | .520 | 223. | 7.9 | 330. |
| 15 | .520 | 223. | 7.9 | 330. |
| 16 | .520 | 223. | 7.8 | 330. |
| 17 | .510 | 219. | 7.8 | 330. |
| 18 | .510 | 219. | 7.8 | 330. |

| | | | | |
|---|---|---|---|---|
| 19 | .510 | 219. | 7.8 | 330. |
| 20 | .510 | 219. | 7.8 | 330. |
| 21 | .520 | 223. | 7.8 | 330. |
| 22 | .590 | 253. | 8.5 | 280. |
| 23 | .640 | 275. | 8.7 | 280. |
| 24 | .650 | 279. | 8.8 | 280. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.0 | 180. |
| 2 | .420 | 180. | 10.1 | 180. |
| 3 | .420 | 180. | 10.1 | 180. |
| 4 | .420 | 180. | 10.0 | 180. |
| 5 | .410 | 176. | 10.0 | 180. |
| 6 | .410 | 176. | 10.0 | 180. |
| 7 | .460 | 198. | 9.4 | 280. |
| 8 | .490 | 210. | 7.8 | 325. |
| 9 | .490 | 210. | 7.7 | 325. |
| 10 | .500 | 215. | 7.7 | 330. |
| 11 | .500 | 215. | 7.7 | 330. |
| 12 | .500 | 215. | 7.7 | 330. |
| 13 | .490 | 210. | 7.7 | 330. |
| 14 | .490 | 210. | 7.7 | 330. |
| 15 | .480 | 206. | 7.7 | 330. |
| 16 | .470 | 202. | 7.7 | 330. |
| 17 | .450 | 193. | 7.8 | 330. |
| 18 | .450 | 193. | 7.8 | 330. |
| 19 | .450 | 193. | 7.8 | 330. |
| 20 | .460 | 198. | 7.8 | 330. |
| 21 | .470 | 202. | 7.8 | 330. |
| 22 | .480 | 206. | 7.9 | 330. |
| 23 | .490 | 210. | 7.9 | 330. |
| 24 | .510 | 219. | 8.7 | 230. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 9.5 | 230. |
| 2 | .520 | 223. | 9.7 | 180. |
| 3 | .440 | 189. | 10.0 | 180. |
| 4 | .430 | 185. | 10.0 | 180. |
| 5 | .440 | 189. | 10.1 | 180. |
| 6 | .430 | 185. | 10.0 | 190. |
| 7 | .520 | 223. | 9.3 | 230. |
| 8 | .530 | 228. | 9.3 | 230. |
| 9 | .500 | 215. | 8.8 | 280. |
| 10 | .470 | 202. | 8.1 | 330. |
| 11 | .460 | 198. | 7.8 | 330. |
| 12 | .550 | 236. | 8.7 | 270. |
| 13 | .570 | 245. | 9.1 | 260. |
| 14 | .550 | 236. | 8.8 | 320. |
| 15 | .540 | 232. | 8.6 | 280. |
| 16 | .550 | 236. | 8.7 | 280. |
| 17 | .550 | 236. | 8.7 | 280. |

| | | | | |
|---|---|---|---|---|
| 18 | .550 | 236. | 8.7 | 280. |
| 19 | .540 | 232. | 8.7 | 280. |
| 20 | .530 | 228. | 8.7 | 280. |
| 21 | .540 | 232. | 8.6 | 280. |
| 22 | .480 | 206. | 8.9 | 230. |
| 23 | .450 | 193. | 9.4 | 230. |
| 24 | .470 | 202. | 9.5 | 230. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.0 | 175. |
| 2 | .400 | 172. | 10.0 | 175. |
| 3 | .410 | 176. | 10.1 | 175. |
| 4 | .420 | 180. | 10.1 | 175. |
| 5 | .420 | 180. | 10.1 | 175. |
| 6 | .420 | 180. | 10.1 | 175. |
| 7 | .410 | 176. | 10.1 | 175. |
| 8 | .530 | 228. | 9.4 | 230. |
| 9 | .540 | 232. | 9.1 | 280. |
| 10 | .480 | 206. | 8.2 | 340. |
| 11 | .460 | 198. | 7.4 | 355. |
| 12 | .410 | 176. | 7.4 | 355. |
| 13 | .410 | 176. | 7.4 | 355. |
| 14 | .420 | 180. | 7.4 | 355. |
| 15 | .420 | 180. | 7.4 | 355. |
| 16 | .450 | 193. | 7.4 | 350. |
| 17 | .480 | 206. | 7.8 | 322. |
| 18 | .490 | 210. | 7.9 | 320. |
| 19 | .490 | 210. | 7.9 | 320. |
| 20 | .480 | 206. | 7.8 | 320. |
| 21 | .500 | 215. | 7.9 | 320. |
| 22 | .430 | 185. | 8.6 | 272. |
| 23 | .440 | 189. | 9.0 | 228. |
| 24 | .580 | 249. | 9.5 | 230. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 10.1 | 175. |
| 2 | .470 | 202. | 10.1 | 175. |
| 3 | .480 | 206. | 10.0 | 175. |
| 4 | .480 | 206. | 10.1 | 175. |
| 5 | .480 | 206. | 10.1 | 175. |
| 6 | .480 | 206. | 10.1 | 175. |
| 7 | .490 | 210. | 10.1 | 175. |
| 8 | .480 | 206. | 10.1 | 175. |
| 9 | .530 | 228. | 9.3 | 290. |
| 10 | .540 | 232. | 8.1 | 330. |
| 11 | .490 | 210. | 7.8 | 300. |
| 12 | .480 | 206. | 9.2 | 230. |
| 13 | .510 | 219. | 9.5 | 230. |
| 14 | .510 | 219. | 9.5 | 230. |
| 15 | .500 | 215. | 9.5 | 230. |
| 16 | .500 | 215. | 9.5 | 232. |

| | | | | |
|---|---|---|---|---|
| 17 | .500 | 215. | 9.5 | 234. |
| 18 | .510 | 219. | 9.6 | 234. |
| 19 | .500 | 215. | 9.6 | 232. |
| 20 | .470 | 202. | 9.0 | 274. |
| 21 | .450 | 193. | 8.9 | 279. |
| 22 | .460 | 198. | 8.8 | 300. |
| 23 | .460 | 198. | 8.4 | 300. |
| 24 | .550 | 236. | 9.3 | 220. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 9.9 | 175. |
| 2 | .460 | 198. | 10.1 | 175. |
| 3 | .490 | 210. | 10.1 | 180. |
| 4 | .490 | 210. | 10.1 | 180. |
| 5 | .500 | 215. | 10.1 | 180. |
| 6 | .490 | 210. | 10.1 | 180. |
| 7 | .490 | 210. | 10.1 | 180. |
| 8 | .490 | 210. | 9.8 | 235. |
| 9 | .480 | 206. | 7.8 | 375. |
| 10 | .470 | 202. | 7.1 | 380. |
| 11 | .460 | 198. | 7.1 | 380. |
| 12 | .480 | 206. | 7.1 | 380. |
| 13 | .530 | 228. | 7.1 | 380. |
| 14 | .550 | 236. | 7.2 | 350. |
| 15 | .600 | 258. | 8.1 | 240. |
| 16 | .600 | 258. | 9.0 | 202. |
| 17 | .630 | 271. | 10.0 | 202. |
| 18 | .640 | 275. | 9.8 | 226. |
| 19 | .490 | 210. | 9.3 | 225. |
| 20 | .530 | 228. | 9.2 | 250. |
| 21 | .540 | 232. | 9.2 | 255. |
| 22 | .530 | 228. | 9.5 | 190. |
| 23 | .470 | 202. | 10.1 | 178. |
| 24 | .470 | 202. | 10.1 | 175. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.1 | 175. |
| 2 | .460 | 198. | 10.1 | 175. |
| 3 | .450 | 193. | 10.1 | 175. |
| 4 | .460 | 198. | 10.1 | 180. |
| 5 | .460 | 198. | 10.1 | 180. |
| 6 | .440 | 189. | 10.1 | 180. |
| 7 | .430 | 185. | 10.1 | 180. |
| 8 | .450 | 193. | 10.1 | 280. |
| 9 | .450 | 193. | 9.6 | 280. |
| 10 | .410 | 176. | 8.7 | 280. |
| 11 | .420 | 180. | 8.7 | 280. |
| 12 | .420 | 180. | 8.8 | 280. |
| 13 | .430 | 185. | 8.8 | 280. |
| 14 | .430 | 185. | 8.8 | 280. |
| 15 | .420 | 180. | 8.8 | 280. |

| | | | | |
|---|---|---|---|---|
| 16 | .420 | 180. | 8.7 | 280. |
| 17 | .460 | 198. | 9.3 | 260. |
| 18 | .470 | 202. | 9.0 | 300. |
| 19 | .460 | 198. | 8.4 | 300. |
| 20 | .440 | 189. | 8.3 | 300. |
| 21 | .450 | 193. | 8.3 | 300. |
| 22 | .470 | 202. | 8.4 | 250. |
| 23 | .490 | 210. | 8.6 | 178. |
| 24 | .450 | 193. | 9.9 | 175. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.1 | 175. |
| 2 | .460 | 198. | 10.1 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .400 | 172. | 10.1 | 180. |
| 5 | .400 | 172. | 10.0 | 180. |
| 6 | .400 | 172. | 10.1 | 180. |
| 7 | .400 | 172. | 10.1 | 375. |
| 8 | .460 | 198. | 8.0 | 425. |
| 9 | .480 | 206. | 6.8 | 420. |
| 10 | .460 | 198. | 6.7 | 420. |
| 11 | .460 | 198. | 6.7 | 430. |
| 12 | .430 | 185. | 6.7 | 420. |
| 13 | .430 | 185. | 6.8 | 425. |
| 14 | .440 | 189. | 6.5 | 430. |
| 15 | .430 | 185. | 6.5 | 430. |
| 16 | .430 | 185. | 6.5 | 422. |
| 17 | .440 | 189. | 6.5 | 422. |
| 18 | .430 | 185. | 6.5 | 422. |
| 19 | .420 | 180. | 6.5 | 422. |
| 20 | .430 | 185. | 6.6 | 420. |
| 21 | .460 | 198. | 6.6 | 420. |
| 22 | .480 | 206. | 6.9 | 365. |
| 23 | .450 | 193. | 8.6 | 274. |
| 24 | .440 | 189. | 8.8 | 270. |

DAY = 14

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 8.5 | 230. |
| 2 | .500 | 215. | 9.6 | 230. |
| 3 | .500 | 215. | 9.5 | 230. |
| 4 | .490 | 210. | 9.4 | 230. |
| 5 | .520 | 223. | 9.5 | 230. |
| 6 | .490 | 210. | 9.1 | 280. |
| 7 | .490 | 210. | 8.3 | 350. |
| 8 | .490 | 210. | 6.7 | 370. |
| 9 | .570 | 245. | 7.7 | 330. |
| 10 | .590 | 253. | 7.8 | 330. |
| 11 | .590 | 253. | 7.9 | 330. |
| 12 | .590 | 253. | 7.8 | 325. |
| 13 | .590 | 253. | 7.9 | 325. |
| 14 | .590 | 253. | 7.9 | 325. |

| | | | | |
|---|---|---|---|---|
| 15 | .600 | 258. | 7.9 | 325. |
| 16 | .420 | 266. | 8.1 | 300. |
| 17 | .660 | 284. | 8.5 | 300. |
| 18 | .590 | 253. | 8.0 | 375. |
| 19 | .530 | 228. | 7.1 | 420. |
| 20 | .590 | 253. | 6.8 | 418. |
| 21 | .590 | 253. | 6.8 | 416. |
| 22 | .610 | 262. | 6.8 | 415. |
| 23 | .580 | 249. | 7.5 | 348. |
| 24 | .580 | 249. | 8.3 | 295. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 8.5 | 295. |
| 2 | .540 | 232. | 8.5 | 295. |
| 3 | .540 | 232. | 8.6 | 295. |
| 4 | .540 | 232. | 8.6 | 300. |
| 5 | .540 | 232. | 8.6 | 300. |
| 6 | .550 | 236. | 8.6 | 300. |
| 7 | .610 | 262. | 7.7 | 360. |
| 8 | .690 | 296. | 8.1 | 330. |
| 9 | .670 | 288. | 8.1 | 330. |
| 10 | .670 | 288. | 8.1 | 330. |
| 11 | .660 | 284. | 8.6 | 275. |
| 12 | .620 | 266. | 9.0 | 275. |
| 13 | .590 | 253. | 9.0 | 275. |
| 14 | .610 | 262. | 9.2 | 250. |
| 15 | .560 | 241. | 8.1 | 348. |
| 16 | .570 | 245. | 7.7 | 350. |
| 17 | .560 | 241. | 7.7 | 350. |
| 18 | .550 | 236. | 7.7 | 350. |
| 19 | .570 | 245. | 7.7 | 350. |
| 20 | .590 | 253. | 7.7 | 350. |
| 21 | .590 | 253. | 7.7 | 350. |
| 22 | .590 | 253. | 7.7 | 350. |
| 23 | .480 | 206. | 8.5 | 300. |
| 24 | .540 | 232. | 8.5 | 295. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 8.4 | 295. |
| 2 | .600 | 258. | 8.4 | 295. |
| 3 | .650 | 279. | 8.3 | 295. |
| 4 | .660 | 284. | 8.4 | 295. |
| 5 | .620 | 266. | 7.5 | 415. |
| 6 | .580 | 249. | 6.9 | 415. |
| 7 | .620 | 266. | 6.9 | 420. |
| 8 | .630 | 271. | 6.9 | 420. |
| 9 | .540 | 232. | 6.8 | 420. |
| 10 | .470 | 202. | 6.8 | 420. |
| 11 | .570 | 245. | 6.8 | 420. |
| 12 | .620 | 266. | 7.1 | 360. |
| 13 | .660 | 284. | 7.5 | 360. |

| | | | | |
|---|---|---|---|---|
| 14 | .670 | 288. | 7.5 | 360. |
| 15 | .680 | 292. | 7.5 | 360. |
| 16 | .700 | 301. | 7.5 | 360. |
| 17 | .710 | 305. | 7.5 | 360. |
| 18 | .730 | 314. | 7.6 | 360. |
| 19 | .710 | 305. | 7.6 | 355. |
| 20 | .690 | 296. | 7.5 | 355. |
| 21 | .710 | 305. | 7.5 | 355. |
| 22 | .730 | 314. | 7.5 | 355. |
| 23 | .720 | 309. | 7.6 | 320. |
| 24 | .490 | 210. | 8.6 | 275. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 8.9 | 270. |
| 2 | .560 | 241. | 9.6 | 225. |
| 3 | .590 | 253. | 9.6 | 230. |
| 4 | .580 | 249. | 9.5 | 230. |
| 5 | .590 | 253. | 9.6 | 230. |
| 6 | .580 | 249. | 9.6 | 230. |
| 7 | .480 | 206. | 7.4 | 430. |
| 8 | .450 | 193. | 6.8 | 418. |
| 9 | .490 | 210. | 6.8 | 418. |
| 10 | .490 | 210. | 6.8 | 418. |
| 11 | .480 | 206. | 6.8 | 418. |
| 12 | .480 | 206. | 6.8 | 418. |
| 13 | .520 | 223. | 7.0 | 360. |
| 14 | .690 | 296. | 8.8 | 272. |
| 15 | .680 | 292. | 8.8 | 272. |
| 16 | .480 | 206. | 7.2 | 420. |
| 17 | .600 | 258. | 6.7 | 420. |
| 18 | .610 | 262. | 6.8 | 420. |
| 19 | .600 | 258. | 6.7 | 420. |
| 20 | .600 | 258. | 6.8 | 420. |
| 21 | .590 | 253. | 6.8 | 420. |
| 22 | .600 | 258. | 6.8 | 420. |
| 23 | .570 | 245. | 6.9 | 350. |
| 24 | .660 | 284. | 8.3 | 265. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 10.0 | 180. |
| 2 | .360 | 155. | 10.1 | 180. |
| 3 | .430 | 185. | 10.0 | 180. |
| 4 | .460 | 198. | 10.0 | 180. |
| 5 | .470 | 202. | 10.0 | 180. |
| 6 | .450 | 193. | 10.0 | 200. |
| 7 | .480 | 206. | 9.0 | 280. |
| 8 | .450 | 193. | 8.7 | 276. |
| 9 | .460 | 198. | 8.7 | 276. |
| 10 | .470 | 202. | 8.7 | 278. |
| 11 | .460 | 198. | 8.7 | 278. |
| 12 | .430 | 185. | 8.7 | 280. |

| | | | | |
|---|---|---|---|---|
| 13 | .420 | 180. | 8.8 | 280. |
| 14 | .510 | 219. | 9.5 | 230. |
| 15 | .510 | 219. | 9.5 | 230. |
| 16 | .510 | 219. | 9.5 | 230. |
| 17 | .510 | 219. | 9.4 | 230. |
| 18 | .520 | 223. | 9.4 | 230. |
| 19 | .520 | 223. | 9.4 | 230. |
| 20 | .510 | 219. | 9.4 | 230. |
| 21 | .520 | 223. | 9.4 | 230. |
| 22 | .530 | 228. | 9.5 | 230. |
| 23 | .510 | 219. | 9.9 | 175. |
| 24 | .460 | 198. | 10.0 | 175. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.0 | 175. |
| 2 | .430 | 185. | 10.0 | 175. |
| 3 | .430 | 185. | 10.0 | 175. |
| 4 | .430 | 185. | 10.1 | 175. |
| 5 | .430 | 185. | 10.1 | 175. |
| 6 | .530 | 228. | 10.0 | 175. |
| 7 | .390 | 168. | 10.1 | 175. |
| 8 | .390 | 168. | 10.0 | 178. |
| 9 | .500 | 215. | 8.8 | 270. |
| 10 | .520 | 223. | 8.8 | 270. |
| 11 | .510 | 219. | 8.8 | 270. |
| 12 | .490 | 210. | 8.8 | 270. |
| 13 | .510 | 219. | 8.8 | 270. |
| 14 | .520 | 223. | 8.8 | 270. |
| 15 | .510 | 219. | 8.8 | 270. |
| 16 | .510 | 219. | 8.8 | 275. |
| 17 | .510 | 219. | 8.8 | 275. |
| 18 | .510 | 219. | 8.8 | 275. |
| 19 | .500 | 215. | 8.7 | 275. |
| 20 | .500 | 215. | 8.7 | 275. |
| 21 | .500 | 215. | 8.7 | 275. |
| 22 | .490 | 210. | 8.7 | 275. |
| 23 | .500 | 215. | 8.9 | 250. |
| 24 | .540 | 232. | 9.9 | 175. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 10.1 | 175. |
| 2 | .440 | 189. | 10.1 | 175. |
| 3 | .450 | 193. | 10.1 | 175. |
| 4 | .440 | 189. | 10.0 | 175. |
| 5 | .460 | 198. | 10.1 | 175. |
| 6 | .470 | 202. | 9.3 | 300. |
| 7 | .470 | 202. | 7.3 | 430. |
| 8 | .490 | 210. | 6.6 | 418. |
| 9 | .560 | 241. | 6.6 | 418. |
| 10 | .560 | 241. | 6.6 | 420. |
| 11 | .550 | 236. | 6.6 | 420. |

| | | | | |
|---|---|---|---|---|
| 12 | .570 | 245. | 6.6 | 416. |
| 13 | .560 | 241. | 6.6 | 416. |
| 14 | .550 | 236. | 6.6 | 415. |
| 15 | .550 | 236. | 6.5 | 415. |
| 16 | .580 | 249. | 6.5 | 420. |
| 17 | .580 | 249. | 6.6 | 420. |
| 18 | .580 | 249. | 6.6 | 420. |
| 19 | .590 | 253. | 6.6 | 420. |
| 20 | .590 | 253. | 6.6 | 420. |
| 21 | .600 | 258. | 6.6 | 420. |
| 22 | .590 | 253. | 6.6 | 420. |
| 23 | .570 | 245. | 6.6 | 420. |
| 24 | .590 | 253. | 6.7 | 400. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 8.6 | 235. |
| 2 | .380 | 163. | 10.0 | 175. |
| 3 | .420 | 180. | 10.0 | 175. |
| 4 | .420 | 180. | 10.0 | 175. |
| 5 | .530 | 228. | 9.1 | 330. |
| 6 | .600 | 258. | 7.0 | 425. |
| 7 | .620 | 266. | 6.7 | 425. |
| 8 | .570 | 245. | 6.5 | 418. |
| 9 | .590 | 253. | 6.5 | 415. |
| 10 | .570 | 245. | 6.5 | 415. |
| 11 | .570 | 245. | 6.5 | 420. |
| 12 | .560 | 241. | 6.5 | 420. |
| 13 | .570 | 245. | 6.5 | 420. |
| 14 | .570 | 245. | 6.5 | 420. |
| 15 | .570 | 245. | 6.5 | 420. |
| 16 | .550 | 236. | 6.5 | 420. |
| 17 | .550 | 236. | 6.5 | 420. |
| 18 | .560 | 241. | 6.5 | 420. |
| 19 | .600 | 258. | 6.6 | 420. |
| 20 | .610 | 262. | 6.6 | 420. |
| 21 | .470 | 202. | 6.6 | 420. |
| 22 | .460 | 198. | 6.6 | 420. |
| 23 | .510 | 219. | 6.6 | 420. |
| 24 | .500 | 215. | 7.5 | 260. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -.470 | -202. | -9.6 | 0. |
| 2 | .460 | 198. | 7.8 | 330. |
| 3 | .470 | 202. | 7.8 | 330. |
| 4 | .380 | 163. | 7.4 | 380. |
| 5 | .360 | 155. | 7.2 | 380. |
| 6 | .390 | 168. | 7.0 | 425. |
| 7 | .550 | 236. | 6.7 | 425. |
| 8 | .560 | 241. | 6.7 | 425. |
| 9 | .550 | 236. | 6.7 | 425. |
| 10 | .540 | 232. | 6.6 | 425. |

| | | | | |
|---|---|---|---|---|
| 11 | .550 | 236. | 6.7 | 425. |
| 12 | .550 | 236. | 6.5 | 420. |
| 13 | .480 | 206. | 6.9 | 375. |
| 14 | .420 | 180. | 7.3 | 350. |
| 15 | .440 | 189. | 7.4 | 350. |
| 16 | .450 | 193. | 7.4 | 350. |
| 17 | .470 | 202. | 7.4 | 350. |
| 18 | .470 | 202. | 8.6 | 235. |
| 19 | .540 | 232. | 9.3 | 225. |
| 20 | .520 | 223. | 9.0 | 280. |
| 21 | .490 | 210. | 8.5 | 280. |
| 22 | .510 | 219. | 8.5 | 280. |
| 23 | .510 | 219. | 8.5 | 275. |
| 24 | .530 | 228. | 8.7 | 260. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.1 | 175. |
| 2 | .380 | 163. | 10.1 | 175. |
| 3 | .410 | 176. | 10.1 | 175. |
| 4 | .410 | 176. | 10.0 | 175. |
| 5 | .410 | 176. | 10.0 | 175. |
| 6 | .420 | 180. | 9.8 | 230. |
| 7 | .490 | 210. | 7.6 | 420. |
| 8 | .530 | 228. | 6.4 | 422. |
| 9 | .580 | 249. | 6.8 | 340. |
| 10 | .580 | 249. | 7.6 | 325. |
| 11 | .560 | 241. | 7.6 | 325. |
| 12 | .520 | 223. | 7.5 | 360. |
| 13 | .460 | 198. | 7.0 | 374. |
| 14 | .450 | 193. | 6.9 | 374. |
| 15 | .530 | 228. | 7.5 | 324. |
| 16 | .530 | 228. | 7.5 | 320. |
| 17 | .530 | 228. | 7.3 | 360. |
| 18 | .470 | 202. | 6.5 | 410. |
| 19 | .440 | 189. | 6.4 | 410. |
| 20 | .440 | 189. | 6.4 | 410. |
| 21 | .460 | 198. | 6.5 | 410. |
| 22 | .480 | 206. | 7.4 | 315. |
| 23 | .480 | 206. | 8.6 | 230. |
| 24 | .440 | 189. | 9.4 | 175. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.0 | 175. |
| 2 | .420 | 180. | 10.0 | 175. |
| 3 | .420 | 180. | 10.0 | 175. |
| 4 | .430 | 185. | 9.9 | 175. |
| 5 | .440 | 189. | 10.0 | 175. |
| 6 | .440 | 189. | 9.9 | 175. |
| 7 | .440 | 189. | 9.1 | 265. |
| 8 | .600 | 258. | 7.8 | 345. |
| 9 | .510 | 219. | 6.7 | 420. |

| | | | | |
|---|---|---|---|---|
| 10 | .480 | 206. | 6.4 | 420. |
| 11 | .490 | 210. | 6.5 | 420. |
| 12 | .490 | 210. | 6.5 | 420. |
| 13 | .500 | 215. | 6.4 | 420. |
| 14 | .490 | 210. | 6.4 | 420. |
| 15 | .470 | 202. | 6.4 | 420. |
| 16 | .480 | 206. | 6.4 | 415. |
| 17 | .480 | 206. | 6.4 | 418. |
| 18 | .470 | 202. | 6.4 | 415. |
| 19 | .480 | 206. | 6.5 | 350. |
| 20 | .560 | 241. | 7.7 | 320. |
| 21 | .590 | 253. | 7.8 | 320. |
| 22 | .550 | 236. | 8.3 | 250. |
| 23 | .540 | 232. | 9.3 | 225. |
| 24 | .460 | 198. | 9.8 | 175. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.1 | 176. |
| 2 | .380 | 163. | 10.1 | 178. |
| 3 | .390 | 168. | 10.0 | 176. |
| 4 | .400 | 172. | 10.0 | 178. |
| 5 | .400 | 172. | 10.0 | 178. |
| 6 | .480 | 206. | 9.8 | 200. |
| 7 | .590 | 253. | 9.5 | 200. |
| 8 | .620 | 266. | 9.5 | 200. |
| 9 | .560 | 241. | 8.5 | 275. |
| 10 | .590 | 253. | 8.5 | 275. |
| 11 | .590 | 253. | 8.5 | 275. |
| 12 | .540 | 232. | 7.8 | 325. |
| 13 | .530 | 228. | 6.9 | 420. |
| 14 | .530 | 228. | 6.3 | 420. |
| 15 | .530 | 228. | 6.3 | 415. |
| 16 | .530 | 228. | 6.4 | 370. |
| 17 | .490 | 210. | 7.6 | 315. |
| 18 | .520 | 223. | 7.6 | 325. |
| 19 | .430 | 185. | 6.9 | 370. |
| 20 | .420 | 180. | 6.9 | 370. |
| 21 | .440 | 189. | 7.7 | 275. |
| 22 | .440 | 189. | 9.5 | 180. |
| 23 | .420 | 180. | 10.0 | 180. |
| 24 | .410 | 176. | 10.0 | 180. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.0 | 180. |
| 2 | .400 | 172. | 10.0 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .410 | 176. | 9.9 | 180. |
| 5 | .420 | 180. | 10.0 | 180. |
| 6 | .420 | 180. | 10.0 | 178. |
| 7 | .430 | 185. | 10.0 | 178. |
| 8 | .430 | 185. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 9 | .400 | 172. | 9.9 | 230. |
| 10 | .470 | 202. | 9.0 | 230. |
| 11 | .500 | 215. | 9.1 | 230. |
| 12 | .460 | 198. | 9.4 | 180. |
| 13 | .390 | 168. | 9.9 | 180. |
| 14 | .410 | 176. | 10.0 | 180. |
| 15 | .410 | 176. | 10.0 | 180. |
| 16 | .410 | 176. | 10.0 | 165. |
| 17 | .410 | 176. | 10.0 | 185. |
| 18 | .480 | 206. | 9.2 | 275. |
| 19 | .590 | 253. | 8.5 | 275. |
| 20 | .580 | 249. | 8.5 | 275. |
| 21 | .610 | 262. | 9.2 | 225. |
| 22 | .510 | 219. | 10.0 | 175. |
| 23 | .510 | 219. | 10.0 | 175. |
| 24 | .510 | 219. | 10.0 | 175. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 10.0 | 178. |
| 2 | .500 | 215. | 10.0 | 178. |
| 3 | .490 | 210. | 10.0 | 178. |
| 4 | .490 | 210. | 10.0 | 178. |
| 5 | .480 | 206. | 10.0 | 178. |
| 6 | .490 | 210. | 9.9 | 200. |
| 7 | .490 | 210. | 7.4 | 400. |
| 8 | .510 | 219. | 6.5 | 420. |
| 9 | .520 | 223. | 6.5 | 420. |
| 10 | .530 | 228. | 6.4 | 420. |
| 11 | .520 | 223. | 6.3 | 420. |
| 12 | .500 | 215. | 6.3 | 420. |
| 13 | .500 | 215. | 6.3 | 420. |
| 14 | .510 | 219. | 6.3 | 420. |
| 15 | .500 | 215. | 6.4 | 420. |
| 16 | .520 | 223. | 6.4 | 415. |
| 17 | .530 | 228. | 6.4 | 415. |
| 18 | .520 | 223. | 6.4 | 415. |
| 19 | .490 | 210. | 6.4 | 415. |
| 20 | .500 | 215. | 6.5 | 410. |
| 21 | .430 | 185. | 6.9 | 372. |
| 22 | .450 | 193. | 7.0 | 330. |
| 23 | .560 | 241. | 7.9 | 305. |
| 24 | .460 | 198. | 9.2 | 220. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.0 | 180. |
| 2 | .430 | 185. | 10.0 | 178. |
| 3 | .430 | 185. | 10.0 | 178. |
| 4 | .430 | 185. | 10.0 | 178. |
| 5 | .410 | 176. | 10.0 | 178. |
| 6 | .430 | 185. | 10.0 | 178. |
| 7 | .460 | 198. | 8.9 | 288. |

| | | | | |
|---|---|---|---|---|
| 8 | .440 | 189. | 7.2 | 415. |
| 9 | .460 | 198. | 6.5 | 415. |
| 10 | .460 | 198. | 6.5 | 415. |
| 11 | .470 | 202. | 6.5 | 415. |
| 12 | .480 | 206. | 6.5 | 415. |
| 13 | .490 | 210. | 6.5 | 415. |
| 14 | .490 | 210. | 6.5 | 415. |
| 15 | .490 | 210. | 6.5 | 415. |
| 16 | .350 | 150. | 7.6 | 315. |
| 17 | .380 | 163. | 7.5 | 360. |
| 18 | .400 | 172. | 7.1 | 375. |
| 19 | .470 | 202. | 6.6 | 412. |
| 20 | .480 | 206. | 6.5 | 412. |
| 21 | .490 | 210. | 6.6 | 412. |
| 22 | .500 | 215. | 6.6 | 412. |
| 23 | .400 | 172. | 7.7 | 275. |
| 24 | .500 | 215. | 9.8 | 180. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.1 | 178. |
| 2 | .470 | 202. | 10.1 | 178. |
| 3 | .470 | 202. | 10.1 | 178. |
| 4 | .470 | 202. | 10.1 | 178. |
| 5 | .480 | 206. | 10.1 | 178. |
| 6 | .500 | 215. | 9.5 | 265. |
| 7 | .480 | 206. | 7.1 | 412. |
| 8 | .510 | 219. | 6.5 | 412. |
| 9 | .510 | 219. | 6.5 | 412. |
| 10 | .510 | 219. | 6.6 | 412. |
| 11 | .560 | 241. | 6.6 | 412. |
| 12 | .590 | 253. | 6.6 | 412. |
| 13 | .580 | 249. | 6.6 | 412. |
| 14 | .580 | 249. | 6.6 | 412. |
| 15 | .560 | 241. | 6.6 | 412. |
| 16 | .560 | 241. | 6.6 | 415. |
| 17 | .580 | 249. | 6.7 | 415. |
| 18 | .580 | 249. | 6.7 | 415. |
| 19 | .570 | 245. | 6.6 | 415. |
| 20 | .560 | 241. | 6.7 | 415. |
| 21 | .560 | 241. | 6.7 | 415. |
| 22 | .560 | 241. | 6.7 | 400. |
| 23 | .500 | 215. | 7.5 | 300. |
| 24 | .440 | 189. | 9.8 | 200. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 10.1 | 178. |
| 2 | .440 | 189. | 10.1 | 178. |
| 3 | .420 | 180. | 10.1 | 178. |
| 4 | .430 | 185. | 10.1 | 178. |
| 5 | .440 | 189. | 10.1 | 178. |
| 6 | .440 | 189. | 9.8 | 220. |

| | | | | |
|---|---|---|---|---|
| 7 | .560 | 241. | 7.6 | 358. |
| 8 | .590 | 253. | 7.3 | 358. |
| 9 | .440 | 189. | 5.8 | 520. |
| 10 | .380 | 163. | 5.2 | 520. |
| 11 | .370 | 159. | 5.2 | 520. |
| 12 | .360 | 155. | 5.1 | 520. |
| 13 | .380 | 163. | 5.1 | 520. |
| 14 | .380 | 163. | 5.1 | 520. |
| 15 | .410 | 176. | 5.0 | 520. |
| 16 | .470 | 202. | 5.4 | 515. |
| 17 | .420 | 180. | 5.0 | 515. |
| 18 | .410 | 176. | 5.1 | 515. |
| 19 | .400 | 172. | 5.1 | 515. |
| 20 | .400 | 172. | 5.1 | 515. |
| 21 | .410 | 176. | 5.2 | 430. |
| 22 | .450 | 193. | 6.6 | 300. |
| 23 | .420 | 180. | 8.2 | 280. |
| 24 | .410 | 176. | 8.8 | 260. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 10.0 | 178. |
| 2 | .450 | 193. | 10.1 | 178. |
| 3 | .460 | 198. | 10.1 | 175. |
| 4 | .450 | 193. | 10.1 | 178. |
| 5 | .460 | 198. | 10.0 | 178. |
| 6 | .530 | 228. | 9.1 | 250. |
| 7 | .500 | 215. | 7.0 | 458. |
| 8 | .460 | 198. | 5.2 | 525. |
| 9 | .490 | 210. | 5.1 | 527. |
| 10 | .480 | 206. | 5.2 | 528. |
| 11 | .500 | 215. | 5.2 | 525. |
| 12 | .510 | 219. | 5.2 | 525. |
| 13 | .510 | 219. | 5.2 | 525. |
| 14 | .510 | 219. | 5.2 | 525. |
| 15 | .520 | 223. | 5.1 | 525. |
| 16 | .480 | 206. | 5.0 | 530. |
| 17 | .450 | 193. | 5.1 | 530. |
| 18 | .460 | 198. | 5.2 | 530. |
| 19 | .480 | 206. | 5.1 | 530. |
| 20 | .490 | 210. | 5.1 | 530. |
| 21 | .480 | 206. | 5.1 | 537. |
| 22 | .470 | 202. | 5.3 | 470. |
| 23 | .570 | 245. | 6.3 | 430. |
| 24 | .510 | 219. | 8.1 | 260. |

DAY = 32

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 9.9 | 178. |
| 2 | .440 | 189. | 10.1 | 178. |
| 3 | .450 | 193. | 10.1 | 175. |
| 4 | .460 | 198. | 10.1 | 178. |
| 5 | .460 | 198. | 10.1 | 178. |

| | | | | |
|---|---|---|---|---|
| 6 | .450 | 193. | 10.1 | 250. |
| 7 | .470 | 202. | 9.0 | 458. |
| 8 | .550 | 236. | 7.6 | 525. |
| 9 | .590 | 253. | 7.6 | 527. |
| 10 | .640 | 275. | 7.2 | 528. |
| 11 | .660 | 284. | 7.1 | 525. |
| 12 | .660 | 284. | 7.1 | 525. |
| 13 | .590 | 253. | 7.6 | 525. |
| 14 | .470 | 202. | 8.3 | 525. |
| 15 | .420 | 180. | 8.6 | 525. |
| 16 | .430 | 185. | 8.6 | 530. |
| 17 | .450 | 193. | 8.6 | 530. |
| 18 | .500 | 215. | 8.0 | 530. |
| 19 | .430 | 185. | 6.5 | 530. |
| 20 | .430 | 185. | 6.6 | 530. |
| 21 | .470 | 202. | 6.9 | 537. |
| 22 | .520 | 223. | 7.5 | 470. |
| 23 | .510 | 219. | 7.4 | 430. |
| 24 | .480 | 206. | 8.6 | 260. |

DAY = 33

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 9.7 | 185. |
| 2 | .480 | 206. | 8.8 | 295. |
| 3 | .640 | 275. | 7.9 | 330. |
| 4 | .590 | 253. | 7.5 | 330. |
| 5 | .610 | 262. | 7.6 | 330. |
| 6 | .590 | 253. | 7.6 | 330. |
| 7 | .500 | 215. | 7.2 | 400. |
| 8 | .550 | 236. | 6.5 | 425. |
| 9 | .520 | 223. | 6.0 | 500. |
| 10 | .460 | 198. | 5.6 | 500. |
| 11 | .440 | 189. | 5.2 | 525. |
| 12 | .470 | 202. | 5.2 | 525. |
| 13 | .490 | 210. | 5.1 | 525. |
| 14 | .470 | 202. | 5.2 | 525. |
| 15 | .480 | 206. | 5.2 | 525. |
| 16 | .490 | 210. | 5.2 | 525. |
| 17 | .470 | 202. | 5.1 | 525. |
| 18 | .460 | 198. | 5.1 | 525. |
| 19 | .430 | 185. | 5.2 | 527. |
| 20 | .450 | 193. | 5.1 | 527. |
| 21 | .460 | 198. | 5.1 | 527. |
| 22 | .470 | 202. | 5.2 | 480. |
| 23 | .520 | 223. | 5.8 | 475. |
| 24 | .490 | 210. | 7.3 | 450. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 8.0 | 300. |
| 2 | .440 | 189. | 8.0 | 300. |
| 3 | .450 | 193. | 8.0 | 300. |
| 4 | .450 | 193. | 8.1 | 300. |

| | | | | |
|---|---|---|---|---|
| 5 | .460 | 198. | 8.0 | 300. |
| 6 | .460 | 198. | 7.8 | 350. |
| 7 | .440 | 189. | 5.6 | 520. |
| 8 | .450 | 193. | 5.0 | 520. |
| 9 | .450 | 193. | 5.0 | 530. |
| 10 | .450 | 193. | 5.0 | 520. |
| 11 | .430 | 185. | 5.1 | 525. |
| 12 | .500 | 215. | 5.3 | 520. |
| 13 | .500 | 215. | 5.4 | 528. |
| 14 | .520 | 223. | 5.5 | 525. |
| 15 | .550 | 236. | 5.4 | 525. |
| 16 | .550 | 236. | 5.3 | 525. |
| 17 | .530 | 228. | 5.1 | 525. |
| 18 | .540 | 232. | 5.1 | 525. |
| 19 | .510 | 219. | 5.1 | 525. |
| 20 | .520 | 223. | 5.1 | 530. |
| 21 | .440 | 189. | 5.2 | 530. |
| 22 | .410 | 176. | 5.2 | 530. |
| 23 | .420 | 180. | 5.2 | 525. |
| 24 | .510 | 219. | 5.8 | 410. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 7.1 | 380. |
| 2 | .620 | 266. | 7.1 | 380. |
| 3 | .570 | 245. | 7.2 | 305. |
| 4 | .420 | 180. | 8.5 | 255. |
| 5 | .450 | 193. | 8.9 | 255. |
| 6 | .460 | 198. | 7.9 | 480. |
| 7 | .430 | 185. | 5.3 | 520. |
| 8 | .480 | 206. | 5.2 | 520. |
| 9 | .490 | 210. | 5.2 | 520. |
| 10 | .530 | 228. | 5.5 | 520. |
| 11 | .540 | 232. | 5.4 | 520. |
| 12 | .500 | 215. | 5.4 | 520. |
| 13 | .510 | 219. | 5.3 | 520. |
| 14 | .530 | 228. | 5.2 | 520. |
| 15 | .540 | 232. | 5.2 | 525. |
| 16 | .530 | 228. | 5.2 | 520. |
| 17 | .470 | 202. | 5.2 | 525. |
| 18 | .460 | 198. | 5.2 | 520. |
| 19 | .480 | 206. | 5.2 | 520. |
| 20 | .500 | 215. | 5.2 | 520. |
| 21 | .470 | 202. | 5.2 | 520. |
| 22 | .470 | 202. | 5.2 | 520. |
| 23 | .480 | 206. | 5.2 | 520. |
| 24 | .500 | 215. | 5.2 | 520. |

DAY = 36

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 5.2 | 485. |
| 2 | .490 | 210. | 5.9 | 475. |
| 3 | .500 | 215. | 5.9 | 475. |

| | | | | |
|---|---|---|---|---|
| 4 | .510 | 219. | 5.9 | 475. |
| 5 | .540 | 232. | 5.9 | 475. |
| 6 | .480 | 206. | 5.4 | 518. |
| 7 | .450 | 193. | 5.3 | 518. |
| 8 | .460 | 198. | 5.3 | 520. |
| 9 | .470 | 202. | 5.3 | 520. |
| 10 | .470 | 202. | 5.3 | 520. |
| 11 | .440 | 189. | 5.3 | 520. |
| 12 | .500 | 215. | 6.1 | 430. |
| 13 | .540 | 232. | 6.4 | 430. |
| 14 | .540 | 232. | 6.4 | 430. |
| 15 | .550 | 236. | 6.4 | 430. |
| 16 | .560 | 241. | 6.3 | 428. |
| 17 | .560 | 241. | 6.4 | 428. |
| 18 | .490 | 210. | 6.0 | 492. |
| 19 | .440 | 189. | 5.4 | 510. |
| 20 | .450 | 193. | 5.4 | 510. |
| 21 | .460 | 198. | 5.4 | 510. |
| 22 | .470 | 202. | 5.5 | 510. |
| 23 | .470 | 202. | 5.5 | 510. |
| 24 | .480 | 206. | 5.5 | 510. |

DAY = 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 6.0 | 460. |
| 2 | .540 | 232. | 6.1 | 460. |
| 3 | .560 | 241. | 6.1 | 460. |
| 4 | .580 | 249. | 6.1 | 460. |
| 5 | .570 | 245. | 6.0 | 460. |
| 6 | .500 | 215. | 5.5 | 510. |
| 7 | .490 | 210. | 5.4 | 510. |
| 8 | .470 | 202. | 5.4 | 515. |
| 9 | .490 | 210. | 5.3 | 515. |
| 10 | .520 | 223. | 5.2 | 520. |
| 11 | .440 | 189. | 5.3 | 520. |
| 12 | .450 | 193. | 5.3 | 520. |
| 13 | .480 | 206. | 5.2 | 520. |
| 14 | .500 | 215. | 5.1 | 520. |
| 15 | .490 | 210. | 5.1 | 520. |
| 16 | .500 | 215. | 5.1 | 520. |
| 17 | .480 | 206. | 5.1 | 520. |
| 18 | .420 | 180. | 5.2 | 520. |
| 19 | .430 | 185. | 5.2 | 518. |
| 20 | .440 | 189. | 5.1 | 515. |
| 21 | .440 | 189. | 5.1 | 515. |
| 22 | .430 | 185. | 5.2 | 520. |
| 23 | .430 | 185. | 5.3 | 520. |
| 24 | .440 | 189. | 5.2 | 518. |

DAY = 38

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 5.2 | 510. |
| 2 | .440 | 189. | 5.3 | 510. |

| | | | | |
|---|---|---|---|---|
| 3 | .450 | 193. | 5.3 | 510. |
| 4 | .460 | 198. | 5.3 | 510. |
| 5 | .470 | 202. | 5.3 | 510. |
| 6 | .450 | 193. | 5.3 | 510. |
| 7 | .430 | 185. | 5.3 | 510. |
| 8 | .440 | 189. | 5.3 | 510. |
| 9 | .450 | 193. | 5.3 | 505. |
| 10 | .450 | 193. | 5.3 | 505. |
| 11 | .460 | 198. | 5.3 | 505. |
| 12 | .470 | 202. | 5.3 | 505. |
| 13 | .510 | 219. | 5.3 | 505. |
| 14 | .510 | 219. | 5.3 | 505. |
| 15 | .530 | 228. | 5.3 | 505. |
| 16 | .530 | 228. | 5.2 | 505. |
| 17 | .490 | 210. | 5.2 | 512. |
| 18 | .450 | 193. | 5.5 | 505. |
| 19 | .470 | 202. | 5.4 | 505. |
| 20 | .480 | 206. | 5.4 | 505. |
| 21 | .470 | 202. | 5.4 | 508. |
| 22 | .470 | 202. | 5.5 | 505. |
| 23 | .480 | 206. | 5.4 | 502. |
| 24 | .480 | 206. | 5.4 | 500. |

DAY = 39

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 5.7 | 430. |
| 2 | .590 | 253. | 6.3 | 430. |
| 3 | .590 | 253. | 6.3 | 430. |
| 4 | .560 | 241. | 6.3 | 440. |
| 5 | .570 | 245. | 6.3 | 435. |
| 6 | .580 | 249. | 6.3 | 435. |
| 7 | .500 | 215. | 5.5 | 510. |
| 8 | .520 | 223. | 5.4 | 510. |
| 9 | .450 | 193. | 5.6 | 510. |
| 10 | .390 | 168. | 5.5 | 510. |
| 11 | .420 | 180. | 5.4 | 510. |
| 12 | .440 | 189. | 5.4 | 510. |
| 13 | .410 | 176. | 5.4 | 510. |
| 14 | .430 | 185. | 5.4 | 510. |
| 15 | .460 | 198. | 5.4 | 510. |
| 16 | .470 | 202. | 5.4 | 508. |
| 17 | .460 | 198. | 5.4 | 507. |
| 18 | .470 | 202. | 6.1 | 430. |
| 19 | .470 | 202. | 6.4 | 430. |
| 20 | .500 | 215. | 6.4 | 430. |
| 21 | .510 | 219. | 6.3 | 430. |
| 22 | .490 | 210. | 6.4 | 430. |
| 23 | .510 | 219. | 6.7 | 373. |
| 24 | .580 | 249. | 7.6 | 330. |

DAY = 40

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 7.9 | 280. |

| | | | | |
|---|---|---|---|---|
| 2 | .410 | 242. | 9.3 | 210. |
| 3 | .500 | 215. | 10.1 | 180. |
| 4 | .520 | 223. | 10.1 | 180. |
| 5 | .530 | 228. | 10.1 | 180. |
| 6 | .530 | 228. | 10.1 | 180. |
| 7 | .530 | 228. | 10.1 | 180. |
| 8 | .540 | 232. | 10.1 | 220. |
| 9 | .570 | 245. | 7.8 | 390. |
| 10 | .410 | 176. | 5.9 | 515. |
| 11 | .350 | 150. | 5.3 | 510. |
| 12 | .380 | 163. | 5.2 | 515. |
| 13 | .380 | 163. | 5.3 | 515. |
| 14 | .400 | 172. | 5.3 | 515. |
| 15 | .410 | 176. | 5.2 | 515. |
| 16 | .420 | 180. | 5.2 | 515. |
| 17 | .420 | 180. | 5.2 | 515. |
| 18 | .410 | 176. | 5.3 | 512. |
| 19 | .400 | 172. | 5.3 | 510. |
| 20 | .410 | 176. | 5.3 | 510. |
| 21 | .460 | 198. | 5.3 | 510. |
| 22 | .460 | 198. | 5.6 | 510. |
| 23 | .460 | 198. | 5.6 | 450. |
| 24 | .530 | 228. | 8.8 | 180. |

DAY = 41

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 10.1 | 175. |
| 2 | .370 | 159. | 10.1 | 175. |
| 3 | .370 | 159. | 10.1 | 175. |
| 4 | .370 | 159. | 10.1 | 175. |
| 5 | .420 | 180. | 10.0 | 210. |
| 6 | .400 | 172. | 8.0 | 380. |
| 7 | .390 | 168. | 5.8 | 500. |
| 8 | .410 | 176. | 5.5 | 510. |
| 9 | .400 | 172. | 5.3 | 510. |
| 10 | .420 | 180. | 5.3 | 510. |
| 11 | .430 | 185. | 5.3 | 510. |
| 12 | .450 | 193. | 5.3 | 510. |
| 13 | .460 | 198. | 5.3 | 510. |
| 14 | .470 | 202. | 5.3 | 510. |
| 15 | .490 | 210. | 5.3 | 510. |
| 16 | .500 | 215. | 5.3 | 510. |
| 17 | .480 | 206. | 5.2 | 515. |
| 18 | .430 | 185. | 5.0 | 515. |
| 19 | .450 | 193. | 5.3 | 515. |
| 20 | .420 | 180. | 5.3 | 510. |
| 21 | .460 | 198. | 5.3 | 510. |
| 22 | .500 | 215. | 5.3 | 510. |
| 23 | .560 | 241. | 5.3 | 515. |
| 24 | .600 | 258. | 5.6 | 460. |

DAY = 42

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .590 | 253. | 7.5 | 290. |
| 2 | .550 | 236. | 8.5 | 290. |
| 3 | .560 | 241. | 8.3 | 290. |
| 4 | .570 | 245. | 8.3 | 290. |
| 5 | .600 | 258. | 7.8 | 350. |
| 6 | .550 | 236. | 6.4 | 490. |
| 7 | .550 | 236. | 5.5 | 500. |
| 8 | .550 | 236. | 5.5 | 515. |
| 9 | .500 | 215. | 5.3 | 520. |
| 10 | .520 | 223. | 5.3 | 520. |
| 11 | .520 | 223. | 5.3 | 525. |
| 12 | .530 | 228. | 5.3 | 525. |
| 13 | .550 | 236. | 5.2 | 525. |
| 14 | .540 | 232. | 5.2 | 525. |
| 15 | .540 | 232. | 5.3 | 525. |
| 16 | .550 | 236. | 5.2 | 525. |
| 17 | .550 | 236. | 5.2 | 525. |
| 18 | .500 | 215. | 5.2 | 525. |
| 19 | .500 | 215. | 5.2 | 525. |
| 20 | .520 | 223. | 5.2 | 525. |
| 21 | .520 | 223. | 5.2 | 525. |
| 22 | .520 | 223. | 5.2 | 525. |
| 23 | .540 | 232. | 5.2 | 525. |
| 24 | .570 | 245. | 5.6 | 400. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 6.8 | 390. |
| 2 | .600 | 258. | 6.9 | 390. |
| 3 | .580 | 249. | 6.6 | 430. |
| 4 | .550 | 236. | 6.2 | 445. |
| 5 | .570 | 245. | 6.1 | 470. |
| 6 | .540 | 232. | 5.7 | 510. |
| 7 | .550 | 236 | 5.3 | 515. |
| 8 | .550 | 236. | 5.2 | 515. |
| 9 | .530 | 228. | 5.3 | 515. |
| 10 | .510 | 219. | 5.3 | 515. |
| 11 | .510 | 219. | 5.3 | 520. |
| 12 | .500 | 215. | 5.2 | 520. |
| 13 | .500 | 215. | 5.3 | 520. |
| 14 | .500 | 215. | 5.2 | 520. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .500 | 215. | 5.2 | 523. |
| 17 | .530 | 228. | 5.4 | 505. |
| 18 | .520 | 223. | 5.4 | 505. |
| 19 | .510 | 219. | 5.5 | 505. |
| 20 | .520 | 223. | 5.4 | 505. |
| 21 | .530 | 228. | 5.4 | 505. |
| 22 | .530 | 228. | 5.4 | 505. |
| 23 | .500 | 215. | 5.5 | 505. |
| 24 | .520 | 223. | 5.4 | 505. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .580 | 249. | 5.9 | 420. |
| 2 | .550 | 236. | 5.8 | 500. |
| 3 | .520 | 223. | 5.5 | 505. |
| 4 | .510 | 219. | 5.5 | 505. |
| 5 | .470 | 202. | 5.5 | 505. |
| 6 | .480 | 206. | 5.4 | 505. |
| 7 | .470 | 202. | 5.4 | 500. |
| 8 | .460 | 198. | 5.4 | 500. |
| 9 | .490 | 210. | 5.4 | 500. |
| 10 | .430 | 185. | 5.5 | 505. |
| 11 | .430 | 185. | 5.5 | 505. |
| 12 | .430 | 185. | 5.4 | 500. |
| 13 | .470 | 202. | 5.4 | 500. |
| 14 | .460 | 198. | 5.4 | 505. |
| 15 | .450 | 193. | 5.5 | 505. |
| 16 | .460 | 198. | 5.5 | 500. |
| 17 | .470 | 202. | 5.5 | 500. |
| 18 | .450 | 193. | 5.5 | 500. |
| 19 | .460 | 198. | 5.5 | 500. |
| 20 | .460 | 198. | 5.5 | 500. |
| 21 | .470 | 202. | 5.4 | 500. |
| 22 | .470 | 202. | 5.5 | 500. |
| 23 | .450 | 193. | 5.5 | 500. |
| 24 | .460 | 198. | 5.5 | 500. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 6.4 | 380. |
| 2 | .500 | 215. | 7.1 | 340. |
| 3 | .440 | 189. | 8.5 | 275. |
| 4 | .440 | 189. | 8.7 | 275. |
| 5 | .440 | 189. | 8.7 | 275. |
| 6 | .520 | 223. | 7.4 | 375. |
| 7 | .530 | 228. | 6.1 | 500. |
| 8 | .530 | 228. | 5.5 | 502. |
| 9 | .500 | 215. | 5.6 | 502. |
| 10 | .490 | 210. | 5.5 | 500. |
| 11 | .500 | 215. | 5.4 | 504. |
| 12 | .490 | 210. | 5.5 | 500. |
| 13 | .490 | 210. | 5.5 | 500. |
| 14 | .470 | 202. | 5.5 | 500. |
| 15 | .470 | 202. | 5.4 | 500. |
| 16 | .480 | 206. | 5.4 | 500. |
| 17 | .500 | 215. | 5.4 | 500. |
| 18 | .500 | 215. | 5.4 | 500. |
| 19 | .470 | 202. | 5.4 | 500. |
| 20 | .480 | 206. | 5.4 | 500. |
| 21 | .500 | 215. | 5.4 | 500. |
| 22 | .510 | 219. | 5.5 | 500. |
| 23 | .500 | 215. | 5.9 | 440. |
| 24 | .560 | 241. | 7.3 | 320. |

DAY = 46

| NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 7.6 | 320. |
| 2 | .540 | 232. | 7.8 | 265. |
| 3 | .490 | 210. | 9.8 | 170. |
| 4 | .420 | 180. | 10.1 | 170. |
| 5 | .420 | 180. | 10.1 | 170. |
| 6 | .490 | 210. | 9.8 | 250. |
| 7 | .560 | 241. | 8.1 | 300. |
| 8 | .560 | 241. | 7.4 | 400. |
| 9 | .450 | 193. | 5.7 | 500. |
| 10 | .440 | 189. | 5.4 | 500. |
| 11 | .450 | 193. | 5.4 | 500. |
| 12 | .450 | 193. | 5.4 | 500. |
| 13 | .440 | 189. | 5.4 | 500. |
| 14 | .440 | 189. | 5.4 | 508. |
| 15 | .430 | 185. | 5.4 | 508. |
| 16 | .460 | 198. | 5.4 | 508. |
| 17 | .480 | 206. | 5.5 | 500. |
| 18 | .510 | 219. | 5.5 | 500. |
| 19 | .530 | 228. | 5.5 | 500. |
| 20 | .520 | 223. | 5.5 | 500. |
| 21 | .490 | 210. | 5.6 | 496. |
| 22 | .500 | 215. | 5.5 | 500. |
| 23 | .510 | 219. | 5.5 | 499. |
| 24 | .520 | 223. | 5.7 | 425. |

DAY = 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 6.4 | 425. |
| 2 | .550 | 236. | 6.4 | 425. |
| 3 | .560 | 241. | 6.4 | 425. |
| 4 | .580 | 249. | 6.3 | 425. |
| 5 | .580 | 249. | 6.4 | 425. |
| 6 | .560 | 241. | 6.4 | 425. |
| 7 | .450 | 193. | 6.7 | 370. |
| 8 | .480 | 206. | 6.4 | 475. |
| 9 | .470 | 202. | 5.7 | 475. |
| 10 | .450 | 193. | 5.7 | 475. |
| 11 | .510 | 219. | 6.2 | 475. |
| 12 | .390 | 168. | 6.7 | 380. |
| 13 | .430 | 185. | 6.7 | 380. |
| 14 | .460 | 198. | 6.8 | 330. |
| 15 | .570 | 245. | 7.3 | 330. |
| 16 | .570 | 245. | 7.4 | 330. |
| 17 | .570 | 245. | 7.4 | 330. |
| 18 | .480 | 206. | 7.0 | 380. |
| 19 | .460 | 198. | 6.9 | 380. |
| 20 | .470 | 202. | 6.9 | 380. |
| 21 | .460 | 198. | 6.8 | 380. |
| 22 | .460 | 198. | 6.8 | 380. |
| 23 | .470 | 202. | 6.9 | 380. |
| 24 | .510 | 219. | 8.3 | 240. |

DAY = 48

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 9.9 | 180. |
| 2 | .380 | 163. | 9.9 | 180. |
| 3 | .380 | 163. | 9.8 | 180. |
| 4 | .370 | 159. | 9.8 | 180. |
| 5 | .390 | 168. | 9.5 | 265. |
| 6 | .430 | 185. | 6.6 | 475. |
| 7 | .360 | 155. | 5.2 | 515. |
| 8 | .370 | 159. | 5.1 | 508. |
| 9 | .390 | 168. | 5.4 | 450. |
| 10 | .430 | 185. | 5.9 | 450. |
| 11 | .420 | 180. | 5.7 | 500. |
| 12 | .400 | 172. | 5.1 | 500. |
| 13 | .420 | 180. | 5.1 | 500. |
| 14 | .420 | 180. | 5.1 | 500. |
| 15 | .420 | 180. | 5.1 | 500. |
| 16 | .450 | 193. | 5.1 | 500. |
| 17 | .450 | 193. | 5.3 | 500. |
| 18 | .430 | 185. | 5.4 | 500. |
| 19 | .440 | 189. | 5.4 | 500. |
| 20 | .470 | 202. | 5.3 | 500. |
| 21 | .480 | 206. | 5.3 | 500. |
| 22 | .500 | 215. | 5.3 | 500. |
| 23 | .510 | 219. | 5.3 | 500. |
| 24 | .510 | 219. | 5.2 | 500. |

DAY = 49



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.2 | 500. |
| 2 | .500 | 215. | 5.3 | 500. |
| 3 | .460 | 198. | 5.5 | 500. |
| 4 | .430 | 185. | 5.4 | 500. |
| 5 | .440 | 189. | 5.3 | 500. |
| 6 | .450 | 193. | 5.4 | 500. |
| 7 | -1.000 | -430. | -1.0 | -1. |
| 8 | .470 | 202. | 5.9 | 500. |
| 9 | .460 | 198. | 5.5 | 500. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .210 | 90. | 10.1 | 100. |
| 12 | .390 | 168. | 10.0 | 180. |
| 13 | .500 | 215. | 9.1 | 205. |
| 14 | .560 | 241. | 7.8 | 335. |
| 15 | .580 | 249. | 7.5 | 335. |
| 16 | .590 | 253. | 7.5 | 335. |
| 17 | .540 | 232. | 7.3 | 408. |
| 18 | .570 | 245. | 6.4 | 450. |
| 19 | .560 | 241. | 6.2 | 450. |
| 20 | .520 | 223. | 6.3 | 450. |
| 21 | .500 | 215. | 6.3 | 450. |
| 22 | .510 | 219. | 6.2 | 450. |
| 23 | .500 | 215. | 6.2 | 450. |
| 24 | .500 | 215. | 6.2 | 450. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 6.2 | 450. |
| 2 | .500 | 215. | 6.2 | 465. |
| 3 | .460 | 198. | 6.2 | 460. |
| 4 | .470 | 202. | 6.2 | 460. |
| 5 | .470 | 202. | 6.2 | 460. |
| 6 | .470 | 202. | 6.2 | 460. |
| 7 | .470 | 202. | 6.2 | 460. |
| 8 | .480 | 206. | 6.2 | 460. |
| 9 | .490 | 210. | 6.0 | 490. |
| 10 | .460 | 198. | 5.7 | 495. |
| 11 | .450 | 193. | 5.7 | 500. |
| 12 | .490 | 210. | 5.6 | 500. |
| 13 | .510 | 219. | 5.6 | 500. |
| 14 | .490 | 210. | 5.6 | 500. |
| 15 | .490 | 210. | 5.6 | 500. |
| 16 | .490 | 210. | 5.6 | 500. |
| 17 | .510 | 219. | 5.6 | 500. |
| 18 | .510 | 219. | 5.6 | 500. |
| 19 | .520 | 223. | 5.5 | 500. |
| 20 | .510 | 219. | 5.6 | 500. |
| 21 | .470 | 202. | 5.7 | 500. |
| 22 | .470 | 202. | 5.7 | 500. |
| 23 | .500 | 215. | 5.6 | 500. |
| 24 | .530 | 228. | 5.6 | 500. |

DAY = 51



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 5.6 | 500. |
| 2 | .500 | 215. | 5.6 | 500. |
| 3 | .470 | 202. | 5.7 | 500. |
| 4 | .500 | 215. | 5.6 | 500. |
| 5 | .470 | 202. | 5.5 | 500. |
| 6 | .400 | 172. | 5.6 | 500. |
| 7 | .440 | 189. | 5.6 | 500. |
| 8 | .450 | 193. | 5.5 | 500. |
| 9 | .450 | 193. | 5.5 | 500. |
| 10 | .430 | 185. | 5.5 | 500. |
| 11 | .410 | 176. | 5.5 | 500. |
| 12 | .410 | 176. | 5.5 | 500. |
| 13 | .420 | 180. | 5.5 | 500. |
| 14 | .420 | 180. | 5.5 | 492. |
| 15 | .430 | 185. | 5.5 | 498. |
| 16 | .440 | 189. | 5.5 | 495. |
| 17 | .460 | 198. | 5.4 | 495. |
| 18 | .480 | 206. | 5.4 | 495. |
| 19 | .460 | 198. | 5.5 | 500. |
| 20 | .400 | 172. | 5.5 | 500. |
| 21 | .410 | 176. | 5.5 | 498. |
| 22 | .420 | 180. | 5.5 | 495. |
| 23 | .450 | 193. | 5.5 | 495. |
| 24 | .460 | 198. | 5.5 | 495. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 5.5 | 495. |
| 2 | .450 | 193. | 5.7 | 480. |
| 3 | .430 | 185. | 5.8 | 480. |
| 4 | .470 | 202. | 6.1 | 450. |
| 5 | .480 | 206. | 6.1 | 450. |
| 6 | .410 | 176. | 5.7 | 495. |
| 7 | .410 | 176. | 5.6 | 495. |
| 8 | .420 | 180. | 5.6 | 485. |
| 9 | .430 | 185. | 5.6 | 485. |
| 10 | .430 | 185. | 5.6 | 485. |
| 11 | .450 | 193. | 5.1 | 490. |
| 12 | .420 | 180. | 5.4 | 485. |
| 13 | .430 | 185. | 5.5 | 485. |
| 14 | .420 | 180. | 5.5 | 485. |
| 15 | .420 | 180. | 5.5 | 488. |
| 16 | .420 | 180. | 5.6 | 485. |
| 17 | .440 | 189. | 5.5 | 490. |
| 18 | .450 | 193. | 5.5 | 490. |
| 19 | .470 | 202. | 5.5 | 490. |
| 20 | .440 | 189. | 5.5 | 490. |
| 21 | .410 | 176. | 5.6 | 485. |
| 22 | .430 | 185. | 5.6 | 485. |
| 23 | .470 | 202. | 5.6 | 490. |
| 24 | .470 | 202. | 5.6 | 488. |

DAY = 53

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .490 | 210. | 5.6 | 488. |
| 2 | .480 | 206. | 5.6 | 480. |
| 3 | .420 | 180. | 5.6 | 485. |
| 4 | .410 | 176. | 5.6 | 485. |
| 5 | .420 | 180. | 5.6 | 485. |
| 6 | .440 | 189. | 5.5 | 488. |
| 7 | .440 | 189. | 5.4 | 490. |
| 8 | .400 | 172. | 5.6 | 490. |
| 9 | .410 | 176. | 5.5 | 490. |
| 10 | .420 | 180. | 5.5 | 488. |
| 11 | .420 | 180. | 5.5 | 493. |
| 12 | .420 | 180. | 5.5 | 491. |
| 13 | .420 | 180. | 5.5 | 488. |
| 14 | .430 | 185. | 5.5 | 491. |
| 15 | .410 | 176. | 5.5 | 493. |
| 16 | .410 | 176. | 5.5 | 490. |
| 17 | .430 | 185. | 5.5 | 485. |
| 18 | .440 | 189. | 5.5 | 490. |
| 19 | .440 | 189. | 5.5 | 490. |
| 20 | .430 | 185. | 5.5 | 490. |
| 21 | .410 | 176. | 5.5 | 490. |
| 22 | .440 | 189. | 5.5 | 490. |
| 23 | .450 | 193. | 5.5 | 490. |
| 24 | .430 | 185. | 5.6 | 490. |

DAY = 54

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 5.6 | 450. |
| 2 | .480 | 206. | 7.1 | 295. |
| 3 | .490 | 210. | 7.8 | 300. |
| 4 | .490 | 210. | 7.8 | 300. |
| 5 | .470 | 202. | 7.7 | 300. |
| 6 | .480 | 206. | 7.7 | 300. |
| 7 | .440 | 189. | 7.1 | 345. |
| 8 | .440 | 189. | 7.0 | 325. |
| 9 | .410 | 176. | 6.0 | 480. |
| 10 | .420 | 180. | 5.6 | 480. |
| 11 | .440 | 189. | 5.6 | 480. |
| 12 | .450 | 193. | 5.8 | 430. |
| 13 | .440 | 189. | 6.2 | 430. |
| 14 | .460 | 198. | 6.2 | 430. |
| 15 | .450 | 193. | 6.3 | 430. |
| 16 | .480 | 206. | 5.9 | 475. |
| 17 | .500 | 215. | 5.6 | 475. |
| 18 | .500 | 215. | 5.6 | 475. |
| 19 | .490 | 210. | 5.5 | 480. |
| 20 | .510 | 219. | 5.5 | 480. |
| 21 | .500 | 215. | 5.6 | 480. |
| 22 | .450 | 193. | 5.6 | 480. |
| 23 | .460 | 198. | 5.5 | 480. |
| 24 | .500 | 215. | 5.9 | 430. |

DAY = 55

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 7.0 | 330. |
| 2 | .420 | 180. | 8.1 | 272. |
| 3 | .400 | 172. | 8.3 | 270. |
| 4 | .400 | 172. | 8.4 | 270. |
| 5 | .410 | 176. | 8.4 | 270. |
| 6 | .430 | 185. | 7.8 | 360. |
| 7 | .450 | 193. | 5.8 | 490. |
| 8 | .440 | 189. | 5.4 | 495. |
| 9 | .450 | 193. | 5.4 | 495. |
| 10 | .480 | 206. | 5.5 | 495. |
| 11 | .490 | 210. | 5.6 | 495. |
| 12 | .500 | 215. | 5.6 | 495. |
| 13 | .500 | 215. | 5.5 | 495. |
| 14 | .500 | 215. | 5.6 | 495. |
| 15 | .490 | 210. | 5.6 | 495. |
| 16 | .490 | 210. | 5.6 | 490. |
| 17 | .500 | 215. | 5.5 | 490. |
| 18 | .520 | 223. | 5.5 | 490. |
| 19 | .490 | 210. | 5.5 | 495. |
| 20 | .480 | 206. | 5.6 | 495. |
| 21 | .490 | 210. | 5.6 | 490. |
| 22 | .500 | 215. | 5.5 | 490. |
| 23 | .500 | 215. | 5.5 | 495. |
| 24 | .490 | 210. | 5.6 | 495. |

DAY = 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.6 | 490. |
| 2 | .520 | 223. | 5.5 | 490. |
| 3 | .480 | 206. | 5.6 | 495. |
| 4 | .440 | 189. | 5.7 | 490. |
| 5 | .450 | 193. | 5.7 | 490. |
| 6 | .400 | 172. | 5.7 | 480. |
| 7 | .490 | 210. | 6.2 | 438. |
| 8 | .500 | 215. | 6.3 | 443. |
| 9 | .510 | 219. | 6.3 | 443. |
| 10 | .600 | 258. | 6.3 | 430. |
| 11 | .590 | 253. | 6.3 | 435. |
| 12 | .520 | 223. | 6.3 | 439. |
| 13 | .480 | 206. | 5.9 | 480. |
| 14 | .470 | 202. | 5.8 | 480. |
| 15 | .480 | 206. | 5.8 | 480. |
| 16 | .490 | 210. | 5.8 | 480. |
| 17 | .510 | 219. | 5.7 | 480. |
| 18 | .490 | 210. | 5.7 | 480. |
| 19 | .500 | 215. | 5.7 | 480. |
| 20 | .520 | 223. | 5.7 | 460. |
| 21 | .560 | 241. | 6.0 | 460. |
| 22 | .570 | 245. | 6.0 | 455. |
| 23 | .550 | 236. | 6.1 | 455. |
| 24 | .560 | 241. | 6.1 | 452. |

DAY = 57

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.1 | 452. |
| 2 | .580 | 249. | 6.1 | 452. |
| 3 | .580 | 249. | 6.1 | 455. |
| 4 | .570 | 245. | 6.2 | 452. |
| 5 | .580 | 249. | 6.1 | 455. |
| 6 | .440 | 189. | 5.7 | 482. |
| 7 | .440 | 189. | 5.7 | 492. |
| 8 | .430 | 185. | 5.7 | 492. |
| 9 | .430 | 185. | 5.7 | 492. |
| 10 | .510 | 219. | 5.8 | 492. |
| 11 | .550 | 236. | 5.8 | 492. |
| 12 | .560 | 241. | 5.7 | 492. |
| 13 | .550 | 236. | 5.8 | 492. |
| 14 | .540 | 232. | 5.8 | 493. |
| 15 | .540 | 232. | 5.8 | 493. |
| 16 | .550 | 236. | 5.7 | 482. |
| 17 | .560 | 241. | 5.7 | 485. |
| 18 | .560 | 241. | 5.7 | 485. |
| 19 | .550 | 236. | 5.8 | 490. |
| 20 | .530 | 228. | 5.8 | 490. |
| 21 | .540 | 232. | 5.8 | 490. |
| 22 | .510 | 219. | 6.0 | 460. |
| 23 | .550 | 236. | 6.7 | 425. |
| 24 | .550 | 236. | 6.7 | 425. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.6 | 428. |
| 2 | .560 | 241. | 6.6 | 425. |
| 3 | .580 | 249. | 6.6 | 428. |
| 4 | .520 | 223. | 6.2 | 480. |
| 5 | .470 | 202. | 5.9 | 488. |
| 6 | .470 | 202. | 5.9 | 482. |
| 7 | .480 | 206. | 5.8 | 480. |
| 8 | .540 | 232. | 6.4 | 380. |
| 9 | .620 | 266. | 7.1 | 380. |
| 10 | .600 | 258. | 7.1 | 380. |
| 11 | .610 | 262. | 7.1 | 380. |
| 12 | .620 | 266. | 7.6 | 320. |
| 13 | .620 | 266. | 7.8 | 320. |
| 14 | .620 | 266. | 7.9 | 320. |
| 15 | .610 | 262. | 7.8 | 320. |
| 16 | .600 | 258. | 7.8 | 320. |
| 17 | .610 | 262. | 7.8 | 320. |
| 18 | .610 | 262. | 7.8 | 320. |
| 19 | .580 | 249. | 7.8 | 320. |
| 20 | .580 | 249. | 7.8 | 320. |
| 21 | .590 | 253. | 7.7 | 340. |
| 22 | .470 | 202. | 6.6 | 430. |
| 23 | .380 | 163. | 5.8 | 490. |
| 24 | .370 | 159. | 5.7 | 490. |

DAY = 59

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 5.7 | 490. |
| 2 | .410 | 176. | 5.8 | 485. |
| 3 | .420 | 180. | 5.7 | 485. |
| 4 | .410 | 176. | 5.7 | 488. |
| 5 | .410 | 176. | 5.7 | 488. |
| 6 | .430 | 185. | 5.7 | 485. |
| 7 | .470 | 202. | 5.9 | 422. |
| 8 | .550 | 236. | 6.6 | 400. |
| 9 | .620 | 266. | 7.1 | 370. |
| 10 | .620 | 266. | 7.7 | 325. |
| 11 | .610 | 262. | 7.6 | 350. |
| 12 | .560 | 241. | 7.4 | 350. |
| 13 | .530 | 228. | 8.4 | 240. |
| 14 | .530 | 228. | 9.1 | 240. |
| 15 | .540 | 232. | 9.1 | 240. |
| 16 | .550 | 236. | 9.2 | 240. |
| 17 | .550 | 236. | 9.2 | 240. |
| 18 | .590 | 253. | 8.5 | 330. |
| 19 | .490 | 210. | 7.1 | 380. |
| 20 | .400 | 172. | 5.9 | 490. |
| 21 | .400 | 172. | 5.4 | 510. |
| 22 | .430 | 185. | 5.4 | 510. |
| 23 | .420 | 180. | 5.5 | 505. |
| 24 | .460 | 198. | 5.6 | 490. |

DAY = 60

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 5.7 | 490. |
| 2 | .460 | 198. | 5.7 | 490. |
| 3 | .460 | 198. | 5.7 | 490. |
| 4 | .470 | 202. | 5.7 | 490. |
| 5 | .480 | 206. | 5.7 | 490. |
| 6 | .480 | 206. | 5.7 | 490. |
| 7 | .480 | 206. | 5.8 | 490. |
| 8 | .500 | 215. | 5.9 | 485. |
| 9 | .490 | 210. | 5.8 | 485. |
| 10 | .430 | 185. | 5.3 | 485. |
| 11 | .530 | 228. | 5.7 | 485. |
| 12 | .510 | 219. | 5.8 | 485. |
| 13 | .470 | 202. | 5.6 | 485. |
| 14 | .520 | 223. | 5.7 | 485. |
| 15 | .530 | 228. | 5.7 | 485. |
| 16 | .520 | 223. | 5.7 | 490. |
| 17 | .510 | 219. | 5.6 | 500. |
| 18 | .480 | 206. | 5.7 | 500. |
| 19 | .490 | 210. | 5.6 | 500. |
| 20 | .500 | 215. | 5.6 | 500. |
| 21 | .480 | 206. | 5.7 | 500. |
| 22 | .490 | 210. | 5.7 | 500. |
| 23 | .510 | 219. | 5.7 | 500. |
| 24 | .510 | 219. | 5.6 | 495. |

DAY = 61

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.8 | 495. |
| 2 | .510 | 219. | 5.8 | 495. |
| 3 | .500 | 215. | 5.7 | 495. |
| 4 | .530 | 228. | 5.7 | 495. |
| 5 | .530 | 228. | 5.7 | 495. |
| 6 | .540 | 232. | 5.7 | 495. |
| 7 | .510 | 219. | 5.8 | 495. |
| 8 | .490 | 210. | 5.8 | 490. |
| 9 | .520 | 223. | 5.8 | 495. |
| 10 | .530 | 228. | 5.7 | 495. |
| 11 | .550 | 236. | 5.7 | 495. |
| 12 | .540 | 232. | 5.7 | 495. |
| 13 | .460 | 198. | 5.8 | 495. |
| 14 | .450 | 193. | 5.8 | 490. |
| 15 | .490 | 210. | 5.8 | 490. |
| 16 | .520 | 223. | 5.7 | 495. |
| 17 | .530 | 228. | 5.6 | 500. |
| 18 | .530 | 228. | 5.7 | 500. |
| 19 | .470 | 202. | 5.8 | 500. |
| 20 | .470 | 202. | 5.7 | 500. |
| 21 | .470 | 202. | 5.7 | 500. |
| 22 | .470 | 202. | 5.7 | 495. |
| 23 | .460 | 198. | 5.8 | 495. |
| 24 | .470 | 202. | 5.8 | 495. |

DAY = 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 5.8 | 495. |
| 2 | .470 | 202. | 5.8 | 495. |
| 3 | .460 | 198. | 5.9 | 495. |
| 4 | .460 | 198. | 5.8 | 495. |
| 5 | .470 | 202. | 5.8 | 495. |
| 6 | .450 | 193. | 5.7 | 495. |
| 7 | .450 | 193. | 5.7 | 495. |
| 8 | .470 | 202. | 5.7 | 490. |
| 9 | .490 | 210. | 5.7 | 490. |
| 10 | .510 | 219. | 5.6 | 490. |
| 11 | .530 | 228. | 5.6 | 490. |
| 12 | .540 | 232. | 5.6 | 490. |
| 13 | .520 | 223. | 5.6 | 495. |
| 14 | .460 | 198. | 5.7 | 495. |
| 15 | .460 | 198. | 5.6 | 495. |
| 16 | .470 | 202. | 5.5 | 495. |
| 17 | .420 | 180. | 5.5 | 495. |
| 18 | .420 | 180. | 5.5 | 495. |
| 19 | .430 | 185. | 5.5 | 495. |
| 20 | .450 | 193. | 5.5 | 495. |
| 21 | .440 | 189. | 5.5 | 495. |
| 22 | .460 | 198. | 5.6 | 495. |
| 23 | .460 | 198. | 5.6 | 495. |
| 24 | .470 | 202. | 5.6 | 495. |

DAY = 63



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 5.6 | 495. |
| 2 | .410 | 176. | 7.5 | 495. |
| 3 | .370 | 159. | 7.9 | 495. |
| 4 | .370 | 159. | 7.9 | 495. |
| 5 | .370 | 159. | 7.8 | 495. |
| 6 | .440 | 189. | 6.4 | 495. |
| 7 | .410 | 176. | 5.5 | 495. |
| 8 | .450 | 193. | 5.5 | 490. |
| 9 | .490 | 210. | 5.6 | 490. |
| 10 | .600 | 258. | 6.7 | 490. |
| 11 | .490 | 210. | 6.8 | 490. |
| 12 | .530 | 228. | 7.3 | 490. |
| 13 | .580 | 249. | 7.6 | 495. |
| 14 | .550 | 236. | 7.3 | 495. |
| 15 | .490 | 210. | 5.9 | 495. |
| 16 | .530 | 228. | 5.5 | 495. |
| 17 | .510 | 219. | 5.6 | 495. |
| 18 | .470 | 202. | 5.6 | 495. |
| 19 | .470 | 202. | 5.6 | 495. |
| 20 | .490 | 210. | 5.6 | 495. |
| 21 | .490 | 210. | 5.6 | 495. |
| 22 | .480 | 206. | 5.6 | 495. |
| 23 | .480 | 206. | 5.6 | 495. |
| 24 | .500 | 215. | 5.7 | 495. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 5.6 | 490. |
| 2 | .510 | 219. | 5.7 | 490. |
| 3 | .500 | 215. | 5.7 | 490. |
| 4 | .510 | 219. | 5.7 | 490. |
| 5 | .520 | 223. | 5.7 | 490. |
| 6 | .500 | 215. | 5.8 | 490. |
| 7 | .490 | 210. | 5.7 | 490. |
| 8 | .500 | 215. | 5.8 | 490. |
| 9 | .500 | 215. | 5.8 | 490. |
| 10 | .450 | 193. | 5.8 | 490. |
| 11 | .450 | 193. | 5.8 | 490. |
| 12 | .450 | 193. | 5.8 | 490. |
| 13 | .450 | 193. | 5.7 | 490. |
| 14 | .450 | 193. | 5.7 | 490. |
| 15 | .440 | 189. | 5.7 | 490. |
| 16 | .430 | 185. | 5.6 | 490. |
| 17 | .440 | 189. | 5.5 | 490. |
| 18 | .440 | 189. | 5.6 | 490. |
| 19 | .430 | 185. | 5.7 | 490. |
| 20 | .440 | 189. | 5.6 | 490. |
| 21 | .440 | 189. | 5.6 | 490. |
| 22 | .450 | 193. | 5.7 | 490. |
| 23 | .450 | 193. | 5.7 | 490. |
| 24 | .440 | 189. | 5.7 | 490. |

DAY = 65

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 5.7 | 490. |
| 2 | .420 | 180. | 5.8 | 490. |
| 3 | .400 | 172. | 5.7 | 490. |
| 4 | .410 | 176. | 5.7 | 490. |
| 5 | .470 | 202. | 5.6 | 490. |
| 6 | .460 | 198. | 5.8 | 490. |
| 7 | .410 | 176. | 5.6 | 490. |
| 8 | .450 | 193. | 5.7 | 490. |
| 9 | .470 | 202. | 5.7 | 485. |
| 10 | .470 | 202. | 5.6 | 485. |
| 11 | .500 | 215. | 5.6 | 490. |
| 12 | .490 | 210. | 5.6 | 490. |
| 13 | .420 | 180. | 5.7 | 490. |
| 14 | .430 | 185. | 5.7 | 490. |
| 15 | .450 | 193. | 5.6 | 490. |
| 16 | .450 | 193. | 5.5 | 485. |
| 17 | .460 | 198. | 5.5 | 482. |
| 18 | .440 | 189. | 5.5 | 490. |
| 19 | .470 | 202. | 5.7 | 490. |
| 20 | .480 | 204. | 5.6 | 485. |
| 21 | .490 | 210. | 5.6 | 485. |
| 22 | .510 | 219. | 5.5 | 490. |
| 23 | .490 | 210. | 5.5 | 488. |
| 24 | .530 | 228. | 6.0 | 400. |

DAY = 66

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 7.3 | 290. |
| 2 | .610 | 262. | 8.2 | 290. |
| 3 | .620 | 266. | 8.2 | 290. |
| 4 | .640 | 275. | 8.1 | 290. |
| 5 | .560 | 241. | 6.9 | 390. |
| 6 | .390 | 168. | 5.6 | 485. |
| 7 | .390 | 168. | 5.5 | 485. |
| 8 | .410 | 176. | 5.6 | 485. |
| 9 | .420 | 180. | 5.6 | 480. |
| 10 | .420 | 180. | 5.7 | 465. |
| 11 | .530 | 228. | 6.4 | 420. |
| 12 | .550 | 236. | 6.5 | 420. |
| 13 | .540 | 232. | 6.6 | 420. |
| 14 | .530 | 228. | 6.6 | 420. |
| 15 | .530 | 228. | 6.6 | 420. |
| 16 | .540 | 232. | 6.5 | 420. |
| 17 | .550 | 236. | 6.6 | 420. |
| 18 | .510 | 219. | 6.6 | 420. |
| 19 | .520 | 223. | 6.6 | 420. |
| 20 | .520 | 223. | 6.6 | 420. |
| 21 | .530 | 228. | 6.6 | 420. |
| 22 | .530 | 228. | 6.6 | 420. |
| 23 | .530 | 228. | 6.7 | 420. |
| 24 | .540 | 232. | 6.7 | 420. |

DAY = 67

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 6.7 | 420. |
| 2 | .560 | 241. | 6.7 | 420. |
| 3 | .580 | 249. | 6.7 | 420. |
| 4 | .570 | 245. | 6.7 | 425. |
| 5 | .560 | 241. | 6.8 | 420. |
| 6 | .570 | 245. | 6.7 | 420. |
| 7 | .580 | 249. | 6.7 | 420. |
| 8 | .600 | 258. | 6.7 | 420. |
| 9 | .600 | 258. | 6.7 | 420. |
| 10 | .610 | 262. | 6.7 | 420. |
| 11 | .620 | 266. | 6.7 | 420. |
| 12 | .610 | 262. | 6.7 | 420. |
| 13 | .580 | 249. | 6.8 | 425. |
| 14 | .570 | 245. | 6.8 | 425. |
| 15 | .580 | 249. | 6.8 | 420. |
| 16 | .590 | 253. | 6.8 | 420. |
| 17 | .610 | 262. | 6.8 | 420. |
| 18 | .580 | 249. | 6.8 | 420. |
| 19 | .590 | 253. | 6.9 | 420. |
| 20 | .600 | 258. | 6.9 | 420. |
| 21 | .600 | 258. | 6.9 | 418. |
| 22 | .610 | 262. | 6.9 | 420. |
| 23 | .610 | 262. | 6.9 | 420. |
| 24 | .610 | 262. | 6.9 | 420. |

DAY = 68

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 6.9 | 420. |
| 2 | .620 | 266. | 6.9 | 420. |
| 3 | .620 | 266. | 6.8 | 420. |
| 4 | .630 | 271. | 6.9 | 420. |
| 5 | .600 | 258. | 6.9 | 420. |
| 6 | .590 | 253. | 6.8 | 420. |
| 7 | .590 | 253. | 6.7 | 420. |
| 8 | .600 | 258. | 6.8 | 420. |
| 9 | .600 | 258. | 6.8 | 420. |
| 10 | .600 | 258. | 6.8 | 420. |
| 11 | .590 | 253. | 6.8 | 420. |
| 12 | .590 | 253. | 6.8 | 420. |
| 13 | .610 | 262. | 6.7 | 420. |
| 14 | .590 | 253. | 6.8 | 420. |
| 15 | .590 | 253. | 6.8 | 420. |
| 16 | .590 | 253. | 6.7 | 418. |
| 17 | .600 | 258. | 6.8 | 420. |
| 18 | .580 | 249. | 6.8 | 420. |
| 19 | .590 | 253. | 6.8 | 420. |
| 20 | .590 | 253. | 6.8 | 420. |
| 21 | .570 | 245. | 6.8 | 420. |
| 22 | .580 | 249. | 6.8 | 420. |
| 23 | .570 | 245. | 6.9 | 420. |
| 24 | .530 | 228. | 7.2 | 350. |

DAY = 69

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 8.4 | 300. |
| 2 | .350 | 150. | 9.7 | 180. |
| 3 | .320 | 137. | 10.2 | 180. |
| 4 | .450 | 193. | 9.7 | 250. |
| 5 | .460 | 198. | 7.6 | 415. |
| 6 | .530 | 228. | 6.9 | 420. |
| 7 | .530 | 228. | 6.8 | 420. |
| 8 | .560 | 241. | 6.9 | 420. |
| 9 | .620 | 266. | 6.9 | 420. |
| 10 | .600 | 258. | 7.0 | 420. |
| 11 | .600 | 258. | 7.0 | 420. |
| 12 | .610 | 262. | 6.9 | 420. |
| 13 | .610 | 262. | 6.9 | 420. |
| 14 | .590 | 253. | 6.9 | 420. |
| 15 | .590 | 253. | 6.9 | 420. |
| 16 | .590 | 253. | 6.9 | 415. |
| 17 | .580 | 249. | 7.0 | 415. |
| 18 | .570 | 245. | 7.0 | 415. |
| 19 | .570 | 245. | 6.9 | 418. |
| 20 | .560 | 241. | 6.9 | 418. |
| 21 | .570 | 245. | 7.0 | 418. |
| 22 | .570 | 245. | 6.9 | 422. |
| 23 | .490 | 210. | 6.2 | 485. |
| 24 | .510 | 219. | 6.2 | 480. |

DAY = 70

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 8.9 | 250. |
| 2 | .440 | 189. | 10.1 | 175. |
| 3 | .410 | 176. | 10.1 | 175. |
| 4 | .410 | 176. | 10.1 | 175. |
| 5 | .410 | 176. | 10.1 | 175. |
| 6 | .450 | 193. | 9.4 | 390. |
| 7 | .530 | 228. | 6.1 | 480. |
| 8 | .540 | 232. | 6.1 | 480. |
| 9 | .560 | 241. | 6.1 | 480. |
| 10 | .560 | 241. | 6.1 | 480. |
| 11 | .560 | 241. | 6.0 | 490. |
| 12 | .530 | 228. | 6.0 | 490. |
| 13 | .510 | 219. | 5.9 | 490. |
| 14 | .520 | 223. | 5.9 | 490. |
| 15 | .510 | 219. | 5.9 | 490. |
| 16 | .530 | 228. | 7.3 | 322. |
| 17 | .570 | 245. | 8.0 | 322. |
| 18 | .560 | 241. | 8.0 | 322. |
| 19 | .570 | 245. | 8.1 | 320. |
| 20 | .490 | 210. | 9.5 | 230. |
| 21 | .500 | 215. | 9.6 | 230. |
| 22 | .400 | 172. | 10.1 | 180. |
| 23 | .360 | 155. | 10.1 | 182. |
| 24 | .360 | 155. | 10.1 | 180. |

DAY = 71



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 10.1 | 180. |
| 2 | .360 | 155. | 10.1 | 185. |
| 3 | .380 | 163. | 10.1 | 185. |
| 4 | .380 | 163. | 10.1 | 185. |
| 5 | .380 | 163. | 10.1 | 180. |
| 6 | .390 | 168. | 10.1 | 185. |
| 7 | .450 | 193. | 9.4 | 260. |
| 8 | .550 | 236. | 7.1 | 465. |
| 9 | .500 | 215. | 5.8 | 470. |
| 10 | .520 | 223. | 5.9 | 475. |
| 11 | .520 | 223. | 5.9 | 475. |
| 12 | .520 | 223. | 5.7 | 475. |
| 13 | .570 | 245. | 6.5 | 360. |
| 14 | .470 | 202. | 8.6 | 230. |
| 15 | .530 | 228. | 9.2 | 230. |
| 16 | .510 | 219. | 9.7 | 180. |
| 17 | .500 | 215. | 10.0 | 180. |
| 18 | .500 | 215. | 10.0 | 180. |
| 19 | .510 | 219. | 10.0 | 180. |
| 20 | .510 | 219. | 10.0 | 180. |
| 21 | .510 | 219. | 10.0 | 180. |
| 22 | .500 | 215. | 10.0 | 180. |
| 23 | .520 | 223. | 10.0 | 180. |
| 24 | .510 | 219. | 10.0 | 180. |

DAY = 72

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 10.0 | 180. |
| 2 | .500 | 215. | 10.0 | 180. |
| 3 | .490 | 210. | 10.0 | 180. |
| 4 | .500 | 215. | 10.0 | 180. |
| 5 | .500 | 215. | 10.0 | 185. |
| 6 | .500 | 215. | 10.0 | 185. |
| 7 | .490 | 210. | 9.9 | 195. |
| 8 | .510 | 219. | 8.1 | 380. |
| 9 | .440 | 189. | 6.5 | 490. |
| 10 | .490 | 210. | 5.9 | 490. |
| 11 | .500 | 215. | 5.9 | 490. |
| 12 | .510 | 219. | 5.9 | 460. |
| 13 | .700 | 301. | 7.1 | 390. |
| 14 | .700 | 301. | 7.2 | 375. |
| 15 | .470 | 202. | 8.6 | 275. |
| 16 | .460 | 198. | 8.9 | 275. |
| 17 | .450 | 193. | 8.9 | 275. |
| 18 | .490 | 210. | 8.5 | 345. |
| 19 | .510 | 219. | 7.3 | 325. |
| 20 | .620 | 266. | 6.8 | 425. |
| 21 | .660 | 284. | 6.7 | 425. |
| 22 | .650 | 279. | 6.8 | 425. |
| 23 | .610 | 262. | 7.2 | 300. |
| 24 | .510 | 219. | 9.8 | 180. |

DAY = 73



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.1 | 180. |
| 2 | .420 | 180. | 10.1 | 180. |
| 3 | .430 | 185. | 10.1 | 180. |
| 4 | .440 | 189. | 10.1 | 175. |
| 5 | .430 | 185. | 10.1 | 175. |
| 6 | .440 | 189. | 10.1 | 180. |
| 7 | .500 | 215. | 9.0 | 360. |
| 8 | .540 | 232. | 7.0 | 445. |
| 9 | .580 | 249. | 6.4 | 460. |
| 10 | .510 | 219. | 5.8 | 490. |
| 11 | .510 | 219. | 5.8 | 500. |
| 12 | .510 | 219. | 5.8 | 500. |
| 13 | .510 | 219. | 5.7 | 500. |
| 14 | .490 | 210. | 5.7 | 488. |
| 15 | .610 | 262. | 6.6 | 412. |
| 16 | .610 | 262. | 6.8 | 412. |
| 17 | .600 | 258. | 6.7 | 412. |
| 18 | .520 | 223. | 6.0 | 475. |
| 19 | .530 | 228. | 6.0 | 475. |
| 20 | .530 | 228. | 6.0 | 475. |
| 21 | .530 | 228. | 6.1 | 475. |
| 22 | .550 | 236. | 6.1 | 475. |
| 23 | .580 | 249. | 6.6 | 428. |
| 24 | .570 | 245. | 8.7 | 220. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 10.1 | 175. |
| 2 | .410 | 176. | 10.1 | 175. |
| 3 | .430 | 185. | 10.1 | 175. |
| 4 | .450 | 193. | 10.1 | 175. |
| 5 | .460 | 198. | 10.1 | 175. |
| 6 | .440 | 189. | 10.0 | 185. |
| 7 | .430 | 185. | 8.6 | 175. |
| 8 | .420 | 180. | 8.6 | 275. |
| 9 | .420 | 180. | 8.6 | 275. |
| 10 | .430 | 185. | 8.6 | 275. |
| 11 | .430 | 185. | 8.6 | 275. |
| 12 | .460 | 198. | 10.0 | 175. |
| 13 | .430 | 185. | 10.1 | 175. |
| 14 | .420 | 180. | 10.1 | 175. |
| 15 | .420 | 180. | 10.1 | 175. |
| 16 | .420 | 180. | 10.1 | 175. |
| 17 | .410 | 176. | 10.1 | 175. |
| 18 | .400 | 172. | 10.1 | 175. |
| 19 | .410 | 176. | 10.1 | 175. |
| 20 | .410 | 176. | 10.1 | 175. |
| 21 | .420 | 180. | 10.1 | 175. |
| 22 | .410 | 176. | 10.1 | 175. |
| 23 | .420 | 180. | 10.1 | 175. |
| 24 | .410 | 176. | 10.1 | 175. |

DAY = 75

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.1 | 175. |
| 2 | .400 | 172. | 10.1 | 175. |
| 3 | .400 | 172. | 10.1 | 175. |
| 4 | .390 | 168. | 10.1 | 175. |
| 5 | .390 | 168. | 10.1 | 175. |
| 6 | .380 | 163. | 10.1 | 175. |
| 7 | .390 | 168. | 10.0 | 175. |
| 8 | .390 | 168. | 10.1 | 175. |
| 9 | .390 | 168. | 10.1 | 175. |
| 10 | .400 | 172. | 10.1 | 175. |
| 11 | .390 | 168. | 10.1 | 175. |
| 12 | .390 | 168. | 10.1 | 175. |
| 13 | .390 | 168. | 10.1 | 175. |
| 14 | .400 | 172. | 10.1 | 175. |
| 15 | .390 | 168. | 10.1 | 175. |
| 16 | .390 | 168. | 10.1 | 175. |
| 17 | .400 | 172. | 10.1 | 175. |
| 18 | .410 | 176. | 10.1 | 175. |
| 19 | .430 | 185. | 10.1 | 175. |
| 20 | .430 | 185. | 10.1 | 175. |
| 21 | .430 | 185. | 10.1 | 175. |
| 22 | .440 | 189. | 10.1 | 175. |
| 23 | .450 | 193. | 10.1 | 175. |
| 24 | .450 | 193. | 10.1 | 175. |

DAY = 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 10.1 | 175. |
| 2 | .440 | 189. | 10.1 | 175. |
| 3 | .430 | 185. | 10.1 | 175. |
| 4 | .420 | 180. | 10.1 | 175. |
| 5 | .420 | 180. | 10.1 | 175. |
| 6 | .440 | 189. | 9.7 | 250. |
| 7 | .440 | 189. | 6.7 | 465. |
| 8 | .430 | 185. | 5.6 | 500. |
| 9 | .440 | 189. | 5.6 | 500. |
| 10 | .450 | 193. | 5.6 | 500. |
| 11 | .470 | 202. | 5.6 | 500. |
| 12 | .470 | 202. | 5.6 | 500. |
| 13 | .470 | 202. | 5.6 | 500. |
| 14 | .480 | 206. | 5.5 | 500. |
| 15 | .470 | 202. | 5.6 | 500. |
| 16 | .470 | 202. | 5.6 | 500. |
| 17 | .480 | 206. | 5.6 | 500. |
| 18 | .490 | 210. | 5.7 | 500. |
| 19 | .500 | 215. | 5.7 | 500. |
| 20 | .660 | 284. | 6.7 | 400. |
| 21 | .710 | 305. | 7.0 | 400. |
| 22 | .610 | 262. | 7.6 | 300. |
| 23 | .470 | 202. | 9.2 | 230. |
| 24 | .490 | 210. | 9.3 | 230. |

DAY = 77

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 9.3 | 230. |
| 2 | .420 | 180. | 10.0 | 180. |
| 3 | .410 | 176. | 10.1 | 180. |
| 4 | .410 | 176. | 10.1 | 180. |
| 5 | .420 | 180. | 10.1 | 180. |
| 6 | .490 | 210. | 9.3 | 340. |
| 7 | .470 | 202. | 6.4 | 485. |
| 8 | .450 | 193. | 5.7 | 490. |
| 9 | .460 | 198. | 5.6 | 490. |
| 10 | .470 | 202. | 5.6 | 490. |
| 11 | .460 | 198. | 5.7 | 490. |
| 12 | .450 | 193. | 5.8 | 490. |
| 13 | .450 | 193. | 5.7 | 490. |
| 14 | .420 | 180. | 5.6 | 490. |
| 15 | .430 | 185. | 5.6 | 490. |
| 16 | .520 | 223. | 6.7 | 390. |
| 17 | .540 | 232. | 6.9 | 390. |
| 18 | .550 | 236. | 6.9 | 390. |
| 19 | .460 | 198. | 6.0 | 490. |
| 20 | .440 | 189. | 5.8 | 490. |
| 21 | .450 | 193. | 5.8 | 490. |
| 22 | .500 | 215. | 6.2 | 390. |
| 23 | .560 | 241. | 7.0 | 390. |
| 24 | .550 | 236. | 7.1 | 390. |

DAY = 78

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 7.9 | 280. |
| 2 | .410 | 176. | 9.1 | 230. |
| 3 | .460 | 198. | 9.9 | 230. |
| 4 | .390 | 168. | 10.0 | 230. |
| 5 | .400 | 172. | 8.5 | 310. |
| 6 | .570 | 245. | 7.6 | 360. |
| 7 | .690 | 296. | 7.3 | 360. |
| 8 | .580 | 249. | 6.6 | 480. |
| 9 | .480 | 206. | 5.8 | 480. |
| 10 | .490 | 210. | 5.8 | 480. |
| 11 | .550 | 236. | 6.2 | 420. |
| 12 | .540 | 232. | 7.0 | 350. |
| 13 | .540 | 232. | 7.7 | 325. |
| 14 | .590 | 253. | 7.8 | 320. |
| 15 | .620 | 266. | 8.1 | 285. |
| 16 | .440 | 189. | 10.0 | 180. |
| 17 | .380 | 163. | 10.1 | 180. |
| 18 | .380 | 163. | 10.1 | 180. |
| 19 | .380 | 163. | 10.1 | 180. |
| 20 | .380 | 163. | 10.1 | 180. |
| 21 | .390 | 168. | 10.1 | 180. |
| 22 | .380 | 163. | 10.1 | 180. |
| 23 | .380 | 163. | 10.1 | 175. |
| 24 | .370 | 159. | 10.1 | 175. |

DAY = 79



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.1 | 175. |
| 2 | .380 | 163. | 10.1 | 175. |
| 3 | .380 | 163. | 10.1 | 175. |
| 4 | .380 | 163. | 10.1 | 175. |
| 5 | .370 | 159. | 10.1 | 175. |
| 6 | .370 | 159. | 10.1 | 175. |
| 7 | .370 | 159. | 10.0 | 175. |
| 8 | .370 | 159. | 10.0 | 180. |
| 9 | .370 | 159. | 10.0 | 180. |
| 10 | .370 | 159. | 10.0 | 180. |
| 11 | .390 | 168. | 10.0 | 180. |
| 12 | .570 | 245. | 9.8 | 200. |
| 13 | .570 | 245. | 9.8 | 180. |
| 14 | .420 | 180. | 10.0 | 180. |
| 15 | .420 | 180. | 10.0 | 178. |
| 16 | .420 | 180. | 10.0 | 180. |
| 17 | .410 | 176. | 10.0 | 180. |
| 18 | .400 | 172. | 10.0 | 180. |
| 19 | .410 | 176. | 10.0 | 180. |
| 20 | .420 | 180. | 10.0 | 180. |
| 21 | .410 | 176. | 10.0 | 180. |
| 22 | .420 | 180. | 10.1 | 180. |
| 23 | .420 | 180. | 10.1 | 180. |
| 24 | .420 | 180. | 10.1 | 180. |

DAY = 80

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.1 | 180. |
| 2 | .400 | 172. | 10.1 | 180. |
| 3 | .400 | 172. | 10.1 | 175. |
| 4 | .400 | 172. | 10.1 | 175. |
| 5 | .470 | 202. | 9.6 | 240. |
| 6 | .510 | 219. | 7.8 | 390. |
| 7 | .530 | 228. | 6.2 | 490. |
| 8 | .520 | 223. | 5.8 | 490. |
| 9 | .520 | 223. | 5.9 | 490. |
| 10 | .500 | 215. | 5.9 | 490. |
| 11 | .510 | 219. | 5.8 | 390. |
| 12 | .570 | 245. | 6.5 | 390. |
| 13 | .670 | 288. | 7.1 | 340. |
| 14 | .660 | 284. | 7.3 | 290. |
| 15 | .670 | 288. | 8.4 | 290. |
| 16 | .450 | 193. | 8.8 | 265. |
| 17 | .420 | 180. | 8.9 | 265. |
| 18 | .420 | 180. | 8.9 | 265. |
| 19 | .430 | 185. | 8.8 | 265. |
| 20 | .430 | 185. | 8.9 | 265. |
| 21 | .420 | 180. | 8.9 | 265. |
| 22 | .430 | 185. | 8.9 | 265. |
| 23 | .450 | 193. | 8.9 | 265. |
| 24 | .440 | 189. | 8.9 | 262. |

DAY = 81

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 8.8 | 280. |
| 2 | .460 | 198. | 8.3 | 300. |
| 3 | .460 | 198. | 8.3 | 300. |
| 4 | .450 | 193. | 8.2 | 300. |
| 5 | .440 | 189. | 8.2 | 300. |
| 6 | .450 | 193. | 8.2 | 300. |
| 7 | .450 | 193. | 8.0 | 300. |
| 8 | .450 | 193. | 8.1 | 300. |
| 9 | .450 | 193. | 8.1 | 300. |
| 10 | .510 | 219. | 7.7 | 350. |
| 11 | .560 | 241. | 7.3 | 350. |
| 12 | .570 | 245. | 7.3 | 350. |
| 13 | .570 | 245. | 7.3 | 350. |
| 14 | .590 | 253. | 7.4 | 300. |
| 15 | .650 | 279. | 8.1 | 300. |
| 16 | .660 | 284. | 8.0 | 300. |
| 17 | .680 | 292. | 8.0 | 300. |
| 18 | .680 | 292. | 8.0 | 310. |
| 19 | .630 | 271. | 7.6 | 325. |
| 20 | .640 | 275. | 7.7 | 325. |
| 21 | .620 | 266. | 7.7 | 325. |
| 22 | .630 | 271. | 7.8 | 325. |
| 23 | .640 | 275. | 7.8 | 325. |
| 24 | .650 | 279. | 7.8 | 325. |

DAY = 82

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.8 | 322. |
| 2 | .720 | 309. | 8.7 | 275. |
| 3 | .720 | 309. | 8.8 | 275. |
| 4 | .710 | 305. | 8.7 | 275. |
| 5 | .720 | 309. | 8.8 | 275. |
| 6 | .740 | 318. | 8.8 | 275. |
| 7 | .730 | 314. | 8.7 | 275. |
| 8 | .750 | 322. | 8.8 | 275. |
| 9 | .680 | 292. | 8.1 | 325. |
| 10 | .650 | 279. | 7.8 | 325. |
| 11 | .640 | 275. | 7.7 | 325. |
| 12 | .660 | 284. | 7.7 | 325. |
| 13 | .660 | 284. | 7.7 | 325. |
| 14 | .640 | 275. | 7.7 | 325. |
| 15 | .640 | 275. | 7.7 | 325. |
| 16 | .590 | 253. | 7.7 | 325. |
| 17 | .570 | 245. | 7.7 | 325. |
| 18 | .570 | 245. | 7.5 | 370. |
| 19 | .510 | 219. | 6.9 | 390. |
| 20 | .490 | 210. | 6.8 | 400. |
| 21 | .500 | 215. | 6.8 | 400. |
| 22 | .500 | 215. | 6.8 | 400. |
| 23 | .500 | 215. | 6.8 | 400. |
| 24 | .510 | 219. | 6.8 | 400. |

DAY = 83



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 6.8 | 400. |
| 2 | .510 | 219. | 6.8 | 400. |
| 3 | .510 | 219. | 6.9 | 400. |
| 4 | .520 | 223. | 6.9 | 400. |
| 5 | .520 | 223. | 6.9 | 400. |
| 6 | .560 | 241. | 7.3 | 325. |
| 7 | .590 | 253. | 7.7 | 340. |
| 8 | .520 | 223. | 7.0 | 400. |
| 9 | .560 | 241. | 6.8 | 430. |
| 10 | .610 | 262. | 6.4 | 440. |
| 11 | .610 | 262. | 6.4 | 445. |
| 12 | .620 | 266. | 6.4 | 445. |
| 13 | .620 | 266. | 6.4 | 445. |
| 14 | .610 | 262. | 6.4 | 445. |
| 15 | .610 | 262. | 6.4 | 445. |
| 16 | .590 | 253. | 6.4 | 445. |
| 17 | .570 | 245. | 6.3 | 425. |
| 18 | .600 | 258. | 6.4 | 460. |
| 19 | .550 | 236. | 6.1 | 450. |
| 20 | .650 | 279. | 7.1 | 375. |
| 21 | .680 | 292. | 7.2 | 375. |
| 22 | .640 | 275. | 6.8 | 425. |
| 23 | .640 | 275. | 6.7 | 425. |
| 24 | .650 | 279. | 6.7 | 425. |

DAY = 84

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.8 | 325. |
| 2 | .600 | 258. | 7.9 | 325. |
| 3 | .560 | 241. | 8.1 | 280. |
| 4 | .450 | 193. | 9.1 | 250. |
| 5 | .470 | 202. | 9.1 | 250. |
| 6 | .410 | 176. | 8.5 | 300. |
| 7 | .430 | 185. | 8.1 | 310. |
| 8 | .530 | 228. | 7.3 | 350. |
| 9 | .570 | 245. | 7.7 | 325. |
| 10 | .590 | 253. | 7.8 | 325. |
| 11 | .590 | 253. | 8.1 | 275. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .490 | 210. | 8.9 | 250. |
| 14 | .500 | 215. | 8.9 | 250. |
| 15 | .160 | 69. | 3.7 | 250. |
| 16 | .210 | 90. | 1.5 | 240. |
| 17 | .310 | 133. | 2.5 | 250. |
| 18 | .310 | 133. | 2.5 | 250. |
| 19 | .350 | 150. | 1.6 | 300. |
| 20 | .420 | 180. | 1.8 | 300. |
| 21 | .430 | 185. | 2.0 | 300. |
| 22 | .430 | 185. | 2.0 | 300. |
| 23 | .420 | 180. | 1.6 | 325. |
| 24 | .360 | 155. | 2.0 | 275. |

DAY = 85



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 2.4 | 275. |
| 2 | .370 | 159. | 2.5 | 275. |
| 3 | .360 | 155. | 2.5 | 275. |
| 4 | .380 | 163. | 2.6 | 272. |
| 5 | .370 | 159. | 2.6 | 272. |
| 6 | .380 | 163. | 1.8 | 322. |
| 7 | .380 | 163. | 1.5 | 371. |
| 8 | .550 | 236. | 7.2 | 325. |
| 9 | .560 | 241. | 7.6 | 300. |
| 10 | .430 | 185. | 8.3 | 270. |
| 11 | .460 | 198. | 8.4 | 275. |
| 12 | .470 | 202. | 8.4 | 275. |
| 13 | .480 | 206. | 8.5 | 275. |
| 14 | .470 | 202. | 8.5 | 275. |
| 15 | .470 | 202. | 8.5 | 275. |
| 16 | .460 | 198. | 8.5 | 275. |
| 17 | .460 | 198. | 8.5 | 275. |
| 18 | .470 | 202. | 7.9 | 370. |
| 19 | .450 | 193. | 6.9 | 380. |
| 20 | .440 | 189. | 6.9 | 380. |
| 21 | .450 | 193. | 7.0 | 380. |
| 22 | .470 | 202. | 7.0 | 380. |
| 23 | .480 | 206. | 7.1 | 380. |
| 24 | .490 | 210. | 7.1 | 378. |

DAY = 86

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .490 | 210. | 7.1 | 375. |
| 2 | .490 | 210. | 7.1 | 375. |
| 3 | .490 | 210. | 7.1 | 378. |
| 4 | .510 | 219. | 7.1 | 380. |
| 5 | .530 | 228. | 7.1 | 380. |
| 6 | .540 | 232. | 7.0 | 380. |
| 7 | .540 | 232. | 8.1 | 280. |
| 8 | .560 | 241. | 7.5 | 350. |
| 9 | .540 | 232. | 7.1 | 380. |
| 10 | .530 | 228. | 7.0 | 380. |
| 11 | .570 | 245. | 7.4 | 330. |
| 12 | .600 | 258. | 7.7 | 300. |
| 13 | .500 | 215. | 8.8 | 250. |
| 14 | .460 | 198. | 8.5 | 275. |
| 15 | .450 | 193. | 8.5 | 275. |
| 16 | .440 | 189. | 8.5 | 275. |
| 17 | .430 | 185. | 8.5 | 275. |
| 18 | .390 | 168. | 7.7 | 380. |
| 19 | .380 | 163. | 6.9 | 380. |
| 20 | .550 | 236. | 6.9 | 380. |
| 21 | .560 | 241. | 6.9 | 380. |
| 22 | .560 | 241. | 6.9 | 380. |
| 23 | .560 | 241. | 7.0 | 380. |
| 24 | .580 | 249. | 7.0 | 375. |

DAY = 87

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 7.6 | 320. |
| 2 | .460 | 198. | 7.6 | 320. |
| 3 | .530 | 228. | 7.6 | 320. |
| 4 | .530 | 228. | 7.6 | 322. |
| 5 | .550 | 236. | 7.6 | 322. |
| 6 | .550 | 236. | 7.6 | 322. |
| 7 | .480 | 206. | 7.0 | 375. |
| 8 | .530 | 228. | 6.5 | 425. |
| 9 | .570 | 245. | 6.5 | 425. |
| 10 | .570 | 245. | 6.5 | 425. |
| 11 | .590 | 253. | 6.9 | 390. |
| 12 | .550 | 236. | 7.0 | 360. |
| 13 | .570 | 245. | 7.7 | 325. |
| 14 | .580 | 249. | 7.7 | 325. |
| 15 | .580 | 249. | 7.8 | 325. |
| 16 | .580 | 249. | 7.8 | 325. |
| 17 | .570 | 245. | 7.8 | 325. |
| 18 | .490 | 210. | 7.4 | 420. |
| 19 | .390 | 168. | 6.4 | 450. |
| 20 | .380 | 163. | 6.4 | 430. |
| 21 | .400 | 172. | 6.4 | 430. |
| 22 | .400 | 172. | 6.4 | 430. |
| 23 | .400 | 172. | 6.4 | 430. |
| 24 | .450 | 193. | 6.4 | 430. |

DAY = 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 6.4 | 430. |
| 2 | .430 | 185. | 6.5 | 430. |
| 3 | .460 | 198. | 6.5 | 430. |
| 4 | .490 | 210. | 6.5 | 430. |
| 5 | .510 | 219. | 6.5 | 430. |
| 6 | .540 | 232. | 6.5 | 430. |
| 7 | .550 | 236. | 6.6 | 430. |
| 8 | .530 | 228. | 6.5 | 430. |
| 9 | .540 | 232. | 6.6 | 430. |
| 10 | .510 | 219. | 6.5 | 440. |
| 11 | .510 | 219. | 6.5 | 435. |
| 12 | .490 | 210. | 6.7 | 415. |
| 13 | .500 | 215. | 6.9 | 380. |
| 14 | .510 | 219. | 7.1 | 375. |
| 15 | .500 | 215. | 7.1 | 375. |
| 16 | .500 | 215. | 7.1 | 375. |
| 17 | .500 | 215. | 7.1 | 375. |
| 18 | .510 | 219. | 7.1 | 375. |
| 19 | .490 | 210. | 7.3 | 345. |
| 20 | .290 | 125. | 7.7 | 330. |
| 21 | .340 | 146. | 7.7 | 330. |
| 22 | .340 | 146. | 7.8 | 330. |
| 23 | .350 | 150. | 7.7 | 330. |
| 24 | .380 | 163. | 7.7 | 330. |

DAY = 89



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 7.7 | 330. |
| 2 | .380 | 163. | 7.7 | 330. |
| 3 | .420 | 180. | 8.5 | 280. |
| 4 | .430 | 185. | 8.6 | 280. |
| 5 | .430 | 185. | 8.6 | 280. |
| 6 | .430 | 185. | 8.6 | 280. |
| 7 | .420 | 180. | 8.6 | 280. |
| 8 | .410 | 176. | 8.4 | 280. |
| 9 | .390 | 168. | 8.2 | 325. |
| 10 | .380 | 163. | 7.7 | 325. |
| 11 | .380 | 163. | 7.7 | 325. |
| 12 | .410 | 176. | 6.3 | 480. |
| 13 | .390 | 168. | 5.6 | 480. |
| 14 | .410 | 176. | 5.5 | 485. |
| 15 | .430 | 185. | 5.6 | 485. |
| 16 | .450 | 193. | 5.6 | 485. |
| 17 | .450 | 193. | 5.6 | 485. |
| 18 | .420 | 180. | 5.7 | 485. |
| 19 | .450 | 193. | 6.0 | 415. |
| 20 | .440 | 189. | 7.3 | 330. |
| 21 | .450 | 193. | 7.6 | 330. |
| 22 | .460 | 198. | 7.7 | 330. |
| 23 | .450 | 193. | 7.7 | 330. |
| 24 | .460 | 198. | 7.6 | 330. |

DAY = 90

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 7.6 | 330. |
| 2 | .470 | 202. | 7.4 | 330. |
| 3 | .460 | 198. | 7.6 | 330. |
| 4 | .570 | 245. | 7.6 | 330. |
| 5 | .600 | 258. | 7.6 | 330. |
| 6 | .540 | 232. | 7.2 | 375. |
| 7 | .570 | 245. | 7.0 | 400. |
| 8 | .560 | 241. | 5.9 | 490. |
| 9 | .450 | 193. | 5.8 | 485. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .540 | 232. | 5.8 | 490. |
| 12 | .500 | 215. | 5.9 | 460. |
| 13 | .460 | 198. | 6.6 | 390. |
| 14 | .490 | 210. | 7.2 | 350. |
| 15 | .430 | 185. | 8.2 | 375. |
| 16 | .480 | 206. | 6.7 | 420. |
| 17 | .440 | 189. | 6.1 | 475. |
| 18 | .420 | 180. | 5.7 | 490. |
| 19 | .410 | 176. | 5.7 | 490. |
| 20 | .400 | 172. | 5.8 | 490. |
| 21 | .400 | 172. | 5.8 | 490. |
| 22 | .400 | 172. | 5.7 | 490. |
| 23 | .400 | 172. | 5.7 | 490. |
| 24 | .410 | 176. | 5.7 | 490. |

DAY = 91



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 5.7 | 490. |
| 2 | .420 | 180. | 5.8 | 490. |
| 3 | .430 | 185. | 5.7 | 490. |
| 4 | .440 | 189. | 5.7 | 490. |
| 5 | .430 | 185. | 5.8 | 490. |
| 6 | .420 | 180. | 5.8 | 490. |
| 7 | .440 | 189. | 5.8 | 490. |
| 8 | .440 | 189. | 5.6 | 490. |
| 9 | .440 | 189. | 5.7 | 495. |
| 10 | .410 | 176. | 5.7 | 500. |
| 11 | .420 | 180. | 5.6 | 495. |
| 12 | .420 | 180. | 5.6 | 495. |
| 13 | .420 | 180. | 5.6 | 490. |
| 14 | .470 | 202. | 6.1 | 420. |
| 15 | .570 | 245. | 7.0 | 385. |
| 16 | .530 | 228. | 6.9 | 420. |
| 17 | .420 | 180. | 6.0 | 485. |
| 18 | .390 | 168. | 5.5 | 485. |
| 19 | .420 | 180. | 6.2 | 370. |
| 20 | .370 | 159. | 7.4 | 340. |
| 21 | .420 | 180. | 7.5 | 340. |
| 22 | .420 | 180. | 7.5 | 340. |
| 23 | .450 | 193. | 7.6 | 290. |
| 24 | .540 | 249. | 9.6 | 200. |

DAY = 92

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 9.9 | 490. |
| 2 | .430 | 185. | 10.1 | 490. |
| 3 | .440 | 189. | 10.1 | 490. |
| 4 | .530 | 228. | 10.1 | 490. |
| 5 | .640 | 275. | 10.2 | 490. |
| 6 | .600 | 258. | 9.7 | 490. |
| 7 | .470 | 202. | 7.3 | 490. |
| 8 | .440 | 189. | 6.3 | 490. |
| 9 | .540 | 232. | 7.0 | 495. |
| 10 | .580 | 249. | 6.9 | 500. |
| 11 | .520 | 223. | 7.0 | 495. |
| 12 | .520 | 223. | 7.0 | 495. |
| 13 | .530 | 228. | 7.0 | 490. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .370 | 159. | .8 | 385. |
| 16 | .370 | 159. | .8 | 420. |
| 17 | .370 | 159. | .8 | 485. |
| 18 | .370 | 159. | .8 | 485. |
| 19 | .360 | 155. | .8 | 370. |
| 20 | .350 | 150. | .9 | 340. |
| 21 | .390 | 168. | 1.2 | 340. |
| 22 | .400 | 172. | 1.6 | 340. |
| 23 | .400 | 172. | 2.0 | 290. |
| 24 | .380 | 163. | 3.3 | 200. |

DAY = 93



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 4.0 | 180. |
| 2 | .380 | 163. | 4.0 | 180. |
| 3 | .380 | 163. | 4.0 | 180. |
| 4 | .380 | 163. | 4.0 | 180. |
| 5 | .380 | 163. | 4.0 | 180. |
| 6 | .350 | 150. | 3.4 | 180. |
| 7 | .380 | 163. | 1.5 | 480. |
| 8 | .500 | 215. | 6.8 | 390. |
| 9 | .510 | 219. | 6.9 | 390. |
| 10 | .520 | 223. | 6.9 | 390. |
| 11 | .580 | 249. | 6.8 | 390. |
| 12 | .580 | 249. | 6.7 | 390. |
| 13 | .720 | 309. | 7.7 | 390. |
| 14 | .770 | 331. | 7.9 | 390. |
| 15 | .770 | 331. | 7.9 | 390. |
| 16 | .770 | 331. | 7.9 | 388. |
| 17 | .780 | 335. | 7.9 | 388. |
| 18 | .790 | 339. | 8.0 | 388. |
| 19 | .770 | 331. | 8.0 | 388. |
| 20 | .620 | 266. | 8.0 | 355. |
| 21 | .630 | 271. | 8.0 | 365. |
| 22 | .620 | 266. | 7.8 | 322. |
| 23 | .610 | 262. | 7.7 | 322. |
| 24 | .630 | 271. | 7.8 | 225. |

DAY = 94

| HOUR | NOx LB/10**6 BTU | NOx NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 7.8 | 332. |
| 2 | .630 | 271. | 7.9 | 333. |
| 3 | .630 | 271. | 7.8 | 333. |
| 4 | .630 | 271. | 7.8 | 332. |
| 5 | .630 | 271. | 7.8 | 332. |
| 6 | .630 | 271. | 7.8 | 335. |
| 7 | .570 | 245. | 7.2 | 415. |
| 8 | .570 | 245. | 6.5 | 465. |
| 9 | .590 | 253. | 6.5 | 420. |
| 10 | .620 | 266. | 6.8 | 420. |
| 11 | .600 | 258. | 6.8 | 420. |
| 12 | .580 | 249. | 6.8 | 420. |
| 13 | .600 | 258. | 6.7 | 420. |
| 14 | .600 | 258. | 6.7 | 420. |
| 15 | .600 | 258. | 6.8 | 420. |
| 16 | .600 | 258. | 6.8 | 418. |
| 17 | .620 | 266. | 6.8 | 418. |
| 18 | .630 | 271. | 6.8 | 418. |
| 19 | .640 | 275. | 6.8 | 418. |
| 20 | .620 | 266. | 6.9 | 418. |
| 21 | .630 | 271. | 6.8 | 418. |
| 22 | .640 | 275. | 6.8 | 418. |
| 23 | .640 | 275. | 6.8 | 418. |
| 24 | .660 | 284. | 6.8 | 420. |

APPENDIX C

OKLAHOMA GAS & ELECTRIC

MUSKOGEE STATION - UNIT 4

Input Data - Revised Analysis

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

DATA SUBMITTED BY OKLAHOMA GAS AND ELECTRIC MUSKOGEE STATION

UNIT 4  SUBBITUMINOUS COAL  NOX MON. REL. ACC. = 10.9 PC

DAY 1 IS OCTOBER 15, 1980  DAY 94 IS JANUARY 16, 1981

550 MWE, COMBUSTION ENGINEERING BOILER WITH OVERFIRE AIR

COAL PROXIMATE 8815+-578TU/LB, 0.337+-0.037 PC SULFUR,

4.86+-0.371 PC ASH, 27.73+-0.36 PC MOISTURE

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 10.0 | 180. |
| 2 | .460 | 198. | 10.0 | 180. |
| 3 | .460 | 198. | 10.0 | 180. |
| 4 | .450 | 193. | 10.0 | 180. |
| 5 | .450 | 193. | 10.0 | 180. |
| 6 | .450 | 193. | 10.0 | 178. |
| 7 | .450 | 193. | 9.7 | 220. |
| 8 | .540 | 232. | 8.1 | 305. |
| 9 | .520 | 223. | 8.6 | 225. |
| 10 | .420 | 180. | 9.9 | 180. |
| 11 | .360 | 155. | 10.0 | 180. |
| 12 | .350 | 150. | 10.0 | 180. |
| 13 | .350 | 150. | 10.0 | 180. |
| 14 | .340 | 146. | 9.8 | 180. |
| 15 | .340 | 146. | 9.8 | 180. |
| 16 | .350 | 150. | 10.0 | 180. |
| 17 | .350 | 150. | 10.0 | 180. |
| 18 | .360 | 155. | 10.0 | 180. |
| 19 | .350 | 150. | 10.0 | 180. |
| 20 | .350 | 150. | 10.0 | 180. |
| 21 | .350 | 150. | 10.0 | 180. |
| 22 | .350 | 150. | 10.0 | 180. |
| 23 | .350 | 150. | 10.0 | 180. |
| 24 | .360 | 155. | 10.0 | 180. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 10.0 | 180. |
| 2 | .360 | 155. | 9.9 | 180. |
| 3 | .350 | 150. | 9.9 | 180. |
| 4 | .340 | 146. | 10.0 | 182. |
| 5 | .330 | 142. | 9.9 | 182. |
| 6 | .340 | 146. | 9.9 | 182. |
| 7 | .400 | 172. | 9.7 | 182. |
| 8 | .400 | 172. | 9.9 | 180. |
| 9 | .440 | 189. | 9.8 | 180. |
| 10 | .400 | 172. | 9.8 | 180. |
| 11 | .400 | 172. | 9.8 | 180. |
| 12 | .390 | 168. | 9.8 | 180. |
| 13 | .380 | 163. | 9.7 | 180. |
| 14 | .400 | 172. | 9.9 | 180. |
| 15 | .420 | 180. | 10.0 | 180. |
| 16 | .410 | 176. | 10.0 | 180. |
| 17 | .400 | 172. | 10.0 | 180. |
| 18 | .390 | 168. | 9.9 | 180. |
| 19 | .390 | 168. | 10.0 | 180. |
| 20 | .390 | 168. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 21 | .390 | 168. | 9.9 | 180. |
| 22 | .390 | 168. | 9.9 | 180. |
| 23 | .390 | 168. | 9.8 | 180. |
| 24 | .380 | 163. | 9.8 | 182. |

DAY = 3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 9.9 | 180. |
| 2 | .410 | 176. | 9.9 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .410 | 176. | 9.9 | 180. |
| 5 | .410 | 176. | 9.9 | 180. |
| 6 | .420 | 180. | 9.9 | 182. |
| 7 | .440 | 189. | 9.4 | 228. |
| 8 | .460 | 198. | 8.8 | 275. |
| 9 | .480 | 206. | 8.6 | 300. |
| 10 | .410 | 176. | 7.8 | 325. |
| 11 | .410 | 176. | 7.7 | 325. |
| 12 | .420 | 180. | 7.8 | 325. |
| 13 | .430 | 185. | 7.8 | 325. |
| 14 | .440 | 189. | 7.9 | 325. |
| 15 | .450 | 193. | 7.9 | 325. |
| 16 | .450 | 193. | 7.9 | 325. |
| 17 | .470 | 202. | 8.2 | 250. |
| 18 | .540 | 232. | 9.5 | 225. |
| 19 | .550 | 236. | 9.5 | 225. |
| 20 | .540 | 232. | 9.4 | 225. |
| 21 | .540 | 232. | 9.4 | 225. |
| 22 | .560 | 241. | 9.5 | 225. |
| 23 | .560 | 241. | 9.5 | 225. |
| 24 | .560 | 241. | 9.5 | 225. |

DAY = 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 9.6 | 195. |
| 2 | .390 | 168. | 10.0 | 180. |
| 3 | .380 | 163. | 10.0 | 180. |
| 4 | .390 | 168. | 10.0 | 180. |
| 5 | .400 | 172. | 10.0 | 180. |
| 6 | .400 | 172. | 10.0 | 180. |
| 7 | .400 | 172. | 10.0 | 180. |
| 8 | .390 | 168. | 10.0 | 180. |
| 9 | .360 | 155. | 10.0 | 180. |
| 10 | .390 | 168. | 10.0 | 180. |
| 11 | .380 | 163. | 10.0 | 180. |
| 12 | .380 | 163. | 10.0 | 180. |
| 13 | .370 | 159. | 10.0 | 180. |
| 14 | .380 | 163. | 10.0 | 180. |
| 15 | .370 | 159. | 10.0 | 180. |
| 16 | .380 | 163. | 10.0 | 180. |
| 17 | .370 | 159. | 10.0 | 180. |
| 18 | .360 | 155. | 10.0 | 180. |
| 19 | .360 | 155. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 20 | .380 | 163. | 10.0 | 180. |
| 21 | .380 | 163. | 10.0 | 180. |
| 22 | .390 | 168. | 10.0 | 180. |
| 23 | .400 | 172. | 10.0 | 180. |
| 24 | -1.000 | -430. | 10.0 | 180. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.0 | 180. |
| 2 | .420 | 180. | 10.1 | 180. |
| 3 | .420 | 180. | 10.1 | 180. |
| 4 | .420 | 180. | 10.0 | 180. |
| 5 | .410 | 176. | 10.0 | 180. |
| 6 | .410 | 176. | 10.0 | 180. |
| 7 | .460 | 198. | 9.4 | 280. |
| 8 | .490 | 210. | 7.8 | 325. |
| 9 | .490 | 210. | 7.7 | 325. |
| 10 | .500 | 215. | 7.7 | 330. |
| 11 | .500 | 215. | 7.7 | 330. |
| 12 | .500 | 215. | 7.7 | 330. |
| 13 | .490 | 210. | 7.7 | 330. |
| 14 | .490 | 210. | 7.7 | 330. |
| 15 | .480 | 206. | 7.7 | 330. |
| 16 | .470 | 202. | 7.7 | 330. |
| 17 | .450 | 193. | 7.8 | 330. |
| 18 | .450 | 193. | 7.8 | 330. |
| 19 | .450 | 193. | 7.8 | 330. |
| 20 | .460 | 198. | 7.8 | 330. |
| 21 | .470 | 202. | 7.8 | 330. |
| 22 | .480 | 206. | 7.9 | 330. |
| 23 | .490 | 210. | 7.9 | 330. |
| 24 | .510 | 219. | 8.7 | 230. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 9.5 | 230. |
| 2 | .520 | 223. | 9.7 | 180. |
| 3 | .440 | 189. | 10.0 | 180. |
| 4 | .430 | 185. | 10.0 | 180. |
| 5 | .440 | 189. | 10.1 | 180. |
| 6 | .430 | 185. | 10.0 | 190. |
| 7 | .520 | 223. | 9.3 | 230. |
| 8 | .530 | 228. | 9.3 | 230. |
| 9 | .500 | 215. | 8.8 | 280. |
| 10 | .470 | 202. | 8.1 | 330. |
| 11 | .460 | 198. | 7.8 | 330. |
| 12 | .550 | 236. | 8.7 | 270. |
| 13 | .570 | 245. | 9.1 | 260. |
| 14 | .550 | 236. | 8.8 | 320. |
| 15 | .540 | 232. | 8.6 | 280. |
| 16 | .550 | 236. | 8.7 | 280. |
| 17 | .550 | 236. | 8.7 | 280. |
| 18 | .550 | 236. | 8.7 | 280. |

| | | | | |
|---|---|---|---|---|
| 19 | .540 | 232. | 8.7 | 280. |
| 20 | .530 | 228. | 8.7 | 280. |
| 21 | .540 | 232. | 8.6 | 280. |
| 22 | .480 | 206. | 8.9 | 230. |
| 23 | .450 | 193. | 9.4 | 230. |
| 24 | .470 | 202. | 9.5 | 230. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.0 | 175. |
| 2 | .400 | 172. | 10.0 | 175. |
| 3 | .410 | 176. | 10.1 | 175. |
| 4 | .420 | 180. | 10.1 | 175. |
| 5 | .420 | 180. | 10.1 | 175. |
| 6 | .420 | 180. | 10.1 | 175. |
| 7 | .410 | 176. | 10.1 | 175. |
| 8 | .530 | 228. | 9.4 | 230. |
| 9 | .540 | 232. | 9.1 | 280. |
| 10 | .480 | 206. | 8.2 | 340. |
| 11 | .460 | 198. | 7.4 | 355. |
| 12 | .410 | 176. | 7.4 | 355. |
| 13 | .410 | 176. | 7.4 | 355. |
| 14 | .420 | 180. | 7.4 | 355. |
| 15 | .420 | 180. | 7.4 | 355. |
| 16 | .450 | 193. | 7.4 | 350. |
| 17 | .480 | 206. | 7.8 | 322. |
| 18 | .490 | 210. | 7.9 | 320. |
| 19 | .490 | 210. | 7.9 | 320. |
| 20 | .480 | 206. | 7.8 | 320. |
| 21 | .500 | 215. | 7.9 | 320. |
| 22 | .430 | 185. | 8.6 | 272. |
| 23 | .440 | 189. | 9.0 | 228. |
| 24 | .580 | 249. | 9.5 | 230. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 10.1 | 175. |
| 2 | .470 | 202. | 10.1 | 175. |
| 3 | .480 | 206. | 10.0 | 175. |
| 4 | .480 | 206. | 10.1 | 175. |
| 5 | .480 | 206. | 10.1 | 175. |
| 6 | .480 | 206. | 10.1 | 175. |
| 7 | .490 | 210. | 10.1 | 175. |
| 8 | .480 | 206. | 10.1 | 175. |
| 9 | .530 | 228. | 9.3 | 290. |
| 10 | .540 | 232. | 8.1 | 330. |
| 11 | .490 | 210. | 7.8 | 300. |
| 12 | .480 | 206. | 9.2 | 230. |
| 13 | .510 | 219. | 9.5 | 230. |
| 14 | .510 | 219. | 9.5 | 230. |
| 15 | .500 | 215. | 9.5 | 230. |
| 16 | .500 | 215. | 9.5 | 232. |
| 17 | .500 | 215. | 9.5 | 234. |

| | | | | |
|---|---|---|---|---|
| 18 | .510 | 219. | 9.6 | 234. |
| 19 | .500 | 215. | 9.6 | 232. |
| 20 | .470 | 202. | 9.0 | 274. |
| 21 | .450 | 193. | 8.9 | 279. |
| 22 | .460 | 198. | 8.8 | 300. |
| 23 | .460 | 198. | 8.4 | 300. |
| 24 | .550 | 236. | 9.3 | 220. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 9.9 | 175. |
| 2 | .460 | 198. | 10.1 | 175. |
| 3 | .490 | 210. | 10.1 | 180. |
| 4 | .490 | 210. | 10.1 | 180. |
| 5 | .500 | 215. | 10.1 | 180. |
| 6 | .490 | 210. | 10.1 | 180. |
| 7 | .490 | 210. | 10.1 | 180. |
| 8 | .490 | 210. | 9.8 | 235. |
| 9 | .480 | 206. | 7.8 | 375. |
| 10 | .470 | 202. | 7.1 | 380. |
| 11 | .460 | 198. | 7.1 | 380. |
| 12 | .480 | 206. | 7.1 | 380. |
| 13 | .530 | 228. | 7.1 | 380. |
| 14 | .550 | 236. | 7.2 | 350. |
| 15 | .600 | 258. | 8.1 | 240. |
| 16 | .600 | 258. | 9.0 | 202. |
| 17 | .630 | 271. | 10.0 | 202. |
| 18 | .640 | 275. | 9.8 | 226. |
| 19 | .490 | 210. | 9.3 | 225. |
| 20 | .530 | 228. | 9.2 | 250. |
| 21 | .540 | 232. | 9.2 | 255. |
| 22 | .530 | 228. | 9.5 | 190. |
| 23 | .470 | 202. | 10.1 | 178. |
| 24 | .470 | 202. | 10.1 | 175. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.1 | 175. |
| 2 | .460 | 198. | 10.1 | 175. |
| 3 | .450 | 193. | 10.1 | 175. |
| 4 | .460 | 198. | 10.1 | 180. |
| 5 | .460 | 198. | 10.1 | 180. |
| 6 | .440 | 189. | 10.1 | 180. |
| 7 | .430 | 185. | 10.1 | 180. |
| 8 | .450 | 193. | 10.1 | 280. |
| 9 | .450 | 193. | 9.6 | 280. |
| 10 | .410 | 176. | 8.7 | 280. |
| 11 | .420 | 180. | 8.7 | 280. |
| 12 | .420 | 180. | 8.8 | 280. |
| 13 | .430 | 185. | 8.8 | 280. |
| 14 | .430 | 185. | 8.8 | 280. |
| 15 | .420 | 180. | 8.8 | 280. |
| 16 | .420 | 180. | 8.7 | 280. |

| | | | | |
|---|---|---|---|---|
| 17 | .460 | 198. | 9.3 | 260. |
| 18 | .470 | 202. | 9.4 | 300. |
| 19 | .460 | 198. | 8.4 | 300. |
| 20 | .440 | 189. | 8.3 | 300. |
| 21 | .450 | 193. | 8.3 | 300. |
| 22 | .470 | 202. | 8.4 | 250. |
| 23 | .490 | 210. | 8.6 | 178. |
| 24 | .450 | 193. | 9.9 | 175. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.1 | 175. |
| 2 | .460 | 198. | 10.1 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .400 | 172. | 10.1 | 180. |
| 5 | .400 | 172. | 10.0 | 180. |
| 6 | .400 | 172. | 10.1 | 180. |
| 7 | .400 | 172. | 10.1 | 375. |
| 8 | .460 | 198. | 8.0 | 425. |
| 9 | .480 | 206. | 6.8 | 420. |
| 10 | .460 | 198. | 6.7 | 420. |
| 11 | .460 | 198. | 6.7 | 430. |
| 12 | .430 | 185. | 6.7 | 420. |
| 13 | .430 | 185. | 6.8 | 425. |
| 14 | .440 | 189. | 6.5 | 430. |
| 15 | .430 | 185. | 6.5 | 430. |
| 16 | .430 | 185. | 6.5 | 422. |
| 17 | .440 | 189. | 6.5 | 422. |
| 18 | .430 | 185. | 6.5 | 422. |
| 19 | .420 | 180. | 6.5 | 422. |
| 20 | .430 | 185. | 6.6 | 420. |
| 21 | .460 | 198. | 6.6 | 420. |
| 22 | .480 | 206. | 6.9 | 365. |
| 23 | .450 | 193. | 8.6 | 274. |
| 24 | .440 | 189. | 8.8 | 270. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 8.4 | 295. |
| 2 | .600 | 258. | 8.4 | 295. |
| 3 | -1.000 | -430. | 8.3 | 295. |
| 4 | -1.000 | -430. | 8.4 | 295. |
| 5 | -1.000 | -430. | 7.5 | 415. |
| 6 | -1.000 | -430. | 6.9 | 415. |
| 7 | -1.000 | -430. | 6.9 | 420. |
| 8 | -1.000 | -430. | 6.9 | 420. |
| 9 | .540 | 232. | 6.8 | 420. |
| 10 | .470 | 202. | 6.8 | 420. |
| 11 | .570 | 245. | 6.8 | 420. |
| 12 | .620 | 266. | 7.1 | 360. |
| 13 | .660 | 284. | 7.5 | 360. |
| 14 | .670 | 288. | 7.5 | 360. |
| 15 | .680 | 292. | 7.5 | 360. |

| | | | | |
|---|---|---|---|---|
| 16 | .700 | 301. | 7.5 | 360. |
| 17 | .710 | 305. | 7.5 | 360. |
| 18 | .730 | 314. | 7.6 | 360. |
| 19 | .710 | 305. | 7.6 | 355. |
| 20 | .690 | 296. | 7.5 | 355. |
| 21 | .710 | 305. | 7.5 | 355. |
| 22 | .730 | 314. | 7.5 | 355. |
| 23 | .720 | 309. | 7.6 | 320. |
| 24 | .490 | 210. | 8.6 | 275. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 8.9 | 270. |
| 2 | .560 | 241. | 9.6 | 225. |
| 3 | .590 | 253. | 9.6 | 230. |
| 4 | .580 | 249. | 9.5 | 230. |
| 5 | .590 | 253. | 9.6 | 230. |
| 6 | .580 | 249. | 9.6 | 230. |
| 7 | .480 | 206. | 7.4 | 430. |
| 8 | .450 | 193. | 6.8 | 418. |
| 9 | .490 | 210. | 6.8 | 418. |
| 10 | .490 | 210. | 6.8 | 418. |
| 11 | .480 | 206. | 6.8 | 418. |
| 12 | .480 | 206. | 6.8 | 418. |
| 13 | .520 | 223. | 7.0 | 360. |
| 14 | .690 | 296. | 8.6 | 272. |
| 15 | .680 | 292. | 8.8 | 272. |
| 16 | .480 | 206. | 7.2 | 420. |
| 17 | .600 | 258. | 6.7 | 420. |
| 18 | .610 | 262. | 6.8 | 420. |
| 19 | .600 | 258. | 6.7 | 420. |
| 20 | .600 | 258. | 6.8 | 420. |
| 21 | .590 | 253. | 6.8 | 420. |
| 22 | .600 | 258. | 6.8 | 420. |
| 23 | .570 | 245. | 6.9 | 350. |
| 24 | .660 | 284. | 8.3 | 265. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 10.0 | 180. |
| 2 | .360 | 155. | 10.1 | 180. |
| 3 | .430 | 185. | 10.0 | 180. |
| 4 | .460 | 198. | 10.0 | 180. |
| 5 | .470 | 202. | 10.0 | 180. |
| 6 | .450 | 193. | 10.0 | 200. |
| 7 | .480 | 206. | 9.0 | 280. |
| 8 | .450 | 193. | 8.7 | 276. |
| 9 | .460 | 198. | 8.7 | 276. |
| 10 | .470 | 202. | 8.7 | 278. |
| 11 | .460 | 198. | 8.7 | 278. |
| 12 | .430 | 185. | 8.7 | 280. |
| 13 | .420 | 180. | 8.8 | 280. |
| 14 | .510 | 219. | 9.5 | 230. |

| | | | | |
|---|---|---|---|---|
| 15 | .510 | 219. | 9.5 | 230. |
| 16 | .510 | 219. | 9.5 | 230. |
| 17 | .510 | 219. | 9.4 | 230. |
| 18 | .520 | 223. | 9.4 | 230. |
| 19 | .520 | 223. | 9.4 | 230. |
| 20 | .510 | 219. | 9.4 | 230. |
| 21 | .520 | 223. | 9.4 | 230. |
| 22 | .530 | 228. | 9.5 | 230. |
| 23 | .510 | 219. | 9.9 | 175. |
| 24 | .460 | 198. | 10.0 | 175. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.0 | 175. |
| 2 | .430 | 185. | 10.0 | 175. |
| 3 | .430 | 185. | 10.0 | 175. |
| 4 | .430 | 185. | 10.1 | 175. |
| 5 | .430 | 185. | 10.1 | 175. |
| 6 | .530 | 228. | 10.0 | 175. |
| 7 | .390 | 168. | 10.1 | 175. |
| 8 | .390 | 168. | 10.0 | 178. |
| 9 | .500 | 215. | 8.8 | 270. |
| 10 | .520 | 223. | 8.8 | 270. |
| 11 | .510 | 219. | 8.8 | 270. |
| 12 | .490 | 210. | 8.8 | 270. |
| 13 | .510 | 219. | 8.8 | 270. |
| 14 | .520 | 223. | 8.8 | 270. |
| 15 | .510 | 219. | 8.8 | 270. |
| 16 | .510 | 219. | 8.8 | 275. |
| 17 | .510 | 219. | 8.8 | 275. |
| 18 | .510 | 219. | 8.8 | 275. |
| 19 | -1.000 | -430. | 8.7 | 275. |
| 20 | -1.000 | -430. | 8.7 | 275. |
| 21 | .500 | 215. | 8.7 | 275. |
| 22 | .490 | 210. | 8.7 | 275. |
| 23 | -1.000 | -430. | 8.9 | 250. |
| 24 | -1.000 | -430. | 9.9 | 175. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 10.1 | 175. |
| 2 | .440 | 189. | 10.1 | 175. |
| 3 | .450 | 193. | 10.1 | 175. |
| 4 | .440 | 189. | 10.0 | 175. |
| 5 | .460 | 198. | 10.1 | 175. |
| 6 | .470 | 202. | 9.3 | 300. |
| 7 | .470 | 202. | 7.3 | 430. |
| 8 | .490 | 210. | 6.6 | 418. |
| 9 | .560 | 241. | 6.6 | 418. |
| 10 | .560 | 241. | 6.6 | 420. |
| 11 | .550 | 236. | 6.6 | 420. |
| 12 | .570 | 245. | 6.6 | 416. |
| 13 | .560 | 241. | 6.6 | 416. |

| | | | | |
|---|---|---|---|---|
| 14 | .550 | 236. | 6.6 | 415. |
| 15 | .550 | 236. | 6.5 | 415. |
| 16 | .580 | 249. | 6.5 | 420. |
| 17 | .580 | 249. | 6.6 | 420. |
| 18 | .580 | 249. | 6.6 | 420. |
| 19 | .590 | 253. | 6.6 | 420. |
| 20 | .590 | 253. | 6.6 | 420. |
| 21 | .600 | 258. | 6.6 | 420. |
| 22 | .590 | 253. | 6.6 | 420. |
| 23 | .570 | 245. | 6.6 | 420. |
| 24 | .590 | 253. | 6.7 | 400. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 8.6 | 235. |
| 2 | .380 | 163. | 10.0 | 175. |
| 3 | .420 | 180. | 10.0 | 175. |
| 4 | .420 | 180. | 10.0 | 175. |
| 5 | .530 | 228. | 9.1 | 330. |
| 6 | .600 | 258. | 7.0 | 425. |
| 7 | .620 | 266. | 6.7 | 425. |
| 8 | .570 | 245. | 6.5 | 418. |
| 9 | .590 | 253. | 6.5 | 415. |
| 10 | .570 | 245. | 6.5 | 415. |
| 11 | .570 | 245. | 6.5 | 420. |
| 12 | .560 | 241. | 6.5 | 420. |
| 13 | .570 | 245. | 6.5 | 420. |
| 14 | .570 | 245. | 6.5 | 420. |
| 15 | .570 | 245. | 6.5 | 420. |
| 16 | .550 | 236. | 6.5 | 420. |
| 17 | .550 | 236. | 6.5 | 420. |
| 18 | .560 | 241. | 6.5 | 420. |
| 19 | .600 | 258. | 6.6 | 420. |
| 20 | .610 | 262. | 6.6 | 420. |
| 21 | .470 | 202. | 6.6 | 420. |
| 22 | .460 | 198. | 6.6 | 420. |
| 23 | .510 | 219. | 6.6 | 420. |
| 24 | .500 | 215. | 7.5 | 260. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -.470 | -202. | -9.6 | 0. |
| 2 | .460 | 198. | 7.8 | 330. |
| 3 | .470 | 202. | 7.8 | 330. |
| 4 | .380 | 163. | 7.4 | 380. |
| 5 | .360 | 155. | 7.2 | 380. |
| 6 | .390 | 168. | 7.0 | 425. |
| 7 | .550 | 236. | 6.7 | 425. |
| 8 | .560 | 241. | 6.7 | 425. |
| 9 | .550 | 236. | 6.7 | 425. |
| 10 | .540 | 232. | 6.6 | 425. |
| 11 | .550 | 236. | 6.7 | 425. |
| 12 | .550 | 236. | 6.5 | 420. |

| | | | | |
|---|---|---|---|---|
| 13 | .480 | 206. | 6.9 | 375. |
| 14 | .420 | 180. | 7.3 | 350. |
| 15 | .440 | 189. | 7.4 | 350. |
| 16 | .450 | 193. | 7.4 | 350. |
| 17 | .470 | 202. | 7.4 | 350. |
| 18 | .470 | 202. | 8.6 | 235. |
| 19 | .540 | 232. | 9.3 | 225. |
| 20 | .520 | 223. | 9.0 | 280. |
| 21 | .490 | 210. | 8.5 | 280. |
| 22 | .510 | 219. | 8.5 | 280. |
| 23 | .510 | 219. | 8.5 | 275. |
| 24 | .530 | 228. | 8.7 | 260. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.1 | 175. |
| 2 | .380 | 163. | 10.1 | 175. |
| 3 | .410 | 176. | 10.1 | 175. |
| 4 | .410 | 176. | 10.0 | 175. |
| 5 | .410 | 176. | 10.0 | 175. |
| 6 | .420 | 180. | 9.8 | 230. |
| 7 | .490 | 210. | 7.6 | 420. |
| 8 | .530 | 228. | 6.4 | 422. |
| 9 | .580 | 249. | 6.8 | 340. |
| 10 | .580 | 249. | 7.6 | 325. |
| 11 | .560 | 241. | 7.6 | 325. |
| 12 | .520 | 223. | 7.5 | 360. |
| 13 | .460 | 198. | 7.0 | 374. |
| 14 | .450 | 193. | 6.9 | 374. |
| 15 | .530 | 228. | 7.5 | 324. |
| 16 | .530 | 228. | 7.5 | 320. |
| 17 | -1.000 | -430. | 7.3 | 360. |
| 18 | -1.000 | -430. | 6.5 | 410. |
| 19 | .440 | 189. | 6.4 | 410. |
| 20 | .440 | 189. | 6.4 | 410. |
| 21 | .460 | 198. | 6.5 | 410. |
| 22 | .480 | 206. | 7.4 | 315. |
| 23 | .480 | 206. | 8.6 | 230. |
| 24 | .440 | 189. | 9.4 | 175. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.0 | 175. |
| 2 | .420 | 180. | 10.0 | 175. |
| 3 | .420 | 180. | 10.0 | 175. |
| 4 | .430 | 185. | 9.9 | 175. |
| 5 | .440 | 189. | 10.0 | 175. |
| 6 | .440 | 189. | 9.9 | 175. |
| 7 | .440 | 189. | 9.1 | 265. |
| 8 | .600 | 258. | 7.8 | 345. |
| 9 | .510 | 219. | 6.7 | 420. |
| 10 | .480 | 206. | 6.4 | 420. |
| 11 | .490 | 210. | 6.5 | 420. |

| | | | | |
|---|---|---|---|---|
| 12 | .490 | 210. | 6.5 | 420. |
| 13 | .500 | 215. | 6.4 | 420. |
| 14 | .490 | 210. | 6.4 | 420. |
| 15 | .470 | 202. | 6.4 | 420. |
| 16 | .480 | 206. | 6.4 | 415. |
| 17 | .480 | 206. | 6.4 | 418. |
| 18 | .470 | 202. | 6.4 | 415. |
| 19 | .480 | 206. | 6.5 | 350. |
| 20 | .560 | 241. | 7.7 | 320. |
| 21 | .590 | 253. | 7.8 | 320. |
| 22 | .550 | 236. | 8.3 | 250. |
| 23 | .540 | 232. | 9.3 | 225. |
| 24 | .460 | 198. | 9.8 | 175. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.1 | 176. |
| 2 | .380 | 163. | 10.1 | 178. |
| 3 | .390 | 168. | 10.0 | 176. |
| 4 | .400 | 172. | 10.0 | 178. |
| 5 | .400 | 172. | 10.0 | 178. |
| 6 | .480 | 206. | 9.8 | 200. |
| 7 | .590 | 253. | 9.5 | 200. |
| 8 | .620 | 266. | 9.5 | 200. |
| 9 | .560 | 241. | 8.5 | 275. |
| 10 | .590 | 253. | 8.5 | 275. |
| 11 | .590 | 253. | 8.5 | 275. |
| 12 | .540 | 232. | 7.8 | 325. |
| 13 | .530 | 228. | 6.9 | 420. |
| 14 | .530 | 228. | 6.3 | 420. |
| 15 | .530 | 228. | 6.3 | 415. |
| 16 | .530 | 228. | 6.4 | 370. |
| 17 | .490 | 210. | 7.6 | 315. |
| 18 | .520 | 223. | 7.6 | 325. |
| 19 | .430 | 185. | 6.9 | 370. |
| 20 | .420 | 180. | 6.9 | 370. |
| 21 | .440 | 189. | 7.7 | 275. |
| 22 | .440 | 189. | 9.5 | 180. |
| 23 | .420 | 180. | 10.0 | 180. |
| 24 | .410 | 176. | 10.0 | 180. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.0 | 180. |
| 2 | .400 | 172. | 10.0 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .410 | 176. | 9.9 | 180. |
| 5 | .420 | 180. | 10.0 | 180. |
| 6 | .420 | 180. | 10.0 | 178. |
| 7 | .430 | 185. | 10.0 | 178. |
| 8 | .430 | 185. | 10.0 | 180. |
| 9 | .400 | 172. | 9.9 | 230. |
| 10 | .470 | 202. | 9.0 | 230. |

| | | | | |
|---|---|---|---|---|
| 11 | .500 | 215. | 9.1 | 230. |
| 12 | .460 | 198. | 9.4 | 180. |
| 13 | .390 | 168. | 9.9 | 180. |
| 14 | .410 | 176. | 10.0 | 180. |
| 15 | .410 | 176. | 10.0 | 180. |
| 16 | .410 | 176. | 10.0 | 165. |
| 17 | .410 | 176. | 10.0 | 185. |
| 18 | .480 | 206. | 9.2 | 275. |
| 19 | .590 | 253. | 8.5 | 275. |
| 20 | .580 | 249. | 8.5 | 275. |
| 21 | .610 | 262. | 9.2 | 225. |
| 22 | .510 | 219. | 10.0 | 175. |
| 23 | .510 | 219. | 10.0 | 175. |
| 24 | .510 | 219. | 10.0 | 175. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.1 | 178. |
| 2 | .470 | 202. | 10.1 | 178. |
| 3 | .470 | 202. | 10.1 | 178. |
| 4 | .470 | 202. | 10.1 | 178. |
| 5 | .480 | 206. | 10.1 | 178. |
| 6 | .500 | 215. | 9.5 | 265. |
| 7 | .480 | 206. | 7.1 | 412. |
| 8 | .510 | 219. | 6.5 | 412. |
| 9 | .510 | 219. | 6.5 | 412. |
| 10 | .510 | 219. | 6.6 | 412. |
| 11 | .560 | 241. | 6.6 | 412. |
| 12 | .590 | 253. | 6.6 | 412. |
| 13 | .580 | 249. | 6.6 | 412. |
| 14 | .580 | 249. | 6.6 | 412. |
| 15 | .560 | 241. | 6.6 | 412. |
| 16 | .560 | 241. | 6.6 | 415. |
| 17 | .580 | 249. | 6.7 | 415. |
| 18 | .580 | 249. | 6.7 | 415. |
| 19 | -1.000 | -430. | 6.6 | 415. |
| 20 | -1.000 | -430. | 6.7 | 415. |
| 21 | -1.000 | -430. | 6.7 | 415. |
| 22 | -1.000 | -430. | 6.7 | 400. |
| 23 | -1.000 | -430. | 7.5 | 300. |
| 24 | -1.000 | -430. | 9.4 | 200. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 10.1 | 178. |
| 2 | .440 | 189. | 10.1 | 178. |
| 3 | .420 | 180. | 10.1 | 178. |
| 4 | .430 | 185. | 10.1 | 178. |
| 5 | .440 | 189. | 10.1 | 178. |
| 6 | .440 | 189. | 9.8 | 220. |
| 7 | .560 | 241. | 7.6 | 358. |
| 8 | .590 | 253. | 7.3 | 358. |
| 9 | .440 | 189. | 5.8 | 520. |

| | | | | |
|---|---|---|---|---|
| 10 | .380 | 163. | 5.2 | 520. |
| 11 | .370 | 159. | 5.2 | 520. |
| 12 | .360 | 155. | 5.1 | 520. |
| 13 | .380 | 163. | 5.1 | 520. |
| 14 | .380 | 163. | 5.1 | 520. |
| 15 | -1.000 | -430. | 5.0 | 520. |
| 16 | -1.000 | -430. | 5.4 | 515. |
| 17 | .420 | 180. | 5.0 | 515. |
| 18 | .410 | 176. | 5.1 | 515. |
| 19 | .400 | 172. | 5.1 | 515. |
| 20 | .400 | 172. | 5.1 | 515. |
| 21 | .410 | 176. | 5.2 | 430. |
| 22 | .450 | 193. | 6.6 | 300. |
| 23 | .420 | 180. | 8.2 | 280. |
| 24 | .410 | 176. | 8.8 | 260. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 10.0 | 178. |
| 2 | .450 | 193. | 10.1 | 178. |
| 3 | .460 | 198. | 10.1 | 175. |
| 4 | .450 | 193. | 10.1 | 178. |
| 5 | .460 | 198. | 10.0 | 178. |
| 6 | .530 | 228. | 9.1 | 250. |
| 7 | .500 | 215. | 7.0 | 458. |
| 8 | .460 | 198. | 5.2 | 525. |
| 9 | .490 | 210. | 5.1 | 527. |
| 10 | .480 | 206. | 5.2 | 528. |
| 11 | .500 | 215. | 5.2 | 525. |
| 12 | .510 | 219. | 5.2 | 525. |
| 13 | .510 | 219. | 5.2 | 525. |
| 14 | .510 | 219. | 5.2 | 525. |
| 15 | .520 | 223. | 5.1 | 525. |
| 16 | .480 | 206. | 5.0 | 530. |
| 17 | .450 | 193. | 5.1 | 530. |
| 18 | .460 | 198. | 5.2 | 530. |
| 19 | .480 | 206. | 5.1 | 530. |
| 20 | .490 | 210. | 5.1 | 530. |
| 21 | .480 | 206. | 5.1 | 537. |
| 22 | .470 | 202. | 5.3 | 470. |
| 23 | .570 | 245. | 6.3 | 430. |
| 24 | .510 | 219. | 8.1 | 260. |

DAY = 32

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 9.9 | 178. |
| 2 | .440 | 189. | 10.1 | 178. |
| 3 | .450 | 193. | 10.1 | 175. |
| 4 | .460 | 198. | 10.1 | 178. |
| 5 | .460 | 198. | 10.1 | 178. |
| 6 | .450 | 193. | 10.1 | 250. |
| 7 | .470 | 202. | 9.0 | 458. |
| 8 | .550 | 236. | 7.6 | 525. |

| | | | | |
|---|---|---|---|---|
| 9 | .590 | 253. | 7.6 | 527. |
| 10 | .640 | 275. | 7.2 | 528. |
| 11 | .660 | 284. | 7.1 | 525. |
| 12 | .660 | 284. | 7.1 | 525. |
| 13 | .590 | 253. | 7.6 | 525. |
| 14 | .470 | 202. | 8.3 | 525. |
| 15 | .420 | 180. | 8.6 | 525. |
| 16 | .430 | 185. | 8.6 | 530. |
| 17 | .450 | 193. | 8.6 | 530. |
| 18 | .500 | 215. | 8.0 | 530. |
| 19 | .430 | 185. | 6.5 | 530. |
| 20 | .430 | 185. | 6.6 | 530. |
| 21 | -1.000 | -430. | 6.9 | 537. |
| 22 | -1.000 | -430. | 7.5 | 470. |
| 23 | .510 | 219. | 7.4 | 430. |
| 24 | .480 | 206. | 8.6 | 260. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 7.1 | 380. |
| 2 | .620 | 266. | 7.1 | 380. |
| 3 | -1.000 | -430. | 7.2 | 305. |
| 4 | -1.000 | -430. | 8.5 | 255. |
| 5 | .450 | 193. | 8.9 | 255. |
| 6 | .460 | 198. | 7.9 | 480. |
| 7 | -1.000 | -430. | 5.3 | 520. |
| 8 | -1.000 | -430. | 5.2 | 520. |
| 9 | .490 | 210. | 5.2 | 520. |
| 10 | .530 | 228. | 5.5 | 520. |
| 11 | .540 | 232. | 5.4 | 520. |
| 12 | .500 | 215. | 5.4 | 520. |
| 13 | .510 | 219. | 5.3 | 520. |
| 14 | .530 | 228. | 5.2 | 520. |
| 15 | .540 | 232. | 5.2 | 525. |
| 16 | .530 | 228. | 5.2 | 520. |
| 17 | .470 | 202. | 5.2 | 525. |
| 18 | .460 | 198. | 5.2 | 520. |
| 19 | .480 | 206. | 5.2 | 520. |
| 20 | .500 | 215. | 5.2 | 520. |
| 21 | .470 | 202. | 5.2 | 520. |
| 22 | .470 | 202. | 5.2 | 520. |
| 23 | .480 | 206. | 5.2 | 520. |
| 24 | .500 | 215. | 5.2 | 520. |

DAY = 36

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 5.2 | 485. |
| 2 | .490 | 210. | 5.9 | 475. |
| 3 | .500 | 215. | 5.9 | 475. |
| 4 | .510 | 219. | 5.9 | 475. |
| 5 | -1.000 | -430. | 5.9 | 475. |
| 6 | -1.000 | -430. | 5.4 | 518. |
| 7 | .450 | 193. | 5.3 | 518. |

| | | | | |
|---|---|---|---|---|
| 8 | .460 | 198. | 5.3 | 520. |
| 9 | -1.000 | -430. | 5.3 | 520. |
| 10 | -1.000 | -430. | 5.3 | 520. |
| 11 | .440 | 189. | 5.3 | 520. |
| 12 | .500 | 215. | 6.1 | 430. |
| 13 | .540 | 232. | 6.4 | 430. |
| 14 | .540 | 232. | 6.4 | 430. |
| 15 | .550 | 236. | 6.4 | 430. |
| 16 | .560 | 241. | 6.3 | 428. |
| 17 | .560 | 241. | 6.4 | 428. |
| 18 | .490 | 210. | 6.0 | 492. |
| 19 | .440 | 189. | 5.4 | 510. |
| 20 | .450 | 193. | 5.4 | 510. |
| 21 | .460 | 198. | 5.4 | 510. |
| 22 | .470 | 202. | 5.5 | 510. |
| 23 | .470 | 202. | 5.5 | 510. |
| 24 | .480 | 206. | 5.5 | 510. |

DAY = 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 6.0 | 460. |
| 2 | .540 | 232. | 6.1 | 460. |
| 3 | .560 | 241. | 6.1 | 460. |
| 4 | .580 | 249. | 6.1 | 460. |
| 5 | .570 | 245. | 6.0 | 460. |
| 6 | .500 | 215. | 5.5 | 510. |
| 7 | .490 | 210. | 5.4 | 510. |
| 8 | .470 | 202. | 5.4 | 515. |
| 9 | .490 | 210. | 5.3 | 515. |
| 10 | .520 | 223. | 5.2 | 520. |
| 11 | .440 | 189. | 5.3 | 520. |
| 12 | .450 | 193. | 5.3 | 520. |
| 13 | .480 | 206. | 5.2 | 520. |
| 14 | .500 | 215. | 5.1 | 520. |
| 15 | .490 | 210. | 5.1 | 520. |
| 16 | .500 | 215. | 5.1 | 520. |
| 17 | .480 | 206. | 5.1 | 520. |
| 18 | .420 | 180. | 5.2 | 520. |
| 19 | .430 | 185. | 5.2 | 518. |
| 20 | .440 | 189. | 5.1 | 515. |
| 21 | .440 | 189. | 5.1 | 515. |
| 22 | .430 | 185. | 5.2 | 520. |
| 23 | .430 | 185. | 5.3 | 520. |
| 24 | .440 | 189. | 5.2 | 518. |

DAY = 38

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 5.2 | 510. |
| 2 | .440 | 189. | 5.3 | 510. |
| 3 | .450 | 193. | 5.3 | 510. |
| 4 | .460 | 198. | 5.3 | 510. |
| 5 | .470 | 202. | 5.3 | 510. |
| 6 | .450 | 193. | 5.3 | 510. |

| | | | | |
|---|---|---|---|---|
| 7 | .430 | 185. | 5.3 | 510. |
| 8 | .440 | 189. | 5.3 | 510. |
| 9 | .450 | 193. | 5.3 | 505. |
| 10 | .450 | 193. | 5.3 | 505. |
| 11 | .460 | 198. | 5.3 | 505. |
| 12 | .470 | 202. | 5.3 | 505. |
| 13 | .510 | 219. | 5.3 | 505. |
| 14 | .510 | 219. | 5.3 | 505. |
| 15 | .530 | 228. | 5.3 | 505. |
| 16 | .530 | 228. | 5.2 | 505. |
| 17 | .490 | 210. | 5.2 | 512. |
| 18 | .450 | 193. | 5.5 | 505. |
| 19 | .470 | 202. | 5.4 | 505. |
| 20 | .480 | 206. | 5.4 | 505. |
| 21 | .470 | 202. | 5.4 | 508. |
| 22 | .470 | 202. | 5.5 | 505. |
| 23 | .480 | 206. | 5.4 | 502. |
| 24 | .480 | 206. | 5.4 | 500. |

DAY = 39

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 5.7 | 430. |
| 2 | .590 | 253. | 6.3 | 430. |
| 3 | .590 | 253. | 6.3 | 430. |
| 4 | .560 | 241. | 6.3 | 440. |
| 5 | .570 | 245. | 6.3 | 435. |
| 6 | .580 | 249. | 6.3 | 435. |
| 7 | .500 | 215. | 5.5 | 510. |
| 8 | .520 | 223. | 5.4 | 510. |
| 9 | .450 | 193. | 5.6 | 510. |
| 10 | .390 | 168. | 5.5 | 510. |
| 11 | .420 | 180. | 5.4 | 510. |
| 12 | .440 | 189. | 5.4 | 510. |
| 13 | .410 | 176. | 5.4 | 510. |
| 14 | .430 | 185. | 5.4 | 510. |
| 15 | .460 | 198. | 5.4 | 510. |
| 16 | .470 | 202. | 5.4 | 508. |
| 17 | .460 | 198. | 5.4 | 507. |
| 18 | .470 | 202. | 6.1 | 430. |
| 19 | .470 | 202. | 6.4 | 430. |
| 20 | .500 | 215. | 6.4 | 430. |
| 21 | .510 | 219. | 6.3 | 430. |
| 22 | .490 | 210. | 6.4 | 430. |
| 23 | .510 | 219. | 6.7 | 373. |
| 24 | .580 | 249. | 7.6 | 330. |

DAY = 40

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 7.9 | 280. |
| 2 | .610 | 262. | 9.3 | 210. |
| 3 | .500 | 215. | 10.1 | 180. |
| 4 | .520 | 223. | 10.1 | 180. |
| 5 | .530 | 228. | 10.1 | 180. |

| | | | | |
|---|---|---|---|---|
| 6 | .530 | 228. | 10.1 | 180. |
| 7 | .530 | 228. | 10.1 | 180. |
| 8 | .540 | 232. | 10.1 | 220. |
| 9 | .570 | 245. | 7.8 | 390. |
| 10 | .410 | 176. | 5.9 | 515. |
| 11 | .350 | 150. | 5.3 | 510. |
| 12 | .380 | 163. | 5.2 | 515. |
| 13 | .380 | 163. | 5.3 | 515. |
| 14 | .400 | 172. | 5.3 | 515. |
| 15 | .410 | 176. | 5.2 | 515. |
| 16 | .420 | 180. | 5.2 | 515. |
| 17 | .420 | 180. | 5.2 | 515. |
| 18 | .410 | 176. | 5.3 | 512. |
| 19 | .400 | 172. | 5.3 | 510. |
| 20 | .410 | 176. | 5.3 | 510. |
| 21 | .460 | 198. | 5.3 | 510. |
| 22 | .460 | 198. | 5.4 | 510. |
| 23 | .460 | 198. | 5.6 | 450. |
| 24 | .530 | 228. | 8.4 | 180. |

DAY = 41

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 10.1 | 175. |
| 2 | .370 | 159. | 10.1 | 175. |
| 3 | .370 | 159. | 10.1 | 175. |
| 4 | .370 | 159. | 10.1 | 175. |
| 5 | .420 | 180. | 10.0 | 210. |
| 6 | .400 | 172. | 8.0 | 380. |
| 7 | .390 | 168. | 5.8 | 500. |
| 8 | .410 | 176. | 5.5 | 510. |
| 9 | .400 | 172. | 5.3 | 510. |
| 10 | .420 | 180. | 5.3 | 510. |
| 11 | .430 | 185. | 5.3 | 510. |
| 12 | .450 | 193. | 5.3 | 510. |
| 13 | .460 | 198. | 5.3 | 510. |
| 14 | .470 | 202. | 5.3 | 510. |
| 15 | .490 | 210. | 5.3 | 510. |
| 16 | .500 | 215. | 5.3 | 510. |
| 17 | .480 | 206. | 5.2 | 515. |
| 18 | .430 | 185. | 5.4 | 515. |
| 19 | .450 | 193. | 5.3 | 515. |
| 20 | .420 | 180. | 5.3 | 510. |
| 21 | -1.000 | -430. | 5.3 | 510. |
| 22 | -1.000 | -430. | 5.3 | 510. |
| 23 | -1.000 | -430. | 5.3 | 515. |
| 24 | -1.000 | -430. | 5.6 | 460. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 6.8 | 390. |
| 2 | .600 | 258. | 6.9 | 390. |
| 3 | .580 | 249. | 6.6 | 430. |
| 4 | .550 | 236. | 6.2 | 445. |

| | | | | |
|---|---|---|---|---|
| 5 | .570 | 245. | 6.1 | 470. |
| 6 | .540 | 232. | 5.7 | 510. |
| 7 | .550 | 236. | 5.3 | 515. |
| 8 | .550 | 236. | 5.2 | 515. |
| 9 | .530 | 228. | 5.3 | 515. |
| 10 | .510 | 219. | 5.3 | 515. |
| 11 | .510 | 219. | 5.3 | 520. |
| 12 | .500 | 215. | 5.2 | 520. |
| 13 | .500 | 215. | 5.3 | 520. |
| 14 | .500 | 215. | 5.2 | 520. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .500 | 215. | 5.2 | 523. |
| 17 | .530 | 228. | 5.4 | 505. |
| 18 | .520 | 223. | 5.4 | 505. |
| 19 | .510 | 219. | 5.5 | 505. |
| 20 | .520 | 223. | 5.4 | 505. |
| 21 | .530 | 228. | 5.4 | 505. |
| 22 | .530 | 228. | 5.4 | 505. |
| 23 | .500 | 215. | 5.5 | 505. |
| 24 | .520 | 223. | 5.4 | 505. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 5.9 | 420. |
| 2 | .550 | 236. | 5.8 | 500. |
| 3 | .520 | 223. | 5.5 | 505. |
| 4 | .510 | 219. | 5.5 | 505. |
| 5 | .470 | 202. | 5.5 | 505. |
| 6 | .480 | 206. | 5.4 | 505. |
| 7 | .470 | 202. | 5.4 | 500. |
| 8 | .460 | 198. | 5.4 | 500. |
| 9 | -1.000 | -430. | 5.4 | 500. |
| 10 | -1.000 | -430. | 5.5 | 505. |
| 11 | -1.000 | -430. | 5.5 | 505. |
| 12 | -1.000 | -430. | 5.4 | 500. |
| 13 | -1.000 | -430. | 5.4 | 500. |
| 14 | -1.000 | -430. | 5.4 | 505. |
| 15 | .450 | 193. | 5.5 | 505. |
| 16 | .460 | 198. | 5.5 | 500. |
| 17 | .470 | 202. | 5.5 | 500. |
| 18 | .450 | 193. | 5.5 | 500. |
| 19 | .460 | 198. | 5.5 | 500. |
| 20 | .460 | 198. | 5.5 | 500. |
| 21 | .470 | 202. | 5.4 | 500. |
| 22 | .470 | 202. | 5.5 | 500. |
| 23 | .450 | 193. | 5.5 | 500. |
| 24 | .460 | 198. | 5.5 | 500. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 6.4 | 380. |
| 2 | .500 | 215. | 7.1 | 340. |
| 3 | .440 | 189. | 8.5 | 275. |

| | | | | |
|---|---|---|---|---|
| 4 | .440 | 189. | 8.7 | 275. |
| 5 | .440 | 189. | 8.7 | 275. |
| 6 | .520 | 223. | 7.4 | 375. |
| 7 | .530 | 228. | 6.1 | 500. |
| 8 | .530 | 228. | 5.5 | 502. |
| 9 | -1.000 | -430. | 5.6 | 502. |
| 10 | -1.000 | -430. | 5.5 | 500. |
| 11 | .500 | 215. | 5.4 | 504. |
| 12 | .490 | 210. | 5.5 | 500. |
| 13 | .490 | 210. | 5.5 | 500. |
| 14 | .470 | 202. | 5.5 | 500. |
| 15 | .470 | 202. | 5.4 | 500. |
| 16 | .480 | 206. | 5.4 | 500. |
| 17 | .500 | 215. | 5.4 | 500. |
| 18 | .500 | 215. | 5.4 | 500. |
| 19 | .470 | 202. | 5.4 | 500. |
| 20 | .480 | 206. | 5.4 | 500. |
| 21 | .500 | 215. | 5.4 | 500. |
| 22 | .510 | 219. | 5.5 | 500. |
| 23 | .500 | 215. | 5.9 | 440. |
| 24 | .560 | 241. | 7.3 | 320. |

DAY = 46

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 7.6 | 320. |
| 2 | .540 | 232. | 7.8 | 265. |
| 3 | .490 | 210. | 9.8 | 170. |
| 4 | .420 | 180. | 10.1 | 170. |
| 5 | .420 | 180. | 10.1 | 170. |
| 6 | .490 | 210. | 9.8 | 250. |
| 7 | .560 | 241. | 8.1 | 300. |
| 8 | .560 | 241. | 7.4 | 400. |
| 9 | .450 | 193. | 5.7 | 500. |
| 10 | .440 | 189. | 5.4 | 500. |
| 11 | .450 | 193. | 5.4 | 500. |
| 12 | .450 | 193. | 5.4 | 500. |
| 13 | .440 | 189. | 5.4 | 500. |
| 14 | .440 | 189. | 5.4 | 508. |
| 15 | .430 | 185. | 5.4 | 508. |
| 16 | .460 | 198. | 5.4 | 508. |
| 17 | .480 | 206. | 5.5 | 500. |
| 18 | .510 | 219. | 5.5 | 500. |
| 19 | .530 | 228. | 5.5 | 500. |
| 20 | .520 | 223. | 5.5 | 500. |
| 21 | .490 | 210. | 5.6 | 496. |
| 22 | .500 | 215. | 5.5 | 500. |
| 23 | .510 | 219. | 5.5 | 499. |
| 24 | .520 | 223. | 5.7 | 425. |

DAY = 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 6.4 | 425. |
| 2 | .550 | 236. | 6.4 | 425. |

| | | | | |
|---|---|---|---|---|
| 3 | .560 | 241. | 6.4 | 425. |
| 4 | .580 | 249. | 6.3 | 425. |
| 5 | .580 | 249. | 6.4 | 425. |
| 6 | .560 | 241. | 6.4 | 425. |
| 7 | .450 | 193. | 6.7 | 370. |
| 8 | .480 | 206. | 6.4 | 475. |
| 9 | .470 | 202. | 5.7 | 475. |
| 10 | .450 | 193. | 5.7 | 475. |
| 11 | .510 | 219. | 6.2 | 475. |
| 12 | .390 | 168. | 6.7 | 380. |
| 13 | .430 | 185. | 6.7 | 380. |
| 14 | .460 | 198. | 6.8 | 330. |
| 15 | .570 | 245. | 7.3 | 330. |
| 16 | .570 | 245. | 7.4 | 330. |
| 17 | -1.000 | -430. | 7.4 | 330. |
| 18 | -1.000 | -430. | 7.0 | 380. |
| 19 | -1.000 | -430. | 6.8 | 380. |
| 20 | -1.000 | -430. | 6.9 | 380. |
| 21 | .460 | 198. | 6.8 | 380. |
| 22 | .460 | 198. | 6.8 | 380. |
| 23 | -1.000 | -430. | 6.9 | 380. |
| 24 | -1.000 | -430. | 8.3 | 240. |

DAY = 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.2 | 500. |
| 2 | .500 | 215. | 5.3 | 500. |
| 3 | .460 | 198. | 5.5 | 500. |
| 4 | .430 | 185. | 5.4 | 500. |
| 5 | .440 | 189. | 5.3 | 500. |
| 6 | .450 | 193. | 5.4 | 500. |
| 7 | -1.000 | -430. | -1.0 | -1. |
| 8 | .470 | 202. | 5.9 | 500. |
| 9 | -1.000 | -430. | 5.5 | 500. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .210 | 90. | 10.1 | 100. |
| 12 | .390 | 168. | 10.0 | 180. |
| 13 | .500 | 215. | 9.1 | 205. |
| 14 | .560 | 241. | 7.8 | 335. |
| 15 | -1.000 | -430. | 7.5 | 335. |
| 16 | -1.000 | -430. | 7.5 | 335. |
| 17 | .540 | 232. | 7.3 | 408. |
| 18 | .570 | 245. | 6.4 | 450. |
| 19 | .560 | 241. | 6.2 | 450. |
| 20 | .520 | 223. | 6.3 | 450. |
| 21 | .500 | 215. | 6.3 | 450. |
| 22 | .510 | 219. | 6.2 | 450. |
| 23 | .500 | 215. | 6.2 | 450. |
| 24 | .500 | 215. | 6.2 | 450. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 6.2 | 450. |

| | | | | |
|---|---|---|---|---|
| 2 | .500 | 215. | 6.2 | 465. |
| 3 | .460 | 198. | 6.2 | 460. |
| 4 | .470 | 202. | 6.2 | 460. |
| 5 | .470 | 202. | 6.2 | 460. |
| 6 | .470 | 202. | 6.2 | 460. |
| 7 | .470 | 202. | 6.2 | 460. |
| 8 | .480 | 206. | 6.2 | 460. |
| 9 | .490 | 210. | 6.0 | 490. |
| 10 | .460 | 198. | 5.7 | 495. |
| 11 | .450 | 193. | 5.7 | 500. |
| 12 | .490 | 210. | 5.6 | 500. |
| 13 | .510 | 219. | 5.6 | 500. |
| 14 | .490 | 210. | 5.6 | 500. |
| 15 | .490 | 210. | 5.6 | 500. |
| 16 | .490 | 210. | 5.6 | 500. |
| 17 | .510 | 219. | 5.6 | 500. |
| 18 | .510 | 219. | 5.6 | 500. |
| 19 | .520 | 223. | 5.5 | 500. |
| 20 | .510 | 219. | 5.6 | 500. |
| 21 | .470 | 202. | 5.7 | 500. |
| 22 | .470 | 202. | 5.7 | 500. |
| 23 | .500 | 215. | 5.6 | 500. |
| 24 | .530 | 228. | 5.6 | 500. |

DAY = 55

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | 7.0 | 330. |
| 2 | -1.000 | -430. | 8.1 | 272. |
| 3 | .400 | 172. | 8.3 | 270. |
| 4 | .400 | 172. | 8.4 | 270. |
| 5 | .410 | 176. | 8.4 | 270. |
| 6 | .430 | 185. | 7.8 | 360. |
| 7 | .450 | 193. | 5.8 | 490. |
| 8 | .440 | 189. | 5.4 | 495. |
| 9 | .450 | 193. | 5.4 | 495. |
| 10 | .480 | 206. | 5.5 | 495. |
| 11 | .490 | 210. | 5.6 | 495. |
| 12 | .500 | 215. | 5.6 | 495. |
| 13 | .500 | 215. | 5.5 | 495. |
| 14 | .500 | 215. | 5.6 | 495. |
| 15 | .490 | 210. | 5.6 | 495. |
| 16 | .490 | 210. | 5.6 | 490. |
| 17 | .500 | 215. | 5.5 | 490. |
| 18 | .520 | 223. | 5.5 | 490. |
| 19 | .490 | 210. | 5.5 | 495. |
| 20 | .480 | 206. | 5.6 | 495. |
| 21 | .490 | 210. | 5.6 | 490. |
| 22 | .500 | 215. | 5.5 | 490. |
| 23 | .500 | 215. | 5.5 | 495. |
| 24 | .490 | 210. | 5.6 | 495. |

DAY = 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.6 | 490. |
| 2 | .520 | 223. | 5.5 | 490. |
| 3 | .480 | 206. | 5.6 | 495. |
| 4 | .440 | 189. | 5.7 | 490. |
| 5 | .450 | 193. | 5.7 | 490. |
| 6 | .400 | 172. | 5.7 | 480. |
| 7 | .490 | 210. | 6.2 | 438. |
| 8 | .500 | 215. | 6.3 | 443. |
| 9 | .510 | 219. | 6.3 | 443. |
| 10 | .600 | 258. | 6.3 | 430. |
| 11 | .590 | 253. | 6.3 | 435. |
| 12 | .520 | 223. | 6.3 | 439. |
| 13 | .480 | 206. | 5.9 | 480. |
| 14 | .470 | 202. | 5.8 | 480. |
| 15 | .480 | 206. | 5.8 | 480. |
| 16 | .490 | 210. | 5.8 | 480. |
| 17 | .510 | 219. | 5.7 | 480. |
| 18 | .490 | 210. | 5.7 | 480. |
| 19 | .500 | 215. | 5.7 | 480. |
| 20 | .520 | 223. | 5.7 | 460. |
| 21 | .560 | 241. | 6.0 | 460. |
| 22 | .570 | 245. | 6.0 | 455. |
| 23 | .550 | 236. | 6.1 | 455. |
| 24 | .560 | 241. | 6.1 | 452. |

DAY = 57

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.1 | 452. |
| 2 | .580 | 249. | 6.1 | 452. |
| 3 | .580 | 249. | 6.1 | 455. |
| 4 | .570 | 245. | 6.2 | 452. |
| 5 | .580 | 249. | 6.1 | 455. |
| 6 | .440 | 189. | 5.7 | 482. |
| 7 | .440 | 189. | 5.7 | 492. |
| 8 | .430 | 185. | 5.7 | 492. |
| 9 | .430 | 185. | 5.7 | 492. |
| 10 | .510 | 219. | 5.8 | 492. |
| 11 | .550 | 236. | 5.8 | 492. |
| 12 | .560 | 241. | 5.7 | 492. |
| 13 | .550 | 236. | 5.8 | 492. |
| 14 | .540 | 232. | 5.8 | 493. |
| 15 | .540 | 232. | 5.8 | 493. |
| 16 | .550 | 236. | 5.7 | 482. |
| 17 | .560 | 241. | 5.7 | 485. |
| 18 | .560 | 241. | 5.7 | 485. |
| 19 | .550 | 236. | 5.8 | 490. |
| 20 | .530 | 228. | 5.8 | 490. |
| 21 | .540 | 232. | 5.8 | 490. |
| 22 | .510 | 219. | 6.0 | 460. |
| 23 | .550 | 236. | 6.7 | 425. |
| 24 | .550 | 236. | 6.7 | 425. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.6 | 428. |
| 2 | .560 | 241. | 6.6 | 425. |
| 3 | .580 | 249. | 6.6 | 428. |
| 4 | .520 | 223. | 6.2 | 480. |
| 5 | .470 | 202. | 5.9 | 488. |
| 6 | .470 | 202. | 5.9 | 482. |
| 7 | .480 | 206. | 5.8 | 480. |
| 8 | .540 | 232. | 6.4 | 340. |
| 9 | .620 | 266. | 7.1 | 380. |
| 10 | .600 | 258. | 7.1 | 380. |
| 11 | .610 | 262. | 7.1 | 380. |
| 12 | .620 | 266. | 7.6 | 320. |
| 13 | .620 | 266. | 7.8 | 320. |
| 14 | .620 | 266. | 7.9 | 320. |
| 15 | .610 | 262. | 7.8 | 320. |
| 16 | .600 | 258. | 7.8 | 320. |
| 17 | .610 | 262. | 7.8 | 320. |
| 18 | .610 | 262. | 7.8 | 320. |
| 19 | .580 | 249. | 7.8 | 320. |
| 20 | .580 | 249. | 7.8 | 320. |
| 21 | .590 | 253. | 7.7 | 340. |
| 22 | .470 | 202. | 6.6 | 430. |
| 23 | .380 | 163. | 5.8 | 490. |
| 24 | .370 | 159. | 5.7 | 490. |

DAY = 59

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 5.7 | 490. |
| 2 | .410 | 176. | 5.8 | 485. |
| 3 | .420 | 180. | 5.7 | 485. |
| 4 | .410 | 176. | 5.7 | 488. |
| 5 | .410 | 176. | 5.7 | 488. |
| 6 | .430 | 185. | 5.7 | 485. |
| 7 | .470 | 202. | 5.9 | 422. |
| 8 | .550 | 236. | 6.6 | 400. |
| 9 | .620 | 266. | 7.1 | 370. |
| 10 | .620 | 266. | 7.7 | 325. |
| 11 | .610 | 262. | 7.6 | 350. |
| 12 | .560 | 241. | 7.4 | 350. |
| 13 | .530 | 228. | 8.4 | 240. |
| 14 | .530 | 228. | 9.1 | 240. |
| 15 | -1.000 | -430. | 9.1 | 240. |
| 16 | -1.000 | -430. | 9.2 | 240. |
| 17 | .550 | 236. | 9.2 | 240. |
| 18 | .590 | 253. | 8.5 | 330. |
| 19 | .490 | 210. | 7.1 | 380. |
| 20 | .400 | 172. | 5.9 | 490. |
| 21 | .400 | 172. | 5.4 | 510. |
| 22 | .430 | 185. | 5.4 | 510. |
| 23 | .420 | 180. | 5.5 | 505. |
| 24 | .460 | 198. | 5.6 | 490. |

DAY = 60

| | NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 5.7 | 490. |
| 2 | .460 | 198. | 5.7 | 490. |
| 3 | .460 | 198. | 5.7 | 490. |
| 4 | .470 | 202. | 5.7 | 490. |
| 5 | .480 | 206. | 5.7 | 490. |
| 6 | .480 | 206. | 5.7 | 490. |
| 7 | .480 | 206. | 5.8 | 490. |
| 8 | .500 | 215. | 5.9 | 485. |
| 9 | .490 | 210. | 5.8 | 485. |
| 10 | .430 | 185. | 5.3 | 485. |
| 11 | .530 | 228. | 5.7 | 485. |
| 12 | .510 | 219. | 5.8 | 485. |
| 13 | .470 | 202. | 5.6 | 485. |
| 14 | .520 | 223. | 5.7 | 485. |
| 15 | .530 | 228. | 5.7 | 485. |
| 16 | .520 | 223. | 5.7 | 490. |
| 17 | .510 | 219. | 5.6 | 500. |
| 18 | .480 | 206. | 5.7 | 500. |
| 19 | .490 | 210. | 5.6 | 500. |
| 20 | .500 | 215. | 5.6 | 500. |
| 21 | .480 | 206. | 5.7 | 500. |
| 22 | .490 | 210. | 5.7 | 500. |
| 23 | .510 | 219. | 5.7 | 500. |
| 24 | .510 | 219. | 5.6 | 495. |

DAY = 61



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.8 | 495. |
| 2 | .510 | 219. | 5.8 | 495. |
| 3 | .500 | 215. | 5.7 | 495. |
| 4 | .530 | 228. | 5.7 | 495. |
| 5 | .530 | 228. | 5.7 | 495. |
| 6 | .540 | 232. | 5.7 | 495. |
| 7 | .510 | 219. | 5.8 | 495. |
| 8 | .490 | 210. | 5.8 | 490. |
| 9 | .520 | 223. | 5.8 | 495. |
| 10 | .530 | 228. | 5.7 | 495. |
| 11 | .550 | 236. | 5.7 | 495. |
| 12 | .540 | 232. | 5.7 | 495. |
| 13 | .460 | 198. | 5.8 | 495. |
| 14 | .450 | 193. | 5.8 | 490. |
| 15 | .490 | 210. | 5.8 | 490. |
| 16 | .520 | 223. | 5.7 | 495. |
| 17 | .530 | 228. | 5.6 | 500. |
| 18 | .530 | 228. | 5.7 | 500. |
| 19 | .470 | 202. | 5.8 | 500. |
| 20 | .470 | 202. | 5.7 | 500. |
| 21 | .470 | 202. | 5.7 | 500. |
| 22 | .470 | 202. | 5.7 | 495. |
| 23 | .460 | 198. | 5.8 | 495. |
| 24 | .470 | 202. | 5.8 | 495. |

DAY = 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 5.8 | 495. |
| 2 | .470 | 202. | 5.8 | 495. |
| 3 | .460 | 198. | 5.9 | 495. |
| 4 | .460 | 198. | 5.8 | 495. |
| 5 | .470 | 202. | 5.8 | 495. |
| 6 | .450 | 193. | 5.7 | 495. |
| 7 | .450 | 193. | 5.7 | 495. |
| 8 | .470 | 202. | 5.7 | 490. |
| 9 | .490 | 210. | 5.7 | 490. |
| 10 | .510 | 219. | 5.6 | 490. |
| 11 | .530 | 228. | 5.6 | 490. |
| 12 | .540 | 232. | 5.6 | 490. |
| 13 | .520 | 223. | 5.6 | 495. |
| 14 | .460 | 198. | 5.7 | 495. |
| 15 | .460 | 198. | 5.6 | 495. |
| 16 | .470 | 202. | 5.5 | 495. |
| 17 | .420 | 180. | 5.5 | 495. |
| 18 | .420 | 180. | 5.5 | 495. |
| 19 | .430 | 185. | 5.5 | 495. |
| 20 | .450 | 193. | 5.5 | 495. |
| 21 | .440 | 189. | 5.5 | 495. |
| 22 | .460 | 198. | 5.6 | 495. |
| 23 | .460 | 198. | 5.6 | 495. |
| 24 | .470 | 202. | 5.6 | 495. |

DAY = 63



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 5.6 | 495. |
| 2 | .410 | 176. | 7.5 | 495. |
| 3 | .370 | 159. | 7.9 | 495. |
| 4 | .370 | 159. | 7.9 | 495. |
| 5 | .370 | 159. | 7.8 | 495. |
| 6 | .440 | 189. | 6.4 | 495. |
| 7 | .410 | 176. | 5.5 | 495. |
| 8 | .450 | 193. | 5.5 | 490. |
| 9 | .490 | 210. | 5.6 | 490. |
| 10 | .600 | 258. | 6.7 | 490. |
| 11 | .490 | 210. | 6.8 | 490. |
| 12 | .530 | 228. | 7.3 | 490. |
| 13 | .580 | 249. | 7.6 | 495. |
| 14 | .550 | 236. | 7.3 | 495. |
| 15 | .490 | 210. | 5.9 | 495. |
| 16 | .530 | 228. | 5.5 | 495. |
| 17 | .510 | 219. | 5.6 | 495. |
| 18 | .470 | 202. | 5.6 | 495. |
| 19 | .470 | 202. | 5.6 | 495. |
| 20 | .490 | 210. | 5.6 | 495. |
| 21 | .490 | 210. | 5.6 | 495. |
| 22 | .480 | 206. | 5.6 | 495. |
| 23 | .480 | 206. | 5.6 | 495. |
| 24 | .500 | 215. | 5.7 | 495. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 5.6 | 490. |
| 2 | .510 | 219. | 5.7 | 490. |
| 3 | .500 | 215. | 5.7 | 490. |
| 4 | .510 | 219. | 5.7 | 490. |
| 5 | .520 | 223. | 5.7 | 490. |
| 6 | .500 | 215. | 5.8 | 490. |
| 7 | .490 | 210. | 5.7 | 490. |
| 8 | .500 | 215. | 5.8 | 490. |
| 9 | .500 | 215. | 5.8 | 490. |
| 10 | .450 | 193. | 5.8 | 490. |
| 11 | .450 | 193. | 5.8 | 490. |
| 12 | .450 | 193. | 5.8 | 490. |
| 13 | .450 | 193. | 5.7 | 490. |
| 14 | .450 | 193. | 5.7 | 490. |
| 15 | .440 | 189. | 5.7 | 490. |
| 16 | .430 | 185. | 5.6 | 490. |
| 17 | .440 | 189. | 5.5 | 490. |
| 18 | .440 | 189. | 5.6 | 490. |
| 19 | .430 | 185. | 5.7 | 490. |
| 20 | .440 | 189. | 5.6 | 490. |
| 21 | .440 | 189. | 5.6 | 490. |
| 22 | .450 | 193. | 5.7 | 490. |
| 23 | .450 | 193. | 5.7 | 490. |
| 24 | .440 | 189. | 5.7 | 490. |

DAY = 65



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 5.7 | 490. |
| 2 | .420 | 180. | 5.8 | 490. |
| 3 | .400 | 172. | 5.7 | 490. |
| 4 | .410 | 176. | 5.7 | 490. |
| 5 | .470 | 202. | 5.6 | 490. |
| 6 | .460 | 198. | 5.8 | 490. |
| 7 | .410 | 176. | 5.6 | 490. |
| 8 | .450 | 193. | 5.7 | 490. |
| 9 | .470 | 202. | 5.7 | 485. |
| 10 | .470 | 202. | 5.6 | 485. |
| 11 | .500 | 215. | 5.6 | 490. |
| 12 | .490 | 210. | 5.6 | 490. |
| 13 | .420 | 180. | 5.7 | 490. |
| 14 | .430 | 185. | 5.7 | 490. |
| 15 | .450 | 193. | 5.6 | 490. |
| 16 | .450 | 193. | 5.5 | 485. |
| 17 | -1.000 | -430. | 5.5 | 482. |
| 18 | -1.000 | -430. | 5.5 | 490. |
| 19 | .470 | 202. | 5.7 | 490. |
| 20 | .480 | 206. | 5.6 | 485. |
| 21 | .490 | 210. | 5.6 | 485. |
| 22 | .510 | 219. | 5.5 | 490. |
| 23 | .490 | 210. | 5.5 | 488. |
| 24 | .530 | 228. | 6.0 | 400. |

DAY = 66

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 7.3 | 390. |
| 2 | .610 | 262. | 8.2 | 390. |
| 3 | .620 | 266. | 8.2 | 390. |
| 4 | .640 | 275. | 8.1 | 390. |
| 5 | .560 | 241. | 6.9 | 390. |
| 6 | .390 | 168. | 5.6 | 485. |
| 7 | .390 | 168. | 5.5 | 485. |
| 8 | .410 | 176. | 5.6 | 485. |
| 9 | .420 | 180. | 5.6 | 480. |
| 10 | .420 | 180. | 5.7 | 465. |
| 11 | .530 | 228. | 6.4 | 420. |
| 12 | .550 | 236. | 6.5 | 420. |
| 13 | .540 | 232. | 6.6 | 420. |
| 14 | .530 | 228. | 6.6 | 420. |
| 15 | .530 | 228. | 6.6 | 420. |
| 16 | .540 | 232. | 6.5 | 420. |
| 17 | .550 | 236. | 6.6 | 420. |
| 18 | .510 | 219. | 6.6 | 420. |
| 19 | .520 | 223. | 6.6 | 420. |
| 20 | .520 | 223. | 6.6 | 420. |
| 21 | .530 | 228. | 6.6 | 420. |
| 22 | .530 | 228. | 6.6 | 420. |
| 23 | .530 | 228. | 6.7 | 420. |
| 24 | .540 | 232. | 6.7 | 420. |

DAY = 68



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 6.9 | 420. |
| 2 | .620 | 266. | 6.9 | 420. |
| 3 | .620 | 266. | 6.8 | 420. |
| 4 | .630 | 271. | 6.9 | 420. |
| 5 | .600 | 258. | 6.9 | 420. |
| 6 | .590 | 253. | 6.8 | 420. |
| 7 | .590 | 253. | 6.7 | 420. |
| 8 | .600 | 258. | 6.8 | 420. |
| 9 | .600 | 258. | 6.8 | 420. |
| 10 | .600 | 258. | 6.8 | 420. |
| 11 | .590 | 253. | 6.8 | 420. |
| 12 | .590 | 253. | 6.8 | 420. |
| 13 | .610 | 262. | 6.7 | 420. |
| 14 | .590 | 253. | 6.8 | 420. |
| 15 | .590 | 253. | 6.8 | 420. |
| 16 | .590 | 253. | 6.7 | 418. |
| 17 | .600 | 258. | 6.8 | 420. |
| 18 | .580 | 249. | 6.8 | 420. |
| 19 | .590 | 253. | 6.8 | 420. |
| 20 | .590 | 253. | 6.8 | 420. |
| 21 | .570 | 245. | 6.8 | 420. |
| 22 | .580 | 249. | 6.8 | 420. |
| 23 | .570 | 245. | 6.9 | 420. |
| 24 | .530 | 228. | 7.2 | 350. |

DAY = 69

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 8.4 | 300. |
| 2 | .350 | 150. | 9.7 | 180. |
| 3 | .320 | 137. | 10.2 | 180. |
| 4 | .450 | 193. | 9.7 | 250. |
| 5 | .460 | 198. | 7.6 | 415. |
| 6 | .530 | 228. | 6.9 | 420. |
| 7 | .530 | 228. | 6.8 | 420. |
| 8 | .560 | 241. | 6.9 | 420. |
| 9 | .620 | 266. | 6.9 | 420. |
| 10 | .600 | 258. | 7.0 | 420. |
| 11 | .600 | 258. | 7.0 | 420. |
| 12 | .610 | 262. | 6.9 | 420. |
| 13 | .610 | 262. | 6.9 | 420. |
| 14 | .590 | 253. | 6.9 | 420. |
| 15 | .590 | 253. | 6.9 | 420. |
| 16 | .590 | 253. | 6.9 | 415. |
| 17 | .580 | 249. | 7.0 | 415. |
| 18 | .570 | 245. | 7.0 | 415. |
| 19 | .570 | 245. | 6.9 | 418. |
| 20 | .560 | 241. | 6.9 | 418. |
| 21 | .570 | 245. | 7.0 | 418. |
| 22 | .570 | 245. | 6.9 | 422. |
| 23 | .490 | 210. | 6.2 | 485. |
| 24 | .510 | 219. | 6.2 | 480. |

DAY = 70

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 8.9 | 250. |
| 2 | .440 | 189. | 10.1 | 175. |
| 3 | .410 | 176. | 10.1 | 175. |
| 4 | .410 | 176. | 10.1 | 175. |
| 5 | .410 | 176. | 10.1 | 175. |
| 6 | .450 | 193. | 9.4 | 390. |
| 7 | .530 | 228. | 6.1 | 480. |
| 8 | .540 | 232. | 6.1 | 480. |
| 9 | .560 | 241. | 6.1 | 480. |
| 10 | .560 | 241. | 6.1 | 480. |
| 11 | .560 | 241. | 6.0 | 490. |
| 12 | .530 | 228. | 6.0 | 490. |
| 13 | .510 | 219. | 5.9 | 490. |
| 14 | .520 | 223. | 5.9 | 490. |
| 15 | .510 | 219. | 5.9 | 490. |
| 16 | .530 | 228. | 7.3 | 322. |
| 17 | .570 | 245. | 8.0 | 322. |
| 18 | .560 | 241. | 8.0 | 322. |
| 19 | .570 | 245. | 8.1 | 320. |
| 20 | .490 | 210. | 9.5 | 230. |
| 21 | .500 | 215. | 9.6 | 230. |
| 22 | .400 | 172. | 10.1 | 180. |
| 23 | .360 | 155. | 10.1 | 182. |
| 24 | .360 | 155. | 10.1 | 180. |

DAY = 71

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 10.1 | 180. |
| 2 | .360 | 155. | 10.1 | 185. |
| 3 | .380 | 163. | 10.1 | 185. |
| 4 | .380 | 163. | 10.1 | 185. |
| 5 | .380 | 163. | 10.1 | 180. |
| 6 | .390 | 168. | 10.1 | 185. |
| 7 | .450 | 193. | 9.4 | 260. |
| 8 | .550 | 236. | 7.1 | 465. |
| 9 | .500 | 215. | 5.8 | 470. |
| 10 | .520 | 223. | 5.9 | 475. |
| 11 | .520 | 223. | 5.9 | 475. |
| 12 | .520 | 223. | 5.7 | 475. |
| 13 | .570 | 245. | 6.5 | 360. |
| 14 | .470 | 202. | 8.6 | 230. |
| 15 | .530 | 228. | 9.2 | 230. |
| 16 | .510 | 219. | 9.7 | 180. |
| 17 | .500 | 215. | 10.0 | 180. |
| 18 | .500 | 215. | 10.0 | 180. |
| 19 | .510 | 219. | 10.0 | 180. |
| 20 | .510 | 219. | 10.0 | 180. |
| 21 | .510 | 219. | 10.0 | 180. |
| 22 | .500 | 215. | 10.0 | 180. |
| 23 | -1.000 | -430. | 10.0 | 180. |
| 24 | -1.000 | -430. | 10.0 | 180. |

DAY = 73



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.1 | 180. |
| 2 | .420 | 180. | 10.1 | 180. |
| 3 | .430 | 185. | 10.1 | 180. |
| 4 | .440 | 189. | 10.1 | 175. |
| 5 | .430 | 185. | 10.1 | 175. |
| 6 | .440 | 189. | 10.1 | 180. |
| 7 | .500 | 215. | 9.0 | 360. |
| 8 | .540 | 232. | 7.0 | 445. |
| 9 | .580 | 249. | 6.4 | 460. |
| 10 | .510 | 219. | 5.8 | 490. |
| 11 | .510 | 219. | 5.8 | 500. |
| 12 | .510 | 219. | 5.8 | 500. |
| 13 | .510 | 219. | 5.7 | 500. |
| 14 | .490 | 210. | 5.7 | 488. |
| 15 | .610 | 262. | 6.6 | 412. |
| 16 | .610 | 262. | 6.8 | 412. |
| 17 | .600 | 258. | 6.7 | 412. |
| 18 | .520 | 223. | 6.0 | 475. |
| 19 | .530 | 228. | 6.0 | 475. |
| 20 | .530 | 228. | 6.0 | 475. |
| 21 | .530 | 228. | 6.1 | 475. |
| 22 | .550 | 236. | 6.1 | 475. |
| 23 | .580 | 249. | 6.6 | 428. |
| 24 | .570 | 245. | 8.7 | 220. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 10.1 | 175. |
| 2 | .410 | 176. | 10.1 | 175. |
| 3 | .430 | 185. | 10.1 | 175. |
| 4 | .450 | 193. | 10.1 | 175. |
| 5 | .460 | 198. | 10.1 | 175. |
| 6 | .440 | 189. | 10.0 | 185. |
| 7 | .430 | 185. | 8.6 | 175. |
| 8 | .420 | 180. | 8.6 | 275. |
| 9 | .420 | 180. | 8.6 | 275. |
| 10 | .430 | 185. | 8.6 | 275. |
| 11 | .430 | 185. | 8.6 | 275. |
| 12 | .460 | 198. | 10.0 | 175. |
| 13 | .430 | 185. | 10.1 | 175. |
| 14 | .420 | 180. | 10.1 | 175. |
| 15 | .420 | 180. | 10.1 | 175. |
| 16 | .420 | 180. | 10.1 | 175. |
| 17 | .410 | 176. | 10.1 | 175. |
| 18 | .400 | 172. | 10.1 | 175. |
| 19 | .410 | 176. | 10.1 | 175. |
| 20 | .410 | 176. | 10.1 | 175. |
| 21 | .420 | 180. | 10.1 | 175. |
| 22 | .410 | 176. | 10.1 | 175. |
| 23 | .420 | 180. | 10.1 | 175. |
| 24 | .410 | 176. | 10.1 | 175. |

DAY = 75



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.1 | 175. |
| 2 | .400 | 172. | 10.1 | 175. |
| 3 | .400 | 172. | 10.1 | 175. |
| 4 | .390 | 168. | 10.1 | 175. |
| 5 | .390 | 168. | 10.1 | 175. |
| 6 | .380 | 163. | 10.1 | 175. |
| 7 | .390 | 168. | 10.0 | 175. |
| 8 | .390 | 168. | 10.1 | 175. |
| 9 | .390 | 168. | 10.1 | 175. |
| 10 | .400 | 172. | 10.1 | 175. |
| 11 | .390 | 168. | 10.1 | 175. |
| 12 | .390 | 168. | 10.1 | 175. |
| 13 | .390 | 168. | 10.1 | 175. |
| 14 | .400 | 172. | 10.1 | 175. |
| 15 | .390 | 168. | 10.1 | 175. |
| 16 | .390 | 168. | 10.1 | 175. |
| 17 | .400 | 172. | 10.1 | 175. |
| 18 | .410 | 176. | 10.1 | 175. |
| 19 | .430 | 185. | 10.1 | 175. |
| 20 | .430 | 185. | 10.1 | 175. |
| 21 | -1.000 | -430. | 10.1 | 175. |
| 22 | -1.000 | -430. | 10.1 | 175. |
| 23 | -1.000 | -430. | 10.1 | 175. |
| 24 | -1.000 | -430. | 10.1 | 175. |

DAY = 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 10.1 | 175. |
| 2 | .440 | 189. | 10.1 | 175. |
| 3 | .430 | 185. | 10.1 | 175. |
| 4 | .420 | 180. | 10.1 | 175. |
| 5 | .420 | 180. | 10.1 | 175. |
| 6 | .440 | 189. | 9.7 | 250. |
| 7 | .440 | 189. | 6.7 | 465. |
| 8 | .430 | 185. | 5.6 | 500. |
| 9 | .440 | 189. | 5.6 | 500. |
| 10 | .450 | 193. | 5.6 | 500. |
| 11 | .470 | 202. | 5.6 | 500. |
| 12 | .470 | 202. | 5.6 | 500. |
| 13 | .470 | 202. | 5.6 | 500. |
| 14 | .480 | 206. | 5.5 | 500. |
| 15 | .470 | 202. | 5.6 | 500. |
| 16 | .470 | 202. | 5.6 | 500. |
| 17 | .480 | 206. | 5.6 | 500. |
| 18 | .490 | 210. | 5.7 | 500. |
| 19 | .500 | 215. | 5.7 | 500. |
| 20 | .660 | 284. | 6.7 | 400. |
| 21 | .710 | 305. | 7.0 | 400. |
| 22 | .610 | 262. | 7.6 | 300. |
| 23 | .470 | 202. | 9.2 | 230. |
| 24 | .490 | 210. | 9.3 | 230. |

DAY = 77



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 9.3 | 230. |
| 2 | .420 | 180. | 10.0 | 180. |
| 3 | .410 | 176. | 10.1 | 180. |
| 4 | .410 | 176. | 10.1 | 180. |
| 5 | .420 | 180. | 10.1 | 180. |
| 6 | .490 | 210. | 9.3 | 340. |
| 7 | .470 | 202. | 6.4 | 485. |
| 8 | .450 | 193. | 5.7 | 490. |
| 9 | .460 | 198. | 5.6 | 490. |
| 10 | .470 | 202. | 5.6 | 490. |
| 11 | .460 | 198. | 5.7 | 490. |
| 12 | .450 | 193. | 5.8 | 490. |
| 13 | .450 | 193. | 5.7 | 490. |
| 14 | .420 | 180. | 5.6 | 490. |
| 15 | .430 | 185. | 5.6 | 490. |
| 16 | .520 | 223. | 6.7 | 390. |
| 17 | .540 | 232. | 6.9 | 390. |
| 18 | .550 | 236. | 6.9 | 390. |
| 19 | .460 | 198. | 6.0 | 490. |
| 20 | .440 | 189. | 5.8 | 490. |
| 21 | .450 | 193. | 5.8 | 490. |
| 22 | .500 | 215. | 6.2 | 390. |
| 23 | .560 | 241. | 7.0 | 390. |
| 24 | .550 | 236. | 7.1 | 390. |

DAY = 78

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | 7.9 | 280. |
| 2 | -1.000 | -430. | 9.1 | 230. |
| 3 | .460 | 198. | 9.9 | 230. |
| 4 | .390 | 168. | 10.0 | 230. |
| 5 | .400 | 172. | 8.5 | 310. |
| 6 | .570 | 245. | 7.6 | 360. |
| 7 | .690 | 296. | 7.3 | 360. |
| 8 | .580 | 249. | 6.6 | 480. |
| 9 | .480 | 206. | 5.8 | 480. |
| 10 | .490 | 210. | 5.8 | 480. |
| 11 | .550 | 236. | 6.2 | 420. |
| 12 | .540 | 232. | 7.0 | 350. |
| 13 | .540 | 232. | 7.7 | 325. |
| 14 | .590 | 253. | 7.8 | 320. |
| 15 | -1.000 | -430. | 8.1 | 285. |
| 16 | -1.000 | -430. | 10.0 | 180. |
| 17 | .380 | 163. | 10.1 | 180. |
| 18 | .380 | 163. | 10.1 | 180. |
| 19 | .380 | 163. | 10.1 | 180. |
| 20 | .380 | 163. | 10.1 | 180. |
| 21 | -1.000 | -430. | 10.1 | 180. |
| 22 | -1.000 | -430. | 10.1 | 180. |
| 23 | .380 | 163. | 10.1 | 175. |
| 24 | .370 | 159. | 10.1 | 175. |

DAY = 79



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | 10.1 | 175. |
| 2 | -1.000 | -430. | 10.1 | 175. |
| 3 | .380 | 163. | 10.1 | 175. |
| 4 | .380 | 163. | 10.1 | 175. |
| 5 | .370 | 159. | 10.1 | 175. |
| 6 | .370 | 159. | 10.1 | 175. |
| 7 | .370 | 159. | 10.0 | 175. |
| 8 | .370 | 159. | 10.0 | 180. |
| 9 | .370 | 159. | 10.0 | 180. |
| 10 | .370 | 159. | 10.0 | 180. |
| 11 | .390 | 168. | 10.0 | 180. |
| 12 | .570 | 245. | 9.8 | 200. |
| 13 | .570 | 245. | 9.8 | 180. |
| 14 | .420 | 180. | 10.0 | 180. |
| 15 | .420 | 180. | 10.0 | 178. |
| 16 | .420 | 180. | 10.0 | 180. |
| 17 | .410 | 176. | 10.0 | 180. |
| 18 | .400 | 172. | 10.0 | 180. |
| 19 | .410 | 176. | 10.0 | 180. |
| 20 | .420 | 180. | 10.0 | 180. |
| 21 | .410 | 176. | 10.0 | 180. |
| 22 | .420 | 180. | 10.1 | 180. |
| 23 | .420 | 180. | 10.1 | 180. |
| 24 | .420 | 180. | 10.1 | 180. |

DAY = 80

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.1 | 180. |
| 2 | .400 | 172. | 10.1 | 180. |
| 3 | .400 | 172. | 10.1 | 175. |
| 4 | .400 | 172. | 10.1 | 175. |
| 5 | .470 | 202. | 9.6 | 240. |
| 6 | .510 | 219. | 7.8 | 390. |
| 7 | .530 | 228. | 6.2 | 490. |
| 8 | .520 | 223. | 5.8 | 490. |
| 9 | .520 | 223. | 5.9 | 490. |
| 10 | .500 | 215. | 5.9 | 490. |
| 11 | .510 | 219. | 5.8 | 390. |
| 12 | .570 | 245. | 6.5 | 390. |
| 13 | .670 | 288. | 7.1 | 340. |
| 14 | .660 | 284. | 7.3 | 290. |
| 15 | .670 | 288. | 8.4 | 290. |
| 16 | .450 | 193. | 8.8 | 265. |
| 17 | .420 | 180. | 8.9 | 265. |
| 18 | .420 | 180. | 8.9 | 265. |
| 19 | .430 | 185. | 8.8 | 265. |
| 20 | .430 | 185. | 8.9 | 265. |
| 21 | .420 | 180. | 8.9 | 265. |
| 22 | .430 | 185. | 8.9 | 265. |
| 23 | .450 | 193. | 8.9 | 265. |
| 24 | .440 | 189. | 8.9 | 262. |

DAY = 81



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 8.8 | 280. |
| 2 | .460 | 198. | 8.3 | 300. |
| 3 | .460 | 198. | 8.3 | 300. |
| 4 | .450 | 193. | 8.2 | 300. |
| 5 | .440 | 189. | 8.2 | 300. |
| 6 | .450 | 193. | 8.2 | 300. |
| 7 | .450 | 193. | 8.0 | 300. |
| 8 | .450 | 193. | 8.1 | 300. |
| 9 | .450 | 193. | 8.1 | 300. |
| 10 | .510 | 219. | 7.7 | 350. |
| 11 | .560 | 241. | 7.3 | 350. |
| 12 | .570 | 245. | 7.3 | 350. |
| 13 | .570 | 245. | 7.3 | 350. |
| 14 | .590 | 253. | 7.4 | 300. |
| 15 | .650 | 279. | 8.1 | 300. |
| 16 | .660 | 284. | 8.0 | 300. |
| 17 | .680 | 292. | 8.0 | 300. |
| 18 | .680 | 292. | 8.0 | 310. |
| 19 | .630 | 271. | 7.6 | 325. |
| 20 | .640 | 275. | 7.7 | 325. |
| 21 | .620 | 266. | 7.7 | 325. |
| 22 | .630 | 271. | 7.8 | 325. |
| 23 | .640 | 275. | 7.8 | 325. |
| 24 | .650 | 279. | 7.8 | 325. |

DAY = 82

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.8 | 322. |
| 2 | .720 | 309. | 8.7 | 275. |
| 3 | .720 | 309. | 8.8 | 275. |
| 4 | .710 | 305. | 8.7 | 275. |
| 5 | .720 | 309. | 8.8 | 275. |
| 6 | .740 | 318. | 8.8 | 275. |
| 7 | .730 | 314. | 8.7 | 275. |
| 8 | .750 | 322. | 8.8 | 275. |
| 9 | .680 | 292. | 8.1 | 325. |
| 10 | .650 | 279. | 7.8 | 325. |
| 11 | .640 | 275. | 7.7 | 325. |
| 12 | .660 | 284. | 7.7 | 325. |
| 13 | .660 | 284. | 7.7 | 325. |
| 14 | .640 | 275. | 7.7 | 325. |
| 15 | .640 | 275. | 7.7 | 325. |
| 16 | .590 | 253. | 7.7 | 325. |
| 17 | .570 | 245. | 7.7 | 325. |
| 18 | .570 | 245. | 7.5 | 370. |
| 19 | .510 | 219. | 6.9 | 390. |
| 20 | .490 | 210. | 6.8 | 400. |
| 21 | .500 | 215. | 6.8 | 400. |
| 22 | .500 | 215. | 6.8 | 400. |
| 23 | .500 | 215. | 6.8 | 400. |
| 24 | .510 | 219. | 6.8 | 400. |

DAY = 83



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 6.8 | 400. |
| 2 | .510 | 219. | 6.8 | 400. |
| 3 | .510 | 219. | 6.9 | 400. |
| 4 | .520 | 223. | 6.9 | 400. |
| 5 | .520 | 223. | 6.9 | 400. |
| 6 | .560 | 241. | 7.3 | 325. |
| 7 | .590 | 253. | 7.7 | 340. |
| 8 | .520 | 223. | 7.0 | 400. |
| 9 | .560 | 241. | 6.8 | 430. |
| 10 | .610 | 262. | 6.4 | 440. |
| 11 | .610 | 262. | 6.4 | 445. |
| 12 | .620 | 266. | 6.4 | 445. |
| 13 | .620 | 266. | 6.4 | 445. |
| 14 | .610 | 262. | 6.4 | 445. |
| 15 | .610 | 262. | 6.4 | 445. |
| 16 | .590 | 253. | 6.4 | 445. |
| 17 | .570 | 245. | 6.3 | 425. |
| 18 | .600 | 258. | 6.4 | 460. |
| 19 | .550 | 236. | 6.1 | 450. |
| 20 | .650 | 279. | 7.1 | 375. |
| 21 | .680 | 292. | 7.2 | 375. |
| 22 | .640 | 275. | 6.8 | 425. |
| 23 | .640 | 275. | 6.7 | 425. |
| 24 | .650 | 279. | 6.7 | 425. |

DAY = 84

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.8 | 325. |
| 2 | .600 | 258. | 7.9 | 325. |
| 3 | .560 | 241. | 8.1 | 280. |
| 4 | .450 | 193. | 9.1 | 250. |
| 5 | .470 | 202. | 9.1 | 250. |
| 6 | .410 | 176. | 8.5 | 300. |
| 7 | .430 | 185. | 8.1 | 310. |
| 8 | .530 | 228. | 7.3 | 350. |
| 9 | .570 | 245. | 7.7 | 325. |
| 10 | .590 | 253. | 7.8 | 325. |
| 11 | .590 | 253. | 8.1 | 275. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .490 | 210. | 8.9 | 250. |
| 14 | .500 | 215. | 8.9 | 250. |
| 15 | .160 | 69. | 3.7 | 250. |
| 16 | -1.000 | -430. | 1.5 | 240. |
| 17 | -1.000 | -430. | 2.5 | 250. |
| 18 | .310 | 133. | 2.5 | 250. |
| 19 | .350 | 150. | 1.6 | 300. |
| 20 | .420 | 180. | 1.8 | 300. |
| 21 | .430 | 185. | 2.0 | 300. |
| 22 | .430 | 185. | 2.0 | 300. |
| 23 | .420 | 180. | 1.6 | 325. |
| 24 | .360 | 155. | 2.0 | 275. |

DAY = 85



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 2.4 | 275. |
| 2 | .370 | 159. | 2.5 | 275. |
| 3 | .360 | 155. | 2.5 | 275. |
| 4 | .380 | 163. | 2.6 | 272. |
| 5 | .370 | 159. | 2.6 | 272. |
| 6 | .380 | 163. | 1.8 | 322. |
| 7 | .380 | 163. | 1.5 | 371. |
| 8 | .550 | 236. | 7.2 | 325. |
| 9 | .560 | 241. | 7.6 | 300. |
| 10 | .430 | 185. | 8.3 | 270. |
| 11 | .460 | 198. | 8.4 | 275. |
| 12 | .470 | 202. | 8.4 | 275. |
| 13 | .480 | 206. | 8.5 | 275. |
| 14 | .470 | 202. | 8.5 | 275. |
| 15 | .470 | 202. | 8.5 | 275. |
| 16 | .460 | 198. | 8.5 | 275. |
| 17 | .460 | 198. | 8.5 | 275. |
| 18 | .470 | 202. | 7.9 | 370. |
| 19 | .450 | 193. | 6.9 | 380. |
| 20 | .440 | 189. | 6.9 | 380. |
| 21 | .450 | 193. | 7.0 | 380. |
| 22 | .470 | 202. | 7.0 | 380. |
| 23 | .480 | 206. | 7.1 | 380. |
| 24 | .490 | 210. | 7.1 | 378. |

DAY = 86

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .490 | 210. | 7.1 | 375. |
| 2 | .490 | 210. | 7.1 | 375. |
| 3 | .490 | 210. | 7.1 | 378. |
| 4 | .510 | 219. | 7.1 | 380. |
| 5 | .530 | 228. | 7.1 | 380. |
| 6 | .540 | 232. | 7.0 | 380. |
| 7 | .540 | 232. | 8.1 | 280. |
| 8 | .560 | 241. | 7.5 | 350. |
| 9 | .540 | 232. | 7.1 | 380. |
| 10 | .530 | 228. | 7.0 | 380. |
| 11 | .570 | 245. | 7.4 | 330. |
| 12 | .600 | 258. | 7.7 | 300. |
| 13 | .500 | 215. | 8.8 | 250. |
| 14 | .460 | 198. | 8.5 | 275. |
| 15 | .450 | 193. | 8.5 | 275. |
| 16 | .440 | 189. | 8.5 | 275. |
| 17 | .430 | 185. | 8.5 | 275. |
| 18 | .390 | 168. | 7.7 | 380. |
| 19 | .380 | 163. | 6.9 | 380. |
| 20 | .550 | 236. | 6.9 | 380. |
| 21 | .560 | 241. | 6.9 | 380. |
| 22 | .560 | 241. | 6.9 | 380. |
| 23 | .560 | 241. | 7.0 | 380. |
| 24 | .580 | 249. | 7.0 | 375. |

DAY = 87



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 7.6 | 320. |
| 2 | .460 | 198. | 7.6 | 320. |
| 3 | .530 | 228. | 7.6 | 320. |
| 4 | .530 | 228. | 7.6 | 322. |
| 5 | .550 | 236. | 7.6 | 322. |
| 6 | .550 | 236. | 7.6 | 322. |
| 7 | .480 | 206. | 7.0 | 375. |
| 8 | .530 | 228. | 6.5 | 425. |
| 9 | .570 | 245. | 6.5 | 425. |
| 10 | .570 | 245. | 6.5 | 425. |
| 11 | .590 | 253. | 6.9 | 390. |
| 12 | .550 | 236. | 7.0 | 360. |
| 13 | .570 | 245. | 7.7 | 325. |
| 14 | .580 | 249. | 7.7 | 325. |
| 15 | .580 | 249. | 7.8 | 325. |
| 16 | .580 | 249. | 7.8 | 325. |
| 17 | .570 | 245. | 7.8 | 325. |
| 18 | -1.000 | -430. | 7.4 | 420. |
| 19 | -1.000 | -430. | 6.4 | 450. |
| 20 | .380 | 163. | 6.4 | 430. |
| 21 | .400 | 172. | 6.4 | 430. |
| 22 | .400 | 172. | 6.4 | 430. |
| 23 | .400 | 172. | 6.4 | 430. |
| 24 | .450 | 193. | 6.4 | 430. |

DAY = 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 6.4 | 430. |
| 2 | .430 | 185. | 6.5 | 430. |
| 3 | .460 | 198. | 6.5 | 430. |
| 4 | .490 | 210. | 6.5 | 430. |
| 5 | .510 | 219. | 6.5 | 430. |
| 6 | .540 | 232. | 6.5 | 430. |
| 7 | .550 | 236. | 6.6 | 430. |
| 8 | .530 | 228. | 6.5 | 430. |
| 9 | .540 | 232. | 6.6 | 430. |
| 10 | .510 | 219. | 6.5 | 440. |
| 11 | .510 | 219. | 6.5 | 435. |
| 12 | .490 | 210. | 6.7 | 415. |
| 13 | .500 | 215. | 6.9 | 380. |
| 14 | .510 | 219. | 7.1 | 375. |
| 15 | .500 | 215. | 7.1 | 375. |
| 16 | .500 | 215. | 7.1 | 375. |
| 17 | .500 | 215. | 7.1 | 375. |
| 18 | .510 | 219. | 7.1 | 375. |
| 19 | .490 | 210. | 7.3 | 345. |
| 20 | .290 | 125. | 7.7 | 330. |
| 21 | .340 | 146. | 7.7 | 330. |
| 22 | .340 | 146. | 7.8 | 330. |
| 23 | .350 | 150. | 7.7 | 330. |
| 24 | .380 | 163. | 7.7 | 330. |

DAY = 89



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 7.7 | 330. |
| 2 | .380 | 163. | 7.7 | 330. |
| 3 | .420 | 180. | 8.5 | 280. |
| 4 | .430 | 185. | 8.6 | 280. |
| 5 | .430 | 185. | 8.6 | 280. |
| 6 | .430 | 185. | 8.6 | 280. |
| 7 | .420 | 180. | 8.6 | 280. |
| 8 | .410 | 176. | 8.4 | 280. |
| 9 | .390 | 168. | 8.2 | 325. |
| 10 | .380 | 163. | 7.7 | 325. |
| 11 | .380 | 163. | 7.7 | 325. |
| 12 | .410 | 176. | 6.3 | 480. |
| 13 | .390 | 168. | 5.6 | 480. |
| 14 | .410 | 176. | 5.5 | 485. |
| 15 | .430 | 185. | 5.6 | 485. |
| 16 | .450 | 193. | 5.6 | 485. |
| 17 | .450 | 193. | 5.6 | 485. |
| 18 | .420 | 180. | 5.7 | 485. |
| 19 | .450 | 193. | 6.0 | 415. |
| 20 | .440 | 189. | 7.3 | 330. |
| 21 | .450 | 193. | 7.6 | 330. |
| 22 | .460 | 198. | 7.7 | 330. |
| 23 | .450 | 193. | 7.7 | 330. |
| 24 | .460 | 198. | 7.6 | 330. |

DAY = 90

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 7.6 | 330. |
| 2 | .470 | 202. | 7.6 | 330. |
| 3 | .460 | 198. | 7.6 | 330. |
| 4 | .570 | 245. | 7.6 | 330. |
| 5 | .600 | 258. | 7.6 | 330. |
| 6 | .540 | 232. | 7.2 | 375. |
| 7 | .570 | 245. | 7.0 | 400. |
| 8 | .560 | 241. | 5.9 | 490. |
| 9 | -1.000 | -430. | 5.8 | 485. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | -1.000 | -430. | 5.8 | 490. |
| 12 | .500 | 215. | 5.9 | 460. |
| 13 | .460 | 198. | 6.6 | 390. |
| 14 | .490 | 210. | 7.2 | 350. |
| 15 | .430 | 185. | 8.2 | 375. |
| 16 | .480 | 206. | 6.7 | 420. |
| 17 | .440 | 189. | 6.1 | 475. |
| 18 | .420 | 180. | 5.7 | 490. |
| 19 | .410 | 176. | 5.7 | 490. |
| 20 | .400 | 172. | 5.8 | 490. |
| 21 | .400 | 172. | 5.8 | 490. |
| 22 | .400 | 172. | 5.7 | 490. |
| 23 | .400 | 172. | 5.7 | 490. |
| 24 | .410 | 176. | 5.7 | 490. |

DAY = 91



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 5.7 | 490. |
| 2 | .420 | 180. | 5.8 | 490. |
| 3 | .430 | 185. | 5.7 | 490. |
| 4 | .440 | 189. | 5.7 | 490. |
| 5 | .430 | 185. | 5.8 | 490. |
| 6 | .420 | 180. | 5.8 | 490. |
| 7 | .440 | 189. | 5.8 | 490. |
| 8 | .440 | 189. | 5.6 | 490. |
| 9 | .440 | 189. | 5.7 | 495. |
| 10 | .410 | 176. | 5.7 | 500. |
| 11 | .420 | 180. | 5.6 | 495. |
| 12 | .420 | 180. | 5.6 | 495. |
| 13 | .420 | 180. | 5.6 | 490. |
| 14 | .470 | 202. | 6.1 | 420. |
| 15 | .570 | 245. | 7.0 | 385. |
| 16 | .530 | 228. | 6.9 | 420. |
| 17 | .420 | 180. | 6.0 | 485. |
| 18 | .390 | 168. | 5.5 | 485. |
| 19 | .420 | 180. | 6.2 | 370. |
| 20 | .370 | 159. | 7.0 | 340. |
| 21 | .420 | 180. | 7.5 | 340. |
| 22 | .420 | 180. | 7.5 | 340. |
| 23 | .450 | 193. | 7.6 | 290. |
| 24 | .580 | 249. | 9.6 | 200. |

DAY = 92

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 9.9 | 490. |
| 2 | .430 | 185. | 10.1 | 490. |
| 3 | .440 | 189. | 10.1 | 490. |
| 4 | .530 | 228. | 10.1 | 490. |
| 5 | .640 | 275. | 10.2 | 490. |
| 6 | .600 | 258. | 9.7 | 490. |
| 7 | .470 | 202. | 7.3 | 490. |
| 8 | .440 | 189. | 6.3 | 490. |
| 9 | .540 | 232. | 7.0 | 495. |
| 10 | .580 | 249. | 6.9 | 500. |
| 11 | .520 | 223. | 7.0 | 495. |
| 12 | .520 | 223. | 7.0 | 495. |
| 13 | .530 | 228. | 7.0 | 490. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | .8 | 385. |
| 16 | .370 | 159. | .8 | 420. |
| 17 | .370 | 159. | .8 | 485. |
| 18 | .370 | 159. | .8 | 485. |
| 19 | .360 | 155. | .8 | 370. |
| 20 | .350 | 150. | .9 | 340. |
| 21 | .390 | 168. | 1.2 | 340. |
| 22 | .400 | 172. | 1.6 | 340. |
| 23 | .400 | 172. | 2.0 | 290. |
| 24 | .380 | 163. | 3.3 | 200. |

DAY = 93

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 4.0 | 180. |
| 2 | .380 | 163. | 4.0 | 180. |
| 3 | .380 | 163. | 4.0 | 180. |
| 4 | .380 | 163. | 4.0 | 180. |
| 5 | .380 | 163. | 4.0 | 180. |
| 6 | .350 | 150. | 3.4 | 180. |
| 7 | .380 | 163. | 1.5 | 480. |
| 8 | .500 | 215. | 6.8 | 390. |
| 9 | .510 | 219. | 6.9 | 390. |
| 10 | .520 | 223. | 6.9 | 390. |
| 11 | .580 | 249. | 6.8 | 390. |
| 12 | .580 | 249. | 6.7 | 390. |
| 13 | .720 | 309. | 7.7 | 390. |
| 14 | .770 | 331. | 7.9 | 390. |
| 15 | .770 | 331. | 7.9 | 390. |
| 16 | .770 | 331. | 7.9 | 388. |
| 17 | .780 | 335. | 7.9 | 388. |
| 18 | .790 | 339. | 8.0 | 388. |
| 19 | .770 | 331. | 8.0 | 388. |
| 20 | .620 | 266. | 8.0 | 355. |
| 21 | .630 | 271. | 8.0 | 365. |
| 22 | .620 | 266. | 7.8 | 322. |
| 23 | .610 | 262. | 7.7 | 322. |
| 24 | .630 | 271. | 7.8 | 225. |

DAY = 94

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 7.8 | 332. |
| 2 | .630 | 271. | 7.9 | 333. |
| 3 | .630 | 271. | 7.8 | 333. |
| 4 | .630 | 271. | 7.8 | 332. |
| 5 | .630 | 271. | 7.8 | 332. |
| 6 | .630 | 271. | 7.8 | 335. |
| 7 | .570 | 245. | 7.2 | 415. |
| 8 | .570 | 245. | 6.5 | 465. |
| 9 | .590 | 253. | 6.5 | 420. |
| 10 | .620 | 266. | 6.8 | 420. |
| 11 | .600 | 258. | 6.8 | 420. |
| 12 | .580 | 249. | 6.8 | 420. |
| 13 | .600 | 258. | 6.7 | 420. |
| 14 | .600 | 258. | 6.7 | 420. |
| 15 | .600 | 258. | 6.8 | 420. |
| 16 | .600 | 258. | 6.8 | 418. |
| 17 | .620 | 266. | 6.8 | 418. |
| 18 | .630 | 271. | 6.8 | 418. |
| 19 | .640 | 275. | 6.8 | 418. |
| 20 | .620 | 266. | 6.9 | 418. |
| 21 | .630 | 271. | 6.8 | 418. |
| 22 | .640 | 275. | 6.8 | 418. |
| 23 | .640 | 275. | 6.8 | 418. |
| 24 | .660 | 284. | 6.8 | 420. |

APPENDIX D

OKLAHOMA GAS & ELECTRIC

MUSKOGEE STATION - UNIT 5

Input Data - Initial Analysis

**PULVERIZED COAL-FIRED UTILITY BOILER NOx EMISSION MONITORING**

DATA SUBMITTED BY OKLAHOMA GAS AND ELECTRIC

MUSKOGEE STATION UNIT 5 SUBBITUMINOUS COAL MON. REL. ACC. = 18.2 PC

DAY 1 IS OCTOBER 15, 1980 DAY 94 IS JANUARY 16, 1981

550 MWE, COMBUSTION ENGINEERING BOILER WITH OVERFIRE AIR

COAL PROPERTIES IDENTICAL TO UNIT 4

BOILER OFF-LINE FROM DEC. 13, 1980 TO DEC. 24, 1980 INCLUSIVE

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 8.2 | 230. |
| 2 | .480 | 206. | 10.0 | 180. |
| 3 | .490 | 210. | 10.0 | 180. |
| 4 | .490 | 210. | 10.0 | 180. |
| 5 | .490 | 210. | 10.0 | 180. |
| 6 | .490 | 210. | 10.0 | 180. |
| 7 | .410 | 176. | 8.7 | 295. |
| 8 | .230 | 99. | 5.6 | 405. |
| 9 | .160 | 69. | 4.6 | 411. |
| 10 | .160 | 69. | 4.5 | 411. |
| 11 | .150 | 64. | 4.5 | 419. |
| 12 | .150 | 64. | 4.1 | 428. |
| 13 | .160 | 69. | 4.1 | 424. |
| 14 | .150 | 64. | 4.2 | 423. |
| 15 | .150 | 64. | 4.1 | 424. |
| 16 | .150 | 64. | 4.0 | 420. |
| 17 | .140 | 60. | 3.7 | 420. |
| 18 | .140 | 60. | 3.7 | 420. |
| 19 | .140 | 60. | 3.5 | 420. |
| 20 | .150 | 64. | 3.5 | 420. |
| 21 | .170 | 73. | 4.4 | 380. |
| 22 | .270 | 116. | 6.3 | 330. |
| 23 | .310 | 133. | 6.8 | 330. |
| 24 | .310 | 133. | 6.8 | 325. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.8 | 325. |
| 2 | .350 | 150. | 7.7 | 280. |
| 3 | .370 | 159. | 9.0 | 180. |
| 4 | .400 | 172. | 10.0 | 180. |
| 5 | .390 | 168. | 10.0 | 180. |
| 6 | .370 | 159. | 9.3 | 265. |
| 7 | .220 | 95. | 5.4 | 425. |
| 8 | .180 | 77. | 2.5 | 469. |
| 9 | .180 | 77. | 2.8 | 471. |
| 10 | .190 | 82. | 3.3 | 472. |
| 11 | .180 | 77. | 3.4 | 490. |
| 12 | .160 | 69. | 1.8 | 509. |
| 13 | .150 | 64. | 1.5 | 508. |
| 14 | .190 | 82. | 2.5 | 514. |
| 15 | .230 | 99. | 2.8 | 514. |
| 16 | .220 | 95. | 2.7 | 514. |
| 17 | .200 | 86. | 2.6 | 515. |
| 18 | .230 | 99. | 3.4 | 500. |
| 19 | .260 | 112. | 4.2 | 480. |
| 20 | .240 | 103. | 4.1 | 400. |

| | | | | |
|---|---|---|---|---|
| 21 | .320 | 137. | 7.5 | 325. |
| 22 | .350 | 150. | 7.8 | 325. |
| 23 | .360 | 155. | 8.1 | 325. |
| 24 | .370 | 159. | 8.0 | 325. |

DAY = 3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 8.4 | 280. |
| 2 | .490 | 210. | 10.0 | 180. |
| 3 | .450 | 193. | 10.0 | 180. |
| 4 | .430 | 185. | 10.0 | 180. |
| 5 | .430 | 185. | 10.0 | 180. |
| 6 | .430 | 185. | 10.0 | 180. |
| 7 | .430 | 185. | 9.9 | 220. |
| 8 | .460 | 198. | 9.2 | 280. |
| 9 | .390 | 168. | 8.5 | 320. |
| 10 | .380 | 163. | 7.8 | 325. |
| 11 | .410 | 176. | 8.0 | 325. |
| 12 | .460 | 198. | 8.1 | 325. |
| 13 | .460 | 198. | 8.2 | 325. |
| 14 | .450 | 193. | 8.3 | 325. |
| 15 | .440 | 189. | 8.3 | 325. |
| 16 | .450 | 193. | 8.4 | 325. |
| 17 | .500 | 215. | 8.8 | 280. |
| 18 | .520 | 223. | 9.9 | 225. |
| 19 | .600 | 258. | 9.9 | 225. |
| 20 | .610 | 262. | 9.9 | 225. |
| 21 | .620 | 266. | 9.9 | 225. |
| 22 | .630 | 271. | 9.9 | 225. |
| 23 | .620 | 266. | 9.9 | 225. |
| 24 | .630 | 271. | 9.8 | 225. |

DAY = 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 9.8 | 226. |
| 2 | .560 | 241. | 9.9 | 190. |
| 3 | .530 | 228. | 10.0 | 180. |
| 4 | .520 | 223. | 10.0 | 181. |
| 5 | .510 | 219. | 10.0 | 180. |
| 6 | .500 | 215. | 10.0 | 180. |
| 7 | .500 | 215. | 10.0 | 180. |
| 8 | .490 | 210. | 10.0 | 180. |
| 9 | .480 | 206. | 10.0 | 180. |
| 10 | .460 | 198. | 9.9 | 290. |
| 11 | .390 | 168. | 8.2 | 325. |
| 12 | .450 | 193. | 8.3 | 325. |
| 13 | .440 | 189. | 8.3 | 325. |
| 14 | .450 | 193. | 8.4 | 325. |
| 15 | .440 | 189. | 8.3 | 325. |
| 16 | .470 | 202. | 8.5 | 330. |
| 17 | .470 | 202. | 8.4 | 330. |
| 18 | .470 | 202. | 8.4 | 330. |
| 19 | .450 | 193. | 8.4 | 330. |

| | | | | |
|---|---|---|---|---|
| 20 | .470 | 202. | 8.5 | 330. |
| 21 | .480 | 206. | 8.5 | 330. |
| 22 | .480 | 206. | 8.5 | 330. |
| 23 | .560 | 241. | 9.6 | 200. |
| 24 | .540 | 232. | 10.0 | 154. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 10.0 | 180. |
| 2 | .500 | 215. | 10.0 | 180. |
| 3 | .500 | 215. | 10.0 | 181. |
| 4 | .470 | 202. | 10.0 | 180. |
| 5 | .470 | 202. | 10.0 | 180. |
| 6 | .470 | 202. | 10.0 | 181. |
| 7 | .470 | 202. | 10.0 | 180. |
| 8 | .480 | 206. | 10.0 | 180. |
| 9 | .480 | 206. | 10.0 | 180. |
| 10 | .470 | 202. | 10.0 | 180. |
| 11 | .480 | 206. | 10.0 | 180. |
| 12 | .490 | 210. | 10.0 | 180. |
| 13 | .480 | 206. | 10.0 | 180. |
| 14 | .490 | 210. | 10.0 | 180. |
| 15 | .490 | 210. | 10.0 | 180. |
| 16 | .480 | 206. | 10.0 | 180. |
| 17 | .460 | 198. | 10.0 | 180. |
| 18 | .460 | 198. | 10.0 | 180. |
| 19 | .470 | 202. | 10.0 | 180. |
| 20 | .480 | 206. | 10.0 | 180. |
| 21 | .500 | 215. | 10.0 | 180. |
| 22 | .500 | 215. | 10.0 | 180. |
| 23 | .480 | 206. | 10.0 | 180. |
| 24 | .480 | 206. | 10.0 | 180. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .490 | 210. | 10.0 | 179. |
| 2 | .480 | 206. | 10.0 | 179. |
| 3 | .510 | 219. | 10.0 | 179. |
| 4 | .520 | 223. | 10.0 | 179. |
| 5 | .510 | 219. | 10.0 | 180. |
| 6 | .520 | 223. | 10.0 | 180. |
| 7 | .510 | 219. | 9.7 | 176. |
| 8 | .440 | 189. | 8.1 | 325. |
| 9 | .480 | 206. | 8.3 | 325. |
| 10 | .480 | 206. | 8.4 | 325. |
| 11 | .490 | 210. | 8.4 | 325. |
| 12 | .500 | 215. | 8.4 | 325. |
| 13 | .480 | 206. | 8.4 | 325. |
| 14 | .500 | 215. | 8.5 | 325. |
| 15 | .490 | 210. | 8.5 | 325. |
| 16 | .490 | 210. | 8.5 | 325. |
| 17 | .480 | 206. | 8.5 | 325. |
| 18 | .500 | 215. | 8.6 | 325. |

| | | | | |
|---|---|---|---|---|
| 19 | .500 | 215. | 9.2 | 280. |
| 20 | .470 | 202. | 8.4 | 330. |
| 21 | .480 | 206. | 8.3 | 330. |
| 22 | .510 | 219. | 9.5 | 220. |
| 23 | .550 | 236. | 9.9 | 220. |
| 24 | .570 | 245. | 9.9 | 213. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 10.0 | 180. |
| 2 | .510 | 219. | 10.0 | 181. |
| 3 | .510 | 219. | 10.0 | 180. |
| 4 | .520 | 223. | 10.0 | 180. |
| 5 | .500 | 215. | 10.0 | 180. |
| 6 | .510 | 219. | 10.0 | 180. |
| 7 | .500 | 215. | 9.6 | 231. |
| 8 | .460 | 198. | 8.2 | 325. |
| 9 | .480 | 206. | 8.2 | 325. |
| 10 | .470 | 202. | 8.2 | 325. |
| 11 | .490 | 210. | 8.3 | 325. |
| 12 | .490 | 210. | 8.4 | 325. |
| 13 | .490 | 210. | 8.3 | 325. |
| 14 | .460 | 198. | 8.3 | 325. |
| 15 | .470 | 202. | 8.4 | 325. |
| 16 | .470 | 202. | 8.4 | 330. |
| 17 | .490 | 210. | 8.4 | 330. |
| 18 | .510 | 219. | 8.4 | 330. |
| 19 | .530 | 228. | 8.4 | 330. |
| 20 | .500 | 215. | 8.4 | 330. |
| 21 | .510 | 219. | 8.4 | 330. |
| 22 | .530 | 228. | 9.2 | 230. |
| 23 | .640 | 275. | 10.0 | 230. |
| 24 | .610 | 262. | 10.0 | 227. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 10.0 | 221. |
| 2 | .510 | 219. | 10.0 | 180. |
| 3 | .530 | 228. | 10.0 | 181. |
| 4 | .510 | 219. | 10.0 | 180. |
| 5 | .500 | 215. | 10.0 | 180. |
| 6 | .510 | 219. | 10.0 | 193. |
| 7 | .580 | 249. | 10.0 | 227. |
| 8 | .490 | 210. | 9.2 | 310. |
| 9 | .420 | 180. | 8.5 | 310. |
| 10 | .400 | 172. | 8.4 | 310. |
| 11 | .410 | 176. | 8.5 | 315. |
| 12 | .480 | 206. | 9.1 | 270. |
| 13 | .490 | 210. | 9.1 | 280. |
| 14 | .490 | 210. | 9.1 | 280. |
| 15 | .490 | 210. | 9.1 | 280. |
| 16 | .480 | 206. | 9.0 | 280. |
| 17 | .480 | 206. | 9.1 | 280. |

| | | | | |
|---|---|---|---|---|
| 18 | .490 | 210. | 9.1 | 280. |
| 19 | .510 | 219. | 9.1 | 280. |
| 20 | .510 | 219. | 9.1 | 280. |
| 21 | .490 | 210. | 9.2 | 280. |
| 22 | .540 | 232. | 9.5 | 230. |
| 23 | .600 | 258. | 10.0 | 230. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.0 | 180. |
| 2 | .380 | 163. | 10.0 | 180. |
| 3 | .450 | 193. | 10.0 | 180. |
| 4 | .460 | 198. | 10.0 | 180. |
| 5 | .470 | 202. | 10.0 | 180. |
| 6 | .480 | 206. | 10.0 | 186. |
| 7 | .580 | 249. | 10.0 | 226. |
| 8 | .600 | 258. | 10.0 | 225. |
| 9 | .540 | 232. | 9.6 | 280. |
| 10 | .490 | 210. | 8.7 | 355. |
| 11 | .430 | 185. | 7.7 | 355. |
| 12 | .440 | 189. | 7.8 | 350. |
| 13 | .450 | 193. | 7.9 | 350. |
| 14 | .450 | 193. | 7.8 | 350. |
| 15 | .440 | 189. | 7.7 | 350. |
| 16 | .440 | 189. | 7.8 | 350. |
| 17 | .460 | 198. | 8.1 | 330. |
| 18 | .480 | 206. | 8.2 | 330. |
| 19 | .500 | 215. | 8.2 | 325. |
| 20 | .490 | 210. | 8.2 | 325. |
| 21 | .550 | 236. | 8.2 | 325. |
| 22 | .570 | 245. | 9.5 | 200. |
| 23 | .540 | 232. | 10.0 | 182. |
| 24 | .570 | 245. | 9.9 | 181. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 10.0 | 180. |
| 2 | .560 | 241. | 10.0 | 180. |
| 3 | .560 | 241. | 10.0 | 180. |
| 4 | .540 | 232. | 10.0 | 180. |
| 5 | .520 | 223. | 10.0 | 180. |
| 6 | .530 | 228. | 10.0 | 181. |
| 7 | .550 | 236. | 10.0 | 180. |
| 8 | .500 | 215. | 9.6 | 280. |
| 9 | .420 | 180. | 8.7 | 330. |
| 10 | .430 | 185. | 8.1 | 330. |
| 11 | .460 | 198. | 8.2 | 340. |
| 12 | .440 | 189. | 7.1 | 430. |
| 13 | .470 | 202. | 7.0 | 430. |
| 14 | .470 | 202. | 7.0 | 430. |
| 15 | .480 | 206. | 7.0 | 430. |
| 16 | .490 | 210. | 7.0 | 425. |

| | | | | |
|---|---|---|---|---|
| 17 | .480 | 206. | 6.9 | 428. |
| 18 | .480 | 206. | 6.9 | 428. |
| 19 | .480 | 206. | 7.0 | 426. |
| 20 | .500 | 215. | 7.0 | 426. |
| 21 | .510 | 219. | 7.0 | 426. |
| 22 | .540 | 232. | 7.3 | 345. |
| 23 | .540 | 232. | 8.6 | 312. |
| 24 | .570 | 245. | 8.9 | 290. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 10.0 | 225. |
| 2 | .590 | 253. | 10.0 | 180. |
| 3 | .580 | 249. | 10.0 | 180. |
| 4 | .580 | 249. | 10.0 | 180. |
| 5 | .570 | 245. | 10.0 | 180. |
| 6 | .570 | 245. | 10.0 | 180. |
| 7 | .570 | 245. | 10.0 | 230. |
| 8 | .450 | 193. | 8.7 | 330. |
| 9 | .490 | 210. | 7.4 | 450. |
| 10 | .510 | 219. | 6.5 | 450. |
| 11 | .510 | 219. | 6.6 | 450. |
| 12 | .490 | 210. | 7.0 | 380. |
| 13 | .470 | 202. | 7.6 | 330. |
| 14 | .560 | 241. | 8.4 | 330. |
| 15 | .560 | 241. | 9.3 | 230. |
| 16 | .630 | 271. | 10.0 | 226. |
| 17 | .620 | 266. | 10.0 | 226. |
| 18 | .640 | 275. | 10.0 | 226. |
| 19 | .650 | 279. | 10.0 | 270. |
| 20 | .540 | 232. | 8.8 | 310. |
| 21 | .530 | 228. | 8.9 | 280. |
| 22 | .510 | 219. | 9.3 | 274. |
| 23 | .610 | 262. | 9.9 | 180. |
| 24 | .570 | 245. | 10.0 | 180. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 10.0 | 180. |
| 2 | .570 | 245. | 10.0 | 180. |
| 3 | .570 | 245. | 10.0 | 180. |
| 4 | .560 | 241. | 10.0 | 180. |
| 5 | .560 | 241. | 10.0 | 180. |
| 6 | .550 | 236. | 10.0 | 180. |
| 7 | .550 | 236. | 10.0 | 180. |
| 8 | .560 | 241. | 10.0 | 330. |
| 9 | .470 | 202. | 8.8 | 330. |
| 10 | .460 | 198. | 8.3 | 330. |
| 11 | .450 | 193. | 8.4 | 330. |
| 12 | .460 | 198. | 8.4 | 330. |
| 13 | .460 | 198. | 8.4 | 330. |
| 14 | .470 | 202. | 8.5 | 330. |
| 15 | .470 | 202. | 8.5 | 330. |

| | | | | |
|---|---|---|---|---|
| 16 | .470 | 202. | 8.5 | 256. |
| 17 | .510 | 219. | 9.1 | 256. |
| 18 | .530 | 228. | 9.6 | 270. |
| 19 | .510 | 219. | 9.4 | 282. |
| 20 | .450 | 193. | 9.1 | 280. |
| 21 | .450 | 193. | 9.1 | 228. |
| 22 | .620 | 266. | 9.8 | 182. |
| 23 | .610 | 262. | 10.0 | 182. |
| 24 | .560 | 241. | 10.0 | 180. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 10.0 | 180. |
| 2 | .560 | 241. | 10.0 | 180. |
| 3 | .560 | 241. | 10.0 | 180. |
| 4 | .550 | 236. | 10.0 | 180. |
| 5 | .550 | 236. | 10.0 | 180. |
| 6 | .550 | 236. | 10.0 | 180. |
| 7 | .520 | 223. | 10.0 | 350. |
| 8 | .530 | 228. | 8.7 | 430. |
| 9 | .420 | 180. | 6.8 | 430. |
| 10 | .420 | 180. | 6.5 | 480. |
| 11 | .330 | 142. | 5.4 | 480. |
| 12 | .320 | 137. | 5.3 | 480. |
| 13 | .330 | 142. | 5.3 | 480. |
| 14 | .360 | 155. | 5.3 | 480. |
| 15 | .360 | 155. | 5.3 | 480. |
| 16 | .360 | 155. | 5.5 | 468. |
| 17 | .390 | 168. | 5.7 | 468. |
| 18 | .390 | 168. | 5.6 | 468. |
| 19 | .360 | 155. | 5.7 | 470. |
| 20 | .360 | 155. | 5.9 | 465. |
| 21 | .370 | 159. | 6.3 | 426. |
| 22 | .380 | 163. | 6.7 | 375. |
| 23 | .400 | 172. | 7.6 | 328. |
| 24 | .410 | 176. | 8.4 | 278. |

DAY = 14

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 8.4 | 278. |
| 2 | .420 | 180. | 8.5 | 278. |
| 3 | .420 | 180. | 8.5 | 275. |
| 4 | .430 | 185. | 8.5 | 275. |
| 5 | .440 | 189. | 8.5 | 275. |
| 6 | .420 | 180. | 8.3 | 310. |
| 7 | .330 | 142. | 6.3 | 425. |
| 8 | .300 | 129. | 6.1 | 425. |
| 9 | .320 | 137. | 6.1 | 425. |
| 10 | .320 | 137. | 6.2 | 425. |
| 11 | .340 | 146. | 6.3 | 425. |
| 12 | .350 | 150. | 6.1 | 425. |
| 13 | .310 | 133. | 6.1 | 425. |
| 14 | .280 | 120. | 6.2 | 425. |

| | | | | |
|---|---|---|---|---|
| 15 | .290 | 125. | 6.2 | 425. |
| 16 | .290 | 125. | 6.2 | 428. |
| 17 | .300 | 129. | 6.3 | 427. |
| 18 | .290 | 125. | 6.3 | 427. |
| 19 | .240 | 103. | 6.2 | 427. |
| 20 | .250 | 107. | 6.2 | 425. |
| 21 | .250 | 107. | 6.2 | 428. |
| 22 | .260 | 112. | 6.2 | 428. |
| 23 | .320 | 137. | 7.0 | 352. |
| 24 | .290 | 125. | 7.8 | 305. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 7.9 | 305. |
| 2 | .250 | 107. | 7.9 | 305. |
| 3 | .260 | 112. | 7.9 | 300. |
| 4 | .260 | 112. | 7.9 | 300. |
| 5 | .250 | 107. | 7.9 | 300. |
| 6 | .250 | 107. | 7.8 | 305. |
| 7 | .260 | 112. | 5.8 | 430. |
| 8 | .270 | 116. | 5.6 | 430. |
| 9 | .280 | 120. | 6.0 | 440. |
| 10 | .270 | 116. | 6.0 | 440. |
| 11 | .280 | 120. | 6.1 | 440. |
| 12 | .280 | 120. | 6.0 | 440. |
| 13 | .290 | 125. | 6.0 | 440. |
| 14 | .270 | 116. | 5.9 | 440. |
| 15 | .280 | 120. | 5.9 | 440. |
| 16 | .280 | 120. | 5.9 | 440. |
| 17 | .300 | 129. | 5.9 | 440. |
| 18 | .290 | 125. | 6.0 | 440. |
| 19 | .290 | 125. | 6.1 | 440. |
| 20 | .280 | 120. | 6.2 | 440. |
| 21 | .290 | 125. | 6.1 | 440. |
| 22 | .300 | 129. | 6.1 | 440. |
| 23 | .330 | 142. | 6.7 | 300. |
| 24 | .390 | 168. | 7.9 | 305. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 8.0 | 305. |
| 2 | .390 | 168. | 8.0 | 305. |
| 3 | .390 | 168. | 8.0 | 305. |
| 4 | .390 | 168. | 8.0 | 300. |
| 5 | -1.000 | -430. | -1.0 | -1. |
| 6 | -1.000 | -430. | -1.0 | -1. |
| 7 | -1.000 | -430. | -1.0 | -1. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .360 | 155. | 10.0 | 175. |
| 11 | .640 | 275. | 9.8 | 200. |
| 12 | .290 | 125. | 8.9 | 280. |
| 13 | .340 | 146. | 8.0 | 280. |

| | | | | |
|---|---|---|---|---|
| 14 | .380 | 163. | 8.0 | 280. |
| 15 | .390 | 168. | 8.0 | 280. |
| 16 | .380 | 163. | 8.0 | 280. |
| 17 | .410 | 176. | 8.2 | 280. |
| 18 | .410 | 176. | 8.3 | 280. |
| 19 | .420 | 180. | 8.3 | 280. |
| 20 | .430 | 185. | 8.3 | 280. |
| 21 | .420 | 180. | 8.3 | 280. |
| 22 | .430 | 185. | 8.3 | 280. |
| 23 | .420 | 180. | 8.2 | 280. |
| 24 | .420 | 180. | 8.1 | 280. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 8.2 | 275. |
| 2 | .430 | 185. | 8.2 | 280. |
| 3 | .420 | 180. | 8.2 | 280. |
| 4 | .420 | 180. | 8.2 | 280. |
| 5 | .420 | 180. | 8.2 | 280. |
| 6 | .420 | 180. | 8.2 | 280. |
| 7 | .430 | 185. | 8.2 | 280. |
| 8 | .420 | 180. | 8.1 | 280. |
| 9 | .440 | 189. | 8.2 | 280. |
| 10 | .450 | 193. | 8.3 | 280. |
| 11 | .470 | 202. | 8.2 | 280. |
| 12 | .460 | 198. | 8.2 | 280. |
| 13 | .420 | 180. | 7.8 | 335. |
| 14 | .300 | 129. | 5.8 | 472. |
| 15 | .290 | 125. | 5.3 | 488. |
| 16 | .340 | 146. | 7.6 | 255. |
| 17 | .410 | 176. | 10.0 | 180. |
| 18 | .400 | 172. | 10.0 | 180. |
| 19 | .400 | 172. | 10.0 | 180. |
| 20 | .390 | 168. | 10.0 | 180. |
| 21 | .390 | 168. | 10.0 | 180. |
| 22 | .390 | 168. | 10.0 | 180. |
| 23 | .400 | 172. | 10.0 | 180. |
| 24 | .420 | 180. | 10.0 | 180. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.0 | 180. |
| 2 | .410 | 176. | 10.0 | 180. |
| 3 | .400 | 172. | 10.0 | 180. |
| 4 | .410 | 176. | 10.0 | 180. |
| 5 | .400 | 172. | 10.0 | 180. |
| 6 | .390 | 168. | 10.0 | 180. |
| 7 | .430 | 185. | 9.8 | 210. |
| 8 | .450 | 193. | 9.5 | 214. |
| 9 | .460 | 198. | 9.8 | 214. |
| 10 | .460 | 198. | 9.5 | 215. |
| 11 | .450 | 193. | 9.8 | 215. |
| 12 | .440 | 189. | 9.3 | 214. |

| | | | | |
|---|---|---|---|---|
| 13 | .450 | 193. | 9.3 | 215. |
| 14 | .450 | 193. | 9.4 | 215. |
| 15 | .460 | 198. | 9.4 | 215. |
| 16 | .460 | 198. | 9.4 | 215. |
| 17 | .460 | 198. | 9.4 | 215. |
| 18 | .460 | 198. | 9.3 | 215. |
| 19 | .450 | 193. | 9.3 | 215. |
| 20 | .460 | 198. | 9.4 | 215. |
| 21 | .460 | 198. | 9.4 | 215. |
| 22 | .470 | 202. | 9.4 | 215. |
| 23 | .440 | 189. | 9.8 | 175. |
| 24 | .370 | 159. | 10.0 | 180. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 10.0 | 180. |
| 2 | .420 | 180. | 10.0 | 180. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .420 | 180. | 10.0 | 180. |
| 5 | .410 | 176. | 10.0 | 180. |
| 6 | .410 | 176. | 10.0 | 180. |
| 7 | .390 | 168. | 10.0 | 180. |
| 8 | .390 | 168. | 10.0 | 180. |
| 9 | .400 | 172. | 10.0 | 180. |
| 10 | .390 | 168. | 9.2 | 225. |
| 11 | .380 | 163. | 9.0 | 225. |
| 12 | .380 | 163. | 9.0 | 225. |
| 13 | .390 | 168. | 9.0 | 225. |
| 14 | .340 | 146. | 8.5 | 254. |
| 15 | .330 | 142. | 8.3 | 255. |
| 16 | .340 | 146. | 8.3 | 255. |
| 17 | .340 | 146. | 8.3 | 255. |
| 18 | .340 | 146. | 8.3 | 255. |
| 19 | .350 | 150. | 8.3 | 255. |
| 20 | .340 | 146. | 8.4 | 255. |
| 21 | .340 | 146. | 8.4 | 256. |
| 22 | .330 | 142. | 8.4 | 255. |
| 23 | .340 | 146. | 8.4 | 255. |
| 24 | .450 | 193. | 9.5 | 175. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 10.0 | 175. |
| 2 | .410 | 176. | 10.0 | 175. |
| 3 | .410 | 176. | 10.0 | 175. |
| 4 | .400 | 172. | 10.0 | 175. |
| 5 | .410 | 176. | 10.0 | 175. |
| 6 | .420 | 180. | 9.4 | 230. |
| 7 | .400 | 172. | 8.9 | 240. |
| 8 | .380 | 163. | 8.9 | 240. |
| 9 | .390 | 168. | 8.8 | 240. |
| 10 | .390 | 168. | 8.8 | 240. |
| 11 | .380 | 163. | 8.8 | 240. |

| | | | | |
|---|---|---|---|---|
| 12 | .380 | 163. | 8.8 | 240. |
| 13 | .380 | 163. | 8.8 | 240. |
| 14 | .380 | 163. | 8.7 | 240. |
| 15 | .390 | 168. | 8.7 | 242. |
| 16 | .390 | 168. | 8.8 | 243. |
| 17 | .400 | 172. | 8.7 | 243. |
| 18 | .410 | 176. | 8.7 | 243. |
| 19 | .380 | 163. | 8.7 | 242. |
| 20 | .380 | 163. | 8.7 | 243. |
| 21 | .380 | 163. | 8.8 | 242. |
| 22 | .390 | 168. | 8.8 | 242. |
| 23 | .380 | 163. | 8.8 | 241. |
| 24 | .400 | 172. | 8.8 | 242. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 9.7 | 197. |
| 2 | .380 | 163. | 10.0 | 181. |
| 3 | .440 | 189. | 10.0 | 190. |
| 4 | .480 | 206. | 10.0 | 185. |
| 5 | .400 | 172. | 9.3 | 235. |
| 6 | .310 | 133. | 8.5 | 238. |
| 7 | .320 | 137. | 8.6 | 238. |
| 8 | .320 | 137. | 8.6 | 235. |
| 9 | .320 | 137. | 8.5 | 235. |
| 10 | .330 | 142. | 8.6 | 235. |
| 11 | .320 | 137. | 8.6 | 240. |
| 12 | .330 | 142. | 8.6 | 240. |
| 13 | .340 | 146. | 8.6 | 240. |
| 14 | .350 | 150. | 8.7 | 240. |
| 15 | .360 | 155. | 8.7 | 250. |
| 16 | .310 | 133. | 7.6 | 306. |
| 17 | .390 | 168. | 6.9 | 348. |
| 18 | .290 | 125. | 5.6 | 443. |
| 19 | .250 | 107. | 5.2 | 479. |
| 20 | .250 | 107. | 5.2 | 479. |
| 21 | .260 | 112. | 5.2 | 479. |
| 22 | .250 | 107. | 5.3 | 478. |
| 23 | .250 | 107. | 5.2 | 478. |
| 24 | .270 | 116. | 5.6 | 415. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .380 | 163. | 10.0 | 175. |
| 4 | .400 | 172. | 10.0 | 175. |
| 5 | .390 | 168. | 9.9 | 190. |
| 6 | .320 | 137. | 8.6 | 340. |
| 7 | .260 | 112. | 5.7 | 450. |
| 8 | .300 | 129. | 5.5 | 458. |
| 9 | .300 | 129. | 5.5 | 460. |
| 10 | .300 | 129. | 5.6 | 458. |

| | | | | |
|---|---|---|---|---|
| 11 | .280 | 120. | 5.6 | 458. |
| 12 | .290 | 125. | 5.6 | 458. |
| 13 | .340 | 146. | 6.3 | 378. |
| 14 | .340 | 146. | 6.6 | 352. |
| 15 | .250 | 107. | 6.3 | 380. |
| 16 | .250 | 107. | 6.3 | 380. |
| 17 | .260 | 112. | 6.3 | 380. |
| 18 | .270 | 116. | 7.0 | 300. |
| 19 | .250 | 107. | 7.4 | 300. |
| 20 | .260 | 112. | 7.4 | 300. |
| 21 | .260 | 112. | 7.4 | 300. |
| 22 | .270 | 116. | 7.4 | 300. |
| 23 | .260 | 112. | 7.4 | 300. |
| 24 | .270 | 116. | 7.6 | 250. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 9.8 | 180. |
| 2 | .460 | 198. | 10.0 | 180. |
| 3 | .450 | 193. | 10.0 | 180. |
| 4 | .450 | 193. | 10.0 | 180. |
| 5 | .460 | 198. | 10.0 | 180. |
| 6 | .450 | 193. | 9.9 | 220. |
| 7 | .240 | 103. | 6.8 | 425. |
| 8 | .240 | 103. | 5.1 | 460. |
| 9 | .360 | 155. | 6.2 | 345. |
| 10 | .290 | 125. | 6.9 | 330. |
| 11 | .300 | 129. | 6.8 | 330. |
| 12 | .300 | 129. | 6.8 | 330. |
| 13 | .310 | 133. | 6.8 | 330. |
| 14 | .350 | 150. | 6.9 | 330. |
| 15 | .360 | 155. | 7.0 | 330. |
| 16 | .370 | 159. | 7.0 | 330. |
| 17 | .340 | 146. | 6.7 | 375. |
| 18 | .300 | 129. | 5.3 | 460. |
| 19 | .290 | 125. | 5.3 | 455. |
| 20 | .290 | 125. | 5.2 | 455. |
| 21 | .310 | 133. | 5.6 | 375. |
| 22 | .270 | 116. | 6.6 | 315. |
| 23 | .370 | 159. | 8.1 | 230. |
| 24 | .520 | 223. | 9.6 | 180. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 10.0 | 180. |
| 2 | .550 | 236. | 10.0 | 180. |
| 3 | .550 | 236. | 10.0 | 180. |
| 4 | .540 | 232. | 10.0 | 180. |
| 5 | .540 | 232. | 10.0 | 180. |
| 6 | .540 | 232. | 10.0 | 180. |
| 7 | .470 | 202. | 9.0 | 222. |
| 8 | .360 | 155. | 7.1 | 328. |
| 9 | .270 | 116. | 5.7 | 432. |

| | | | | |
|---|---|---|---|---|
| 10 | .270 | 116. | 5.2 | 477. |
| 11 | .260 | 112. | 5.2 | 474. |
| 12 | .250 | 107. | 5.2 | 475. |
| 13 | .260 | 112. | 5.2 | 477. |
| 14 | .290 | 125. | 5.3 | 478. |
| 15 | .290 | 125. | 5.3 | 479. |
| 16 | .260 | 112. | 5.4 | 475. |
| 17 | .270 | 116. | 5.3 | 470. |
| 18 | .260 | 112. | 5.3 | 470. |
| 19 | .310 | 133. | 5.9 | 410. |
| 20 | .320 | 137. | 7.0 | 330. |
| 21 | .360 | 155. | 7.1 | 330. |
| 22 | .450 | 193. | 8.4 | 255. |
| 23 | .460 | 198. | 8.4 | 250. |
| 24 | .570 | 245. | 9.8 | 180. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 10.0 | 180. |
| 2 | .590 | 253. | 10.0 | 180. |
| 3 | .590 | 253. | 10.0 | 180. |
| 4 | .610 | 262. | 10.0 | 176. |
| 5 | .620 | 266. | 10.0 | 176. |
| 6 | .590 | 253. | 9.9 | 196. |
| 7 | .570 | 245. | 9.8 | 196. |
| 8 | .570 | 245. | 9.9 | 196. |
| 9 | .410 | 176. | 8.5 | 235. |
| 10 | .360 | 155. | 7.9 | 253. |
| 11 | .350 | 150. | 6.9 | 317. |
| 12 | .370 | 159. | 6.8 | 325. |
| 13 | .150 | 64. | 9.3 | 192. |
| 14 | .020 | 9. | 10.0 | 28. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .290 | 125. | 9.6 | 205. |
| 17 | .340 | 146. | 8.6 | 210. |
| 18 | .320 | 137. | 7.3 | 320. |
| 19 | .390 | 168. | 7.2 | 325. |
| 20 | .390 | 168. | 7.2 | 325. |
| 21 | .390 | 168. | 7.3 | 330. |
| 22 | .450 | 193. | 7.9 | 270. |
| 23 | .530 | 228. | 9.7 | 165. |
| 24 | .640 | 275. | 10.0 | 174. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 10.0 | 174. |
| 2 | .610 | 262. | 10.0 | 175. |
| 3 | .600 | 258. | 10.0 | 175. |
| 4 | .600 | 258. | 10.0 | 175. |
| 5 | .610 | 262. | 10.0 | 175. |
| 6 | .590 | 253. | 10.0 | 175. |
| 7 | .610 | 262. | 10.0 | 175. |
| 8 | .610 | 262. | 10.0 | 175. |

| | | | | |
|---|---|---|---|---|
| 9 | .590 | 253. | 9.9 | 178. |
| 10 | .430 | 185. | 8.7 | 226. |
| 11 | .410 | 176. | 8.5 | 227. |
| 12 | .420 | 180. | 8.6 | 226. |
| 13 | .440 | 189. | 8.7 | 226. |
| 14 | .470 | 202. | 8.9 | 221. |
| 15 | .500 | 215. | 9.2 | 214. |
| 16 | .500 | 215. | 9.3 | 210. |
| 17 | .520 | 223. | 9.3 | 210. |
| 18 | .540 | 232. | 9.3 | 210. |
| 19 | .410 | 176. | 8.1 | 275. |
| 20 | .360 | 155. | 7.6 | 275. |
| 21 | .370 | 159. | 7.7 | 275. |
| 22 | .390 | 168. | 7.9 | 260. |
| 23 | .610 | 262. | 9.8 | 175. |
| 24 | .660 | 284. | 10.0 | 175. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 10.0 | 175. |
| 2 | .630 | 271. | 10.0 | 175. |
| 3 | .620 | 266. | 10.0 | 175. |
| 4 | .620 | 266. | 10.0 | 175. |
| 5 | .600 | 258. | 10.0 | 175. |
| 6 | .580 | 249. | 10.0 | 205. |
| 7 | .370 | 159. | 6.5 | 382. |
| 8 | .360 | 155. | 4.8 | 426. |
| 9 | .340 | 146. | 5.0 | 452. |
| 10 | .320 | 137. | 4.8 | 473. |
| 11 | .320 | 137. | 4.7 | 471. |
| 12 | .320 | 137. | 5.0 | 445. |
| 13 | .340 | 146. | 5.6 | 409. |
| 14 | .350 | 150. | 5.5 | 414. |
| 15 | .400 | 172. | 6.7 | 303. |
| 16 | .350 | 150. | 6.6 | 340. |
| 17 | .360 | 155. | 6.5 | 375. |
| 18 | .330 | 142. | 5.9 | 425. |
| 19 | .290 | 125. | 5.4 | 425. |
| 20 | .320 | 137. | 5.3 | 435. |
| 21 | .340 | 146. | 5.1 | 435. |
| 22 | .360 | 155. | 5.3 | 370. |
| 23 | .380 | 163. | 7.9 | 225. |
| 24 | .450 | 193. | 9.0 | 225. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 10.0 | 175. |
| 2 | .580 | 249. | 10.0 | 175. |
| 3 | .570 | 245. | 10.0 | 175. |
| 4 | .580 | 249. | 10.0 | 175. |
| 5 | .580 | 249. | 10.0 | 175. |
| 6 | .570 | 245. | 10.0 | 185. |
| 7 | .470 | 202. | 7.5 | 312. |

| | | | | |
|---|---|---|---|---|
| 8 | .350 | 150. | 5.7 | 440. |
| 9 | .280 | 120. | 4.4 | 518. |
| 10 | .280 | 120. | 3.9 | 525. |
| 11 | .290 | 125. | 4.0 | 515. |
| 12 | .280 | 120. | 4.1 | 515. |
| 13 | .300 | 129. | 4.3 | 515. |
| 14 | .280 | 120. | 4.4 | 515. |
| 15 | .290 | 125. | 4.3 | 515. |
| 16 | .290 | 125. | 4.3 | 505. |
| 17 | .340 | 146. | 4.7 | 485. |
| 18 | .340 | 146. | 4.8 | 480. |
| 19 | .290 | 125. | 4.7 | 485. |
| 20 | .240 | 103. | 4.8 | 485. |
| 21 | .250 | 107. | 4.7 | 470. |
| 22 | .320 | 137. | 5.7 | 375. |
| 23 | .360 | 155. | 7.8 | 235. |
| 24 | .580 | 249. | 10.0 | 180. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 10.0 | 180. |
| 2 | .600 | 258. | 10.0 | 180. |
| 3 | .610 | 262. | 10.0 | 180. |
| 4 | .610 | 262. | 10.0 | 180. |
| 5 | .620 | 266. | 10.0 | 180. |
| 6 | .460 | 198. | 8.5 | 300. |
| 7 | .330 | 142. | 5.1 | 490. |
| 8 | .380 | 163. | 3.8 | 500. |
| 9 | .370 | 159. | 3.9 | 500. |
| 10 | .360 | 155. | 4.0 | 495. |
| 11 | .310 | 133. | 4.2 | 520. |
| 12 | .270 | 116. | 4.0 | 505. |
| 13 | .280 | 120. | 3.9 | 506. |
| 14 | .280 | 120. | 3.7 | 505. |
| 15 | .290 | 125. | 3.8 | 505. |
| 16 | .290 | 125. | 3.9 | 505. |
| 17 | .300 | 129. | 4.5 | 495. |
| 18 | .320 | 137. | 4.5 | 495. |
| 19 | .320 | 137. | 4.8 | 485. |
| 20 | .320 | 137. | 4.8 | 485. |
| 21 | .310 | 133. | 4.7 | 485. |
| 22 | .300 | 129. | 4.8 | 465. |
| 23 | .320 | 137. | 5.8 | 265. |
| 24 | .390 | 168. | 8.6 | 230. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 10.0 | 180. |
| 2 | .550 | 236. | 10.0 | 180. |
| 3 | .550 | 236. | 10.0 | 180. |
| 4 | .560 | 241. | 10.0 | 180. |
| 5 | .540 | 232. | 9.9 | 205. |
| 6 | .350 | 150. | 7.2 | 305. |

| | | | | |
|---|---|---|---|---|
| 7 | .270 | 116. | 5.1 | 427. |
| 8 | .270 | 116. | 5.0 | 433. |
| 9 | .280 | 120. | 5.1 | 434. |
| 10 | .260 | 112. | 4.5 | 484. |
| 11 | .250 | 107. | 4.1 | 509. |
| 12 | .230 | 99. | 4.0 | 508. |
| 13 | .240 | 103. | 4.0 | 507. |
| 14 | .260 | 112. | 4.2 | 510. |
| 15 | .250 | 107. | 4.4 | 508. |
| 16 | .260 | 112. | 4.7 | 485. |
| 17 | .260 | 112. | 4.3 | 500. |
| 18 | .270 | 116. | 4.3 | 500. |
| 19 | .270 | 116. | 4.5 | 495. |
| 20 | .280 | 120. | 4.6 | 470. |
| 21 | .300 | 129. | 5.4 | 430. |
| 22 | .320 | 137. | 5.5 | 410. |
| 23 | .320 | 137. | 6.5 | 300. |
| 24 | .420 | 180. | 7.7 | 278. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 9.2 | 180. |
| 2 | .600 | 258. | 10.0 | 180. |
| 3 | .590 | 253. | 10.0 | 180. |
| 4 | .570 | 245. | 10.0 | 180. |
| 5 | .560 | 241. | 10.0 | 180. |
| 6 | .510 | 219. | 9.0 | 225. |
| 7 | .300 | 129. | 5.9 | 392. |
| 8 | .290 | 125. | 4.0 | 500. |
| 9 | .320 | 137. | 4.0 | 500. |
| 10 | .320 | 137. | 4.2 | 500. |
| 11 | .350 | 150. | 4.4 | 490. |
| 12 | .350 | 150. | 4.5 | 485. |
| 13 | .290 | 125. | 4.5 | 495. |
| 14 | .250 | 107. | 4.3 | 490. |
| 15 | .270 | 116. | 4.3 | 490. |
| 16 | .290 | 125. | 4.3 | 500. |
| 17 | .300 | 129. | 4.3 | 500. |
| 18 | .320 | 137. | 4.4 | 500. |
| 19 | .340 | 146. | 4.8 | 485. |
| 20 | .340 | 146. | 4.8 | 485. |
| 21 | .350 | 150. | 4.8 | 485. |
| 22 | .360 | 155. | 5.1 | 440. |
| 23 | .370 | 159. | 6.4 | 330. |
| 24 | .260 | 112. | 6.9 | 319. |

DAY = 32

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 7.3 | 284. |
| 2 | .440 | 189. | 9.6 | 195. |
| 3 | .420 | 180. | 10.0 | 180. |
| 4 | .430 | 185. | 10.0 | 180. |
| 5 | .440 | 189. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 6 | .420 | 180. | 10.0 | 181. |
| 7 | .440 | 189. | 10.0 | 180. |
| 8 | .360 | 155. | 9.0 | 310. |
| 9 | .270 | 116. | 6.0 | 350. |
| 10 | .230 | 99. | 5.3 | 385. |
| 11 | .260 | 112. | 5.4 | 370. |
| 12 | .290 | 125. | 5.7 | 330. |
| 13 | .300 | 129. | 6.0 | 330. |
| 14 | .310 | 133. | 6.3 | 300. |
| 15 | .270 | 116. | 6.8 | 325. |
| 16 | .320 | 137. | 6.2 | 330. |
| 17 | .330 | 142. | 6.2 | 330. |
| 18 | .330 | 142. | 6.1 | 345. |
| 19 | .270 | 116. | 4.9 | 395. |
| 20 | .290 | 125. | 5.4 | 380. |
| 21 | .320 | 137. | 5.9 | 330. |
| 22 | .350 | 150. | 6.2 | 300. |
| 23 | .270 | 116. | 7.2 | 280. |
| 24 | .340 | 146. | 8.3 | 230. |

DAY = 33

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 10.0 | 180. |
| 2 | .320 | 137. | 7.7 | 325. |
| 3 | .300 | 129. | 5.9 | 344. |
| 4 | .290 | 125. | 5.9 | 345. |
| 5 | .290 | 125. | 5.9 | 347. |
| 6 | .290 | 125. | 5.9 | 345. |
| 7 | .310 | 133. | 5.9 | 346. |
| 8 | .280 | 120. | 5.6 | 380. |
| 9 | .260 | 112. | 4.4 | 495. |
| 10 | .230 | 99. | 3.6 | 500. |
| 11 | .240 | 103. | 3.7 | 500. |
| 12 | .260 | 112. | 3.8 | 500. |
| 13 | .260 | 112. | 3.9 | 500. |
| 14 | .250 | 107. | 3.9 | 500. |
| 15 | .260 | 112. | 4.0 | 500. |
| 16 | .270 | 116. | 4.0 | 505. |
| 17 | .260 | 112. | 4.0 | 510. |
| 18 | .250 | 107. | 4.1 | 505. |
| 19 | .260 | 112. | 3.9 | 505. |
| 20 | .260 | 112. | 3.9 | 505. |
| 21 | .260 | 112. | 3.9 | 505. |
| 22 | .260 | 112. | 3.8 | 505. |
| 23 | .280 | 120. | 3.9 | 500. |
| 24 | .350 | 150. | 6.5 | 341. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 7.7 | 265. |
| 2 | .410 | 176. | 9.2 | 204. |
| 3 | .470 | 202. | 10.0 | 180. |
| 4 | .460 | 198. | 10.0 | 180. |

| | | | | |
|---|---|---|---|---|
| 5 | .460 | 198. | 9.9 | 190. |
| 6 | .360 | 155. | 7.4 | 330. |
| 7 | .220 | 95. | 4.3 | 449. |
| 8 | .220 | 95. | 3.6 | 495. |
| 9 | .240 | 103. | 3.8 | 500. |
| 10 | .230 | 99. | 3.7 | 500. |
| 11 | .270 | 116. | 3.8 | 509. |
| 12 | .250 | 107. | 4.2 | 500. |
| 13 | .250 | 107. | 4.0 | 500. |
| 14 | .240 | 103. | 4.1 | 500. |
| 15 | .250 | 107. | 4.0 | 490. |
| 16 | .270 | 116. | 3.9 | 495. |
| 17 | .270 | 116. | 3.8 | 495. |
| 18 | .270 | 116. | 4.0 | 495. |
| 19 | .270 | 116. | 4.1 | 495. |
| 20 | .280 | 120. | 4.1 | 495. |
| 21 | .280 | 120. | 4.1 | 445. |
| 22 | .210 | 90. | 4.2 | 445. |
| 23 | .200 | 86. | 5.0 | 440. |
| 24 | .220 | 95. | 4.7 | 463. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 4.0 | 482. |
| 2 | .240 | 103. | 5.7 | 383. |
| 3 | .230 | 99. | 5.6 | 375. |
| 4 | .270 | 116. | 7.1 | 295. |
| 5 | .350 | 150. | 8.7 | 226. |
| 6 | .270 | 116. | 7.0 | 460. |
| 7 | .240 | 103. | 3.9 | 495. |
| 8 | .240 | 103. | 3.6 | 500. |
| 9 | .250 | 107. | 3.8 | 500. |
| 10 | .250 | 107. | 3.8 | 500. |
| 11 | .270 | 116. | 3.5 | 500. |
| 12 | .250 | 107. | 3.3 | 500. |
| 13 | .260 | 112. | 3.4 | 500. |
| 14 | .270 | 116. | 4.6 | 500. |
| 15 | .270 | 116. | 4.7 | 500. |
| 16 | .300 | 129. | 5.0 | 500. |
| 17 | .340 | 146. | 5.6 | 490. |
| 18 | .400 | 172. | 6.1 | 460. |
| 19 | .420 | 180. | 6.3 | 450. |
| 20 | .430 | 185. | 6.3 | 450. |
| 21 | .450 | 193. | 6.3 | 450. |
| 22 | .480 | 206. | 6.8 | 445. |
| 23 | .470 | 202. | 6.5 | 445. |
| 24 | .460 | 198. | 6.7 | 446. |

DAY = 36

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 6.6 | 446. |
| 2 | .470 | 202. | 6.6 | 434. |
| 3 | .470 | 202. | 6.6 | 446. |

| | | | | |
|---|---|---|---|---|
| 4 | .460 | 198. | 6.5 | 446. |
| 5 | .460 | 198. | 6.5 | 446. |
| 6 | .470 | 202. | 6.4 | 450. |
| 7 | .480 | 206. | 6.4 | 450. |
| 8 | .470 | 202. | 6.3 | 445. |
| 9 | .450 | 193. | 6.4 | 450. |
| 10 | .420 | 180. | 6.5 | 450. |
| 11 | .420 | 180. | 6.4 | 450. |
| 12 | .410 | 176. | 6.3 | 455. |
| 13 | .430 | 185. | 6.3 | 455. |
| 14 | .370 | 159. | 6.0 | 450. |
| 15 | .380 | 163. | 6.1 | 450. |
| 16 | .390 | 168. | 6.0 | 440. |
| 17 | .460 | 198. | 6.3 | 440. |
| 18 | .440 | 189. | 6.2 | 450. |
| 19 | .440 | 189. | 6.1 | 450. |
| 20 | .480 | 206. | 6.0 | 450. |
| 21 | .480 | 206. | 6.1 | 450. |
| 22 | .400 | 172. | 6.3 | 450. |
| 23 | .390 | 168. | 6.2 | 450. |
| 24 | .400 | 172. | 6.0 | 451. |

DAY = 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 6.9 | 404. |
| 2 | .400 | 172. | 7.1 | 400. |
| 3 | .410 | 176. | 7.1 | 400. |
| 4 | .420 | 180. | 7.1 | 400. |
| 5 | .420 | 180. | 7.1 | 402. |
| 6 | .450 | 193. | 6.3 | 450. |
| 7 | .440 | 189. | 6.2 | 455. |
| 8 | .450 | 193. | 6.2 | 450. |
| 9 | .400 | 172. | 6.1 | 450. |
| 10 | .380 | 163. | 6.0 | 450. |
| 11 | .380 | 163. | 6.0 | 450. |
| 12 | .380 | 163. | 6.1 | 450. |
| 13 | .400 | 172. | 6.1 | 450. |
| 14 | .430 | 185. | 6.1 | 450. |
| 15 | .410 | 176. | 6.0 | 450. |
| 16 | .380 | 163. | 6.0 | 450. |
| 17 | .380 | 163. | 6.0 | 450. |
| 18 | .390 | 168. | 6.0 | 450. |
| 19 | .380 | 163. | 6.2 | 450. |
| 20 | .390 | 168. | 6.2 | 450. |
| 21 | .390 | 168. | 6.1 | 450. |
| 22 | .360 | 155. | 6.2 | 450. |
| 23 | .390 | 168. | 6.2 | 450. |
| 24 | .410 | 176. | 6.1 | 452. |

DAY = 38

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 6.1 | 452. |
| 2 | .400 | 172. | 6.2 | 452. |

| | | | | |
|---|---|---|---|---|
| 3 | .340 | 146. | 6.2 | 451. |
| 4 | .340 | 146. | 6.2 | 451. |
| 5 | .360 | 155. | 6.2 | 451. |
| 6 | .370 | 159. | 6.2 | 451. |
| 7 | .370 | 159. | 6.2 | 451. |
| 8 | .380 | 163. | 6.2 | 449. |
| 9 | .390 | 168. | 6.2 | 448. |
| 10 | .380 | 163. | 6.3 | 450. |
| 11 | .360 | 155. | 6.3 | 448. |
| 12 | .360 | 155. | 6.2 | 448. |
| 13 | .360 | 155. | 6.2 | 448. |
| 14 | .340 | 146. | 6.2 | 448. |
| 15 | .350 | 150. | 6.2 | 445. |
| 16 | .370 | 159. | 6.2 | 448. |
| 17 | .380 | 163. | 6.2 | 445. |
| 18 | .370 | 159. | 6.3 | 448. |
| 19 | .370 | 159. | 6.3 | 450. |
| 20 | .400 | 172. | 6.2 | 450. |
| 21 | .420 | 180. | 6.2 | 448. |
| 22 | .390 | 168. | 6.3 | 449. |
| 23 | .380 | 163. | 6.3 | 449. |
| 24 | .410 | 176. | 6.2 | 450. |

DAY = 39

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 6.1 | 450. |
| 2 | .390 | 168. | 6.2 | 445. |
| 3 | .440 | 189. | 6.8 | 400. |
| 4 | .440 | 189. | 6.9 | 400. |
| 5 | .450 | 193. | 6.9 | 400. |
| 6 | .450 | 193. | 6.8 | 410. |
| 7 | .410 | 176. | 6.2 | 445. |
| 8 | .420 | 180. | 6.2 | 449. |
| 9 | .420 | 180. | 6.2 | 445. |
| 10 | .390 | 168. | 6.2 | 445. |
| 11 | .400 | 172. | 6.3 | 445. |
| 12 | .400 | 172. | 6.3 | 445. |
| 13 | .410 | 176. | 6.2 | 445. |
| 14 | .390 | 168. | 6.2 | 445. |
| 15 | .380 | 163. | 6.3 | 445. |
| 16 | .400 | 172. | 6.3 | 450. |
| 17 | .410 | 176. | 6.2 | 445. |
| 18 | .420 | 180. | 6.2 | 448. |
| 19 | .420 | 180. | 6.1 | 445. |
| 20 | .410 | 176. | 6.2 | 443. |
| 21 | .380 | 163. | 6.4 | 445. |
| 22 | .390 | 168. | 6.2 | 448. |
| 23 | .400 | 172. | 6.3 | 420. |
| 24 | .450 | 193. | 9.1 | 205. |

DAY = 40

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 10.1 | 180. |

| | | | | |
|---|---|---|---|---|
| 2 | .420 | 266. | 10.1 | 180. |
| 3 | .410 | 262. | 10.1 | 180. |
| 4 | .410 | 262. | 10.1 | 175. |
| 5 | .420 | 266. | 10.1 | 175. |
| 6 | .410 | 262. | 10.1 | 175. |
| 7 | .420 | 266. | 10.1 | 175. |
| 8 | .400 | 258. | 10.0 | 230. |
| 9 | .420 | 180. | 7.3 | 435. |
| 10 | .330 | 142. | 6.2 | 435. |
| 11 | .330 | 142. | 6.0 | 440. |
| 12 | .330 | 142. | 6.0 | 440. |
| 13 | .300 | 129. | 5.9 | 440. |
| 14 | .280 | 120. | 5.8 | 440. |
| 15 | .290 | 125. | 5.8 | 440. |
| 16 | .320 | 137. | 5.9 | 445. |
| 17 | .360 | 155. | 6.1 | 447. |
| 18 | .340 | 146. | 6.1 | 447. |
| 19 | .350 | 150. | 6.1 | 448. |
| 20 | .380 | 163. | 6.1 | 445. |
| 21 | .380 | 163. | 6.1 | 448. |
| 22 | .350 | 150. | 6.1 | 447. |
| 23 | .380 | 163. | 6.3 | 390. |
| 24 | .390 | 168. | 7.9 | 275. |

DAY = 41

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 8.9 | 275. |
| 2 | .420 | 180. | 9.1 | 180. |
| 3 | .530 | 228. | 10.0 | 180. |
| 4 | .540 | 232. | 10.0 | 180. |
| 5 | .540 | 232. | 10.0 | 180. |
| 6 | .450 | 193. | 9.1 | 330. |
| 7 | .350 | 150. | 6.2 | 460. |
| 8 | .380 | 163. | 5.8 | 460. |
| 9 | .380 | 163. | 5.8 | 460. |
| 10 | .370 | 159. | 6.0 | 460. |
| 11 | .380 | 163. | 6.0 | 462. |
| 12 | .380 | 163. | 5.9 | 469. |
| 13 | .380 | 163. | 5.8 | 469. |
| 14 | .360 | 155. | 5.8 | 470. |
| 15 | .360 | 155. | 5.7 | 468. |
| 16 | .340 | 146. | 5.8 | 460. |
| 17 | .320 | 137. | 5.9 | 465. |
| 18 | .350 | 150. | 5.8 | 465. |
| 19 | .370 | 159. | 5.8 | 465. |
| 20 | .370 | 159. | 5.7 | 465. |
| 21 | .380 | 163. | 5.7 | 465. |
| 22 | .380 | 163. | 5.8 | 470. |
| 23 | .340 | 146. | 5.9 | 460. |
| 24 | .380 | 163. | 6.2 | 405. |

DAY = 42

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .440 | 189. | 7.8 | 320. |
| 2 | .480 | 206. | 8.2 | 320. |
| 3 | .420 | 180. | 8.6 | 275. |
| 4 | .390 | 168. | 9.1 | 275. |
| 5 | .410 | 176. | 8.7 | 320. |
| 6 | .360 | 155. | 6.5 | 460. |
| 7 | .360 | 155. | 6.0 | 455. |
| 8 | .360 | 155. | 5.9 | 455. |
| 9 | .350 | 150. | 5.9 | 460. |
| 10 | .340 | 146. | 6.0 | 465. |
| 11 | .360 | 155. | 5.9 | 465. |
| 12 | .360 | 155. | 5.8 | 468. |
| 13 | .370 | 159. | 5.8 | 468. |
| 14 | .370 | 159. | 5.8 | 468. |
| 15 | .380 | 163. | 5.8 | 468. |
| 16 | .380 | 163. | 5.7 | 465. |
| 17 | .370 | 159. | 5.8 | 465. |
| 18 | .330 | 142. | 6.0 | 460. |
| 19 | .350 | 150. | 6.0 | 460. |
| 20 | .390 | 168. | 6.4 | 395. |
| 21 | .540 | 232. | 9.2 | 260. |
| 22 | .530 | 228. | 9.6 | 260. |
| 23 | .530 | 228. | 9.6 | 260. |
| 24 | .530 | 228. | 9.6 | 260. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 9.6 | 255. |
| 2 | .530 | 228. | 9.6 | 255. |
| 3 | .530 | 228. | 9.6 | 255. |
| 4 | .520 | 223. | 9.5 | 262. |
| 5 | .440 | 189. | 9.2 | 360. |
| 6 | .340 | 146. | 6.8 | 440. |
| 7 | .330 | 142. | 5.9 | 460. |
| 8 | .340 | 146. | 6.0 | 460. |
| 9 | .340 | 146. | 5.9 | 460. |
| 10 | .350 | 150. | 5.9 | 460. |
| 11 | .350 | 150. | 5.9 | 465. |
| 12 | .350 | 150. | 5.8 | 465. |
| 13 | .350 | 150. | 5.7 | 465. |
| 14 | .350 | 150. | 5.7 | 465. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .330 | 142. | 6.0 | 467. |
| 17 | .330 | 142. | 5.9 | 466. |
| 18 | .340 | 146. | 5.9 | 466. |
| 19 | .330 | 142. | 6.0 | 466. |
| 20 | .330 | 142. | 6.0 | 466. |
| 21 | .350 | 150. | 5.9 | 466. |
| 22 | .350 | 150. | 5.9 | 465. |
| 23 | .340 | 146. | 6.0 | 467. |
| 24 | .350 | 150. | 5.9 | 460. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .350 | 150. | 6.0 | 458. |
| 2 | .360 | 155. | 5.9 | 455. |
| 3 | .360 | 155. | 6.1 | 453. |
| 4 | .360 | 155. | 6.1 | 450. |
| 5 | .350 | 150. | 6.2 | 450. |
| 6 | .350 | 150. | 6.1 | 452. |
| 7 | .360 | 155. | 6.1 | 452. |
| 8 | .360 | 155. | 6.0 | 450. |
| 9 | .360 | 155. | 6.0 | 455. |
| 10 | .350 | 150. | 6.0 | 455. |
| 11 | .370 | 159. | 6.1 | 455. |
| 12 | .370 | 159. | 6.2 | 455. |
| 13 | .370 | 159. | 6.2 | 450. |
| 14 | .370 | 159. | 6.2 | 450. |
| 15 | .370 | 159. | 6.2 | 445. |
| 16 | .380 | 163. | 6.2 | 453. |
| 17 | .380 | 163. | 6.2 | 453. |
| 18 | .370 | 159. | 6.2 | 453. |
| 19 | .310 | 133. | 6.2 | 452. |
| 20 | .310 | 133. | 6.3 | 452. |
| 21 | .320 | 137. | 6.3 | 452. |
| 22 | .320 | 137. | 6.2 | 451. |
| 23 | .320 | 137. | 6.3 | 451. |
| 24 | .340 | 146. | 6.3 | 445. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 6.9 | 370. |
| 2 | .370 | 159. | 7.6 | 320. |
| 3 | .420 | 180. | 8.2 | 320. |
| 4 | .420 | 180. | 8.2 | 320. |
| 5 | .420 | 180. | 8.2 | 320. |
| 6 | .420 | 180. | 8.2 | 340. |
| 7 | .340 | 146. | 7.4 | 360. |
| 8 | .340 | 146. | 6.6 | 424. |
| 9 | .350 | 150. | 6.2 | 447. |
| 10 | .350 | 150. | 6.2 | 445. |
| 11 | .340 | 146. | 6.4 | 440. |
| 12 | .340 | 146. | 6.2 | 453. |
| 13 | .360 | 155. | 6.2 | 450. |
| 14 | .350 | 150. | 6.1 | 449. |
| 15 | .360 | 155. | 6.8 | 350. |
| 16 | .430 | 185. | 8.2 | 329. |
| 17 | .440 | 189. | 8.2 | 328. |
| 18 | .430 | 185. | 8.2 | 329. |
| 19 | .430 | 185. | 8.2 | 328. |
| 20 | .430 | 185. | 8.2 | 328. |
| 21 | .440 | 189. | 8.2 | 328. |
| 22 | .450 | 193. | 8.2 | 328. |
| 23 | .450 | 193. | 8.3 | 317. |
| 24 | .480 | 206. | 10.0 | 180. |

DAY = 46

| | NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.0 | 180. |
| 2 | .460 | 198. | 10.0 | 180. |
| 3 | .460 | 198. | 10.0 | 180. |
| 4 | .470 | 202. | 10.0 | 180. |
| 5 | .450 | 193. | 10.0 | 180. |
| 6 | .480 | 206. | 10.0 | 225. |
| 7 | .370 | 159. | 8.4 | 380. |
| 8 | .270 | 116. | 6.6 | 445. |
| 9 | .310 | 133. | 6.0 | 445. |
| 10 | .320 | 137. | 6.0 | 445. |
| 11 | .310 | 133. | 6.0 | 448. |
| 12 | .340 | 146. | 6.1 | 446. |
| 13 | .350 | 150. | 6.1 | 448. |
| 14 | .340 | 146. | 6.1 | 450. |
| 15 | .340 | 146. | 6.2 | 450. |
| 16 | .340 | 146. | 6.2 | 452. |
| 17 | .330 | 142. | 6.2 | 453. |
| 18 | .320 | 137. | 6.1 | 454. |
| 19 | .320 | 137. | 6.1 | 452. |
| 20 | .320 | 137. | 6.0 | 453. |
| 21 | .430 | 185. | 8.1 | 324. |
| 22 | .530 | 228. | 9.8 | 225. |
| 23 | .450 | 193. | 9.0 | 283. |
| 24 | .470 | 202. | 9.0 | 280. |

DAY = 07

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 8.9 | 280. |
| 2 | .520 | 223. | 8.9 | 280. |
| 3 | .510 | 219. | 8.9 | 280. |
| 4 | .510 | 219. | 8.9 | 280. |
| 5 | .520 | 223. | 8.9 | 280. |
| 6 | .520 | 223. | 8.9 | 280. |
| 7 | .340 | 146. | 6.8 | 440. |
| 8 | .320 | 137. | 6.1 | 450. |
| 9 | .320 | 137. | 6.1 | 450. |
| 10 | .300 | 129. | 6.1 | 450. |
| 11 | .380 | 163. | 7.0 | 375. |
| 12 | .380 | 163. | 7.9 | 326. |
| 13 | .380 | 163. | 8.0 | 328. |
| 14 | .390 | 168. | 8.2 | 275. |
| 15 | .410 | 176. | 9.1 | 278. |
| 16 | .440 | 189. | 9.1 | 278. |
| 17 | .440 | 189. | 9.1 | 277. |
| 18 | .380 | 163. | 8.3 | 320. |
| 19 | .390 | 168. | 8.1 | 328. |
| 20 | .380 | 163. | 8.1 | 325. |
| 21 | .390 | 168. | 8.1 | 328. |
| 22 | .380 | 163. | 8.1 | 328. |
| 23 | .380 | 163. | 8.1 | 328. |
| 24 | .390 | 168. | 8.7 | 270. |

DAY = 08

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 10.0 | 176. |
| 2 | .420 | 180. | 10.0 | 176. |
| 3 | .490 | 210. | 10.0 | 176. |
| 4 | .490 | 210. | 10.0 | 176. |
| 5 | .480 | 206. | 9.9 | 260. |
| 6 | .260 | 112. | 7.2 | 445. |
| 7 | .280 | 120. | 6.1 | 445. |
| 8 | .280 | 120. | 6.1 | 440. |
| 9 | .290 | 125. | 6.0 | 442. |
| 10 | .270 | 116. | 6.1 | 448. |
| 11 | .280 | 120. | 6.1 | 450. |
| 12 | .280 | 120. | 6.0 | 446. |
| 13 | .280 | 120. | 6.0 | 446. |
| 14 | .280 | 120. | 6.0 | 446. |
| 15 | .280 | 120. | 6.0 | 450. |
| 16 | .300 | 129. | 6.1 | 452. |
| 17 | .300 | 129. | 6.0 | 456. |
| 18 | .290 | 125. | 6.1 | 456. |
| 19 | .310 | 133. | 6.1 | 458. |
| 20 | .310 | 133. | 6.0 | 455. |
| 21 | .320 | 137. | 6.0 | 457. |
| 22 | .330 | 142. | 6.1 | 455. |
| 23 | .340 | 146. | 6.1 | 455. |
| 24 | .350 | 150. | 6.1 | 445. |

DAY = 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 6.0 | 455. |
| 2 | .350 | 150. | 6.0 | 455. |
| 3 | .360 | 155. | 6.0 | 455. |
| 4 | .360 | 155. | 6.0 | 455. |
| 5 | .340 | 146. | 6.1 | 455. |
| 6 | .350 | 150. | 6.1 | 455. |
| 7 | .360 | 155. | 6.1 | 450. |
| 8 | .360 | 155. | 6.1 | 450. |
| 9 | .370 | 159. | 6.1 | 450. |
| 10 | .360 | 155. | 6.2 | 450. |
| 11 | .370 | 159. | 6.3 | 455. |
| 12 | .370 | 159. | 6.2 | 450. |
| 13 | .370 | 159. | 6.2 | 450. |
| 14 | .370 | 159. | 6.2 | 450. |
| 15 | .380 | 163. | 6.2 | 450. |
| 16 | .370 | 159. | 6.2 | 452. |
| 17 | .370 | 159. | 6.3 | 454. |
| 18 | .370 | 159. | 6.3 | 454. |
| 19 | .370 | 159. | 6.3 | 454. |
| 20 | .370 | 159. | 6.3 | 454. |
| 21 | .370 | 159. | 6.3 | 454. |
| 22 | .380 | 163. | 6.2 | 452. |
| 23 | .370 | 159. | 6.2 | 452. |
| 24 | .380 | 163. | 6.3 | 453. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 6.3 | 450. |
| 2 | .370 | 159. | 6.3 | 450. |
| 3 | .370 | 159. | 6.3 | 450. |
| 4 | .380 | 163. | 6.3 | 455. |
| 5 | .380 | 163. | 6.3 | 455. |
| 6 | .390 | 168. | 6.3 | 450. |
| 7 | .380 | 163. | 6.3 | 455. |
| 8 | .390 | 168. | 6.3 | 450. |
| 9 | .390 | 168. | 6.3 | 445. |
| 10 | .370 | 159. | 6.3 | 450. |
| 11 | .370 | 159. | 6.4 | 448. |
| 12 | .370 | 159. | 6.3 | 448. |
| 13 | .360 | 155. | 6.3 | 446. |
| 14 | .350 | 150. | 6.3 | 450. |
| 15 | .380 | 163. | 6.3 | 450. |
| 16 | .410 | 176. | 6.3 | 450. |
| 17 | .410 | 176. | 6.2 | 450. |
| 18 | .400 | 172. | 6.2 | 450. |
| 19 | .400 | 172. | 6.2 | 450. |
| 20 | .410 | 176. | 6.2 | 450. |
| 21 | .420 | 180. | 6.2 | 450. |
| 22 | .420 | 180. | 6.2 | 450. |
| 23 | .430 | 185. | 6.2 | 450. |
| 24 | .430 | 185. | 6.2 | 450. |

DAY = 51



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 6.2 | 450. |
| 2 | .440 | 189. | 6.1 | 450. |
| 3 | .430 | 185. | 6.1 | 450. |
| 4 | .400 | 172. | 6.2 | 450. |
| 5 | .380 | 163. | 6.3 | 450. |
| 6 | .380 | 163. | 6.3 | 450. |
| 7 | .390 | 168. | 6.3 | 450. |
| 8 | .380 | 163. | 6.2 | 448. |
| 9 | .370 | 159. | 6.1 | 450. |
| 10 | .360 | 155. | 6.2 | 452. |
| 11 | .360 | 155. | 6.2 | 450. |
| 12 | .360 | 155. | 6.2 | 450. |
| 13 | .380 | 163. | 6.1 | 450. |
| 14 | .350 | 150. | 6.1 | 450. |
| 15 | .360 | 155. | 6.2 | 455. |
| 16 | .410 | 176. | 6.2 | 445. |
| 17 | .370 | 159. | 6.1 | 445. |
| 18 | .360 | 155. | 6.1 | 450. |
| 19 | .370 | 159. | 6.1 | 450. |
| 20 | .380 | 163. | 6.1 | 450. |
| 21 | .330 | 142. | 6.1 | 450. |
| 22 | .300 | 129. | 6.1 | 450. |
| 23 | .290 | 125. | 6.1 | 445. |
| 24 | .300 | 129. | 6.0 | 445. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 6.1 | 450. |
| 2 | .310 | 133. | 6.3 | 430. |
| 3 | .320 | 137. | 6.3 | 430. |
| 4 | .310 | 133. | 6.3 | 430. |
| 5 | .300 | 129. | 6.2 | 450. |
| 6 | .290 | 125. | 6.0 | 450. |
| 7 | .300 | 129. | 6.1 | 450. |
| 8 | .310 | 133. | 6.1 | 448. |
| 9 | .320 | 137. | 6.1 | 445. |
| 10 | .310 | 133. | 6.1 | 443. |
| 11 | .310 | 133. | 6.1 | 432. |
| 12 | .310 | 133. | 6.1 | 447. |
| 13 | .280 | 120. | 6.2 | 448. |
| 14 | .280 | 120. | 6.2 | 448. |
| 15 | .280 | 120. | 6.2 | 450. |
| 16 | .280 | 120. | 6.2 | 440. |
| 17 | .280 | 120. | 6.2 | 440. |
| 18 | .270 | 116. | 6.1 | 440. |
| 19 | .280 | 120. | 6.1 | 445. |
| 20 | .280 | 120. | 6.1 | 442. |
| 21 | .270 | 116. | 6.1 | 445. |
| 22 | .280 | 120. | 6.1 | 445. |
| 23 | .280 | 120. | 6.1 | 445. |
| 24 | .280 | 120. | 6.1 | 445. |

DAY = 53



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 6.1 | 442. |
| 2 | .280 | 120. | 6.1 | 445. |
| 3 | .290 | 125. | 6.2 | 445. |
| 4 | .290 | 125. | 6.1 | 445. |
| 5 | .290 | 125. | 6.1 | 445. |
| 6 | .290 | 125. | 6.1 | 448. |
| 7 | .290 | 125. | 6.1 | 445. |
| 8 | .290 | 125. | 6.1 | 454. |
| 9 | .310 | 133. | 6.1 | 453. |
| 10 | .310 | 133. | 6.2 | 452. |
| 11 | .310 | 133. | 6.5 | 449. |
| 12 | .310 | 133. | 6.1 | 450. |
| 13 | .310 | 133. | 6.1 | 452. |
| 14 | .310 | 133. | 6.1 | 451. |
| 15 | .310 | 133. | 6.1 | 454. |
| 16 | .300 | 129. | 6.1 | 450. |
| 17 | .290 | 125. | 6.1 | 445. |
| 18 | .290 | 125. | 6.1 | 450. |
| 19 | .300 | 129. | 6.1 | 445. |
| 20 | .310 | 133. | 6.0 | 445. |
| 21 | .290 | 125. | 6.1 | 450. |
| 22 | .290 | 125. | 6.1 | 445. |
| 23 | .300 | 129. | 6.2 | 440. |
| 24 | .350 | 150. | 8.4 | 258. |

DAY = 54

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 9.2 | 290. |
| 2 | .280 | 120. | 7.3 | 375. |
| 3 | .360 | 155. | 7.9 | 325. |
| 4 | .350 | 150. | 8.4 | 275. |
| 5 | .370 | 159. | 8.9 | 275. |
| 6 | .420 | 180. | 8.9 | 275. |
| 7 | .430 | 185. | 8.9 | 275. |
| 8 | .440 | 189. | 8.9 | 279. |
| 9 | .360 | 155. | 6.7 | 413. |
| 10 | .360 | 155. | 6.1 | 451. |
| 11 | .350 | 150. | 6.1 | 453. |
| 12 | .350 | 150. | 6.2 | 451. |
| 13 | .360 | 155. | 6.2 | 452. |
| 14 | .370 | 159. | 6.1 | 452. |
| 15 | .340 | 146. | 6.2 | 452. |
| 16 | .350 | 150. | 6.2 | 450. |
| 17 | .360 | 155. | 6.1 | 450. |
| 18 | .340 | 146. | 6.1 | 450. |
| 19 | .340 | 146. | 6.0 | 445. |
| 20 | .360 | 155. | 6.1 | 445. |
| 21 | .360 | 155. | 6.1 | 450. |
| 22 | .360 | 155. | 6.1 | 450. |
| 23 | .360 | 155. | 6.1 | 450. |
| 24 | .380 | 163. | 6.5 | 405. |

DAY = 55



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 7.7 | 305. |
| 2 | .450 | 193. | 8.8 | 275. |
| 3 | .440 | 189. | 8.9 | 275. |
| 4 | .400 | 172. | 8.2 | 355. |
| 5 | .370 | 159. | 7.4 | 355. |
| 6 | .380 | 163. | 6.5 | 450. |
| 7 | .400 | 172. | 6.2 | 450. |
| 8 | .420 | 180. | 6.2 | 452. |
| 9 | .390 | 168. | 6.1 | 453. |
| 10 | .380 | 163. | 6.2 | 453. |
| 11 | .400 | 172. | 6.2 | 458. |
| 12 | .400 | 172. | 6.2 | 453. |
| 13 | .410 | 176. | 6.2 | 453. |
| 14 | .410 | 176. | 6.2 | 453. |
| 15 | .400 | 172. | 6.2 | 450. |
| 16 | .400 | 172. | 6.2 | 450. |
| 17 | .400 | 172. | 6.1 | 450. |
| 18 | .380 | 163. | 6.2 | 450. |
| 19 | .380 | 163. | 6.2 | 450. |
| 20 | .390 | 168. | 6.2 | 450. |
| 21 | .380 | 163. | 6.2 | 450. |
| 22 | .390 | 168. | 6.2 | 450. |
| 23 | .390 | 168. | 6.2 | 450. |
| 24 | .380 | 163. | 6.2 | 450. |

DAY = 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 6.2 | 445. |
| 2 | .370 | 159. | 6.2 | 450. |
| 3 | .370 | 159. | 6.2 | 448. |
| 4 | .380 | 163. | 6.1 | 448. |
| 5 | .380 | 163. | 6.2 | 450. |
| 6 | .380 | 163. | 6.2 | 455. |
| 7 | .380 | 163. | 6.1 | 450. |
| 8 | .400 | 172. | 6.1 | 448. |
| 9 | .420 | 180. | 6.1 | 448. |
| 10 | .440 | 189. | 6.1 | 448. |
| 11 | .410 | 176. | 6.1 | 450. |
| 12 | .380 | 163. | 6.1 | 450. |
| 13 | .380 | 163. | 6.1 | 450. |
| 14 | .370 | 159. | 6.1 | 450. |
| 15 | .380 | 163. | 6.1 | 450. |
| 16 | .360 | 155. | 6.1 | 450. |
| 17 | .330 | 142. | 6.3 | 445. |
| 18 | .330 | 142. | 6.2 | 445. |
| 19 | .340 | 146. | 6.2 | 445. |
| 20 | .340 | 146. | 6.2 | 400. |
| 21 | .400 | 172. | 6.9 | 410. |
| 22 | .390 | 168. | 6.8 | 405. |
| 23 | .390 | 168. | 6.8 | 410. |
| 24 | .390 | 168. | 6.9 | 405. |

DAY = 57



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 6.9 | 405. |
| 2 | .400 | 172. | 6.8 | 405. |
| 3 | .390 | 168. | 6.8 | 425. |
| 4 | .350 | 150. | 6.2 | 442. |
| 5 | .350 | 150. | 6.2 | 445. |
| 6 | .370 | 159. | 6.2 | 448. |
| 7 | .400 | 172. | 6.2 | 448. |
| 8 | .380 | 163. | 6.2 | 450. |
| 9 | .360 | 155. | 6.1 | 449. |
| 10 | .360 | 155. | 6.1 | 448. |
| 11 | .380 | 163. | 6.2 | 448. |
| 12 | .440 | 189. | 6.4 | 451. |
| 13 | .450 | 193. | 6.3 | 452. |
| 14 | .500 | 215. | 6.2 | 448. |
| 15 | .470 | 202. | 6.2 | 438. |
| 16 | .410 | 176. | 6.2 | 450. |
| 17 | .440 | 189. | 6.2 | 450. |
| 18 | .430 | 185. | 6.1 | 450. |
| 19 | .440 | 189. | 6.3 | 450. |
| 20 | .440 | 189. | 6.3 | 450. |
| 21 | .450 | 193. | 6.2 | 450. |
| 22 | .450 | 193. | 6.2 | 450. |
| 23 | .450 | 193. | 6.2 | 450. |
| 24 | .440 | 189. | 6.4 | 428. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 7.8 | 300. |
| 2 | .490 | 210. | 9.7 | 228. |
| 3 | .530 | 228. | 10.0 | 228. |
| 4 | .520 | 223. | 9.9 | 230. |
| 5 | .430 | 185. | 8.6 | 310. |
| 6 | .330 | 142. | 6.4 | 450. |
| 7 | .310 | 133. | 6.0 | 445. |
| 8 | .320 | 137. | 6.1 | 451. |
| 9 | .330 | 142. | 6.5 | 426. |
| 10 | .300 | 129. | 7.1 | 380. |
| 11 | .290 | 125. | 7.1 | 381. |
| 12 | .290 | 125. | 7.0 | 368. |
| 13 | .290 | 125. | 7.0 | 381. |
| 14 | .280 | 120. | 7.0 | 380. |
| 15 | .280 | 120. | 7.1 | 381. |
| 16 | .280 | 120. | 7.1 | 380. |
| 17 | .290 | 125. | 7.1 | 370. |
| 18 | .300 | 129. | 7.2 | 370. |
| 19 | .310 | 133. | 7.2 | 370. |
| 20 | .300 | 129. | 7.2 | 370. |
| 21 | .300 | 129. | 7.2 | 370. |
| 22 | .310 | 133. | 7.1 | 430. |
| 23 | .260 | 112. | 6.3 | 445. |
| 24 | .270 | 116. | 6.2 | 445. |

DAY = 59



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 6.2 | 442. |
| 2 | .340 | 146. | 6.8 | 355. |
| 3 | .440 | 189. | 7.5 | 340. |
| 4 | .450 | 193. | 7.5 | 340. |
| 5 | .390 | 168. | 6.9 | 440. |
| 6 | .300 | 129. | 6.2 | 442. |
| 7 | .360 | 155. | 6.8 | 378. |
| 8 | .370 | 159. | 6.9 | 380. |
| 9 | .380 | 163. | 7.2 | 352. |
| 10 | .320 | 137. | 7.5 | 340. |
| 11 | .380 | 163. | 7.8 | 340. |
| 12 | .380 | 163. | 7.8 | 340. |
| 13 | .370 | 159. | 6.8 | 450. |
| 14 | .430 | 185. | 6.2 | 450. |
| 15 | .430 | 185. | 6.2 | 450. |
| 16 | .440 | 189. | 6.2 | 455. |
| 17 | .450 | 193. | 6.2 | 455. |
| 18 | .440 | 189. | 6.2 | 455. |
| 19 | .380 | 163. | 6.3 | 405. |
| 20 | .280 | 120. | 8.2 | 350. |
| 21 | .300 | 129. | 10.0 | 105. |
| 22 | .170 | 73. | 10.0 | 110. |
| 23 | .110 | 47. | 10.0 | 90. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 72

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .170 | 73. | 9.2 | 105. |
| 4 | .260 | 112. | 7.3 | 140. |
| 5 | .360 | 155. | 11.5 | 140. |
| 6 | .400 | 172. | 12.3 | 140. |
| 7 | .400 | 172. | 12.3 | 140. |
| 8 | .420 | 180. | 12.3 | 140. |
| 9 | .310 | 133. | 10.0 | 140. |
| 10 | .300 | 129. | 10.0 | 140. |
| 11 | .310 | 133. | 10.0 | 140. |
| 12 | .290 | 125. | 10.0 | 140. |
| 13 | .270 | 116. | 10.0 | 140. |
| 14 | .270 | 116. | 10.0 | 140. |
| 15 | .260 | 112. | 10.0 | 140. |
| 16 | .260 | 112. | 10.0 | 140. |
| 17 | .250 | 107. | 10.0 | 140. |
| 18 | .250 | 107. | 10.0 | 140. |
| 19 | .240 | 103. | 10.0 | 140. |
| 20 | .250 | 107. | 10.0 | 140. |
| 21 | .260 | 112. | 10.0 | 140. |
| 22 | .240 | 103. | 10.0 | 140. |
| 23 | .230 | 99. | 10.0 | 140. |
| 24 | .240 | 103. | 10.0 | 135. |

DAY = 73



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 10.0 | 135. |
| 2 | .240 | 103. | 10.0 | 135. |
| 3 | .250 | 107. | 10.0 | 135. |
| 4 | .250 | 107. | 10.0 | 135. |
| 5 | .240 | 103. | 10.0 | 135. |
| 6 | .240 | 103. | 10.0 | 135. |
| 7 | .230 | 99. | 10.0 | 135. |
| 8 | .240 | 103. | 10.0 | 134. |
| 9 | .240 | 103. | 10.0 | 134. |
| 10 | .260 | 112. | 10.0 | 134. |
| 11 | .420 | 180. | 10.0 | 135. |
| 12 | .310 | 133. | 10.0 | 134. |
| 13 | .290 | 125. | 10.0 | 134. |
| 14 | .260 | 112. | 10.0 | 134. |
| 15 | .280 | 120. | 10.0 | 136. |
| 16 | .290 | 125. | 10.0 | 134. |
| 17 | .290 | 125. | 10.0 | 136. |
| 18 | .290 | 125. | 10.0 | 134. |
| 19 | .290 | 125. | 10.0 | 134. |
| 20 | .290 | 125. | 10.0 | 134. |
| 21 | .290 | 125. | 10.0 | 134. |
| 22 | .280 | 120. | 10.0 | 134. |
| 23 | .280 | 120. | 10.0 | 134. |
| 24 | .300 | 129. | 10.0 | 134. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 10.0 | 135. |
| 2 | .300 | 129. | 10.0 | 135. |
| 3 | .300 | 129. | 10.0 | 135. |
| 4 | .310 | 133. | 10.0 | 135. |
| 5 | .300 | 129. | 10.0 | 135. |
| 6 | .330 | 142. | 10.0 | 135. |
| 7 | .320 | 137. | 10.0 | 135. |
| 8 | .310 | 133. | 10.0 | 135. |
| 9 | .310 | 133. | 10.0 | 134. |
| 10 | .310 | 133. | 10.0 | 134. |
| 11 | .300 | 129. | 10.0 | 134. |
| 12 | .280 | 120. | 10.0 | 134. |
| 13 | .290 | 125. | 10.0 | 134. |
| 14 | .260 | 112. | 10.0 | 134. |
| 15 | .260 | 112. | 10.0 | 134. |
| 16 | .250 | 107. | 10.0 | 134. |
| 17 | .240 | 103. | 10.0 | 134. |
| 18 | .240 | 103. | 10.0 | 134. |
| 19 | .250 | 107. | 10.0 | 134. |
| 20 | .260 | 112. | 10.0 | 134. |
| 21 | .270 | 116. | 10.0 | 135. |
| 22 | .280 | 120. | 10.0 | 135. |
| 23 | .280 | 120. | 10.0 | 135. |
| 24 | .280 | 120. | 10.0 | 135. |

DAY = 75



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 10.0 | 135. |
| 2 | .290 | 125. | 10.0 | 135. |
| 3 | .290 | 125. | 10.0 | 135. |
| 4 | .290 | 125. | 10.0 | 135. |
| 5 | .300 | 129. | 10.0 | 135. |
| 6 | .300 | 129. | 10.0 | 135. |
| 7 | .300 | 129. | 10.0 | 135. |
| 8 | .300 | 129. | 10.0 | 136. |
| 9 | .300 | 129. | 10.0 | 136. |
| 10 | .310 | 133. | 10.0 | 136. |
| 11 | .300 | 129. | 10.0 | 136. |
| 12 | .300 | 129. | 10.0 | 135. |
| 13 | .290 | 125. | 10.0 | 134. |
| 14 | .280 | 120. | 10.0 | 134. |
| 15 | .280 | 120. | 10.0 | 134. |
| 16 | .260 | 112. | 10.0 | 134. |
| 17 | .260 | 112. | 10.0 | 134. |
| 18 | .270 | 116. | 10.0 | 134. |
| 19 | .260 | 112. | 10.0 | 134. |
| 20 | .250 | 107. | 10.0 | 134. |
| 21 | .270 | 116. | 10.0 | 136. |
| 22 | .270 | 116. | 10.0 | 136. |
| 23 | .270 | 116. | 10.0 | 136. |
| 24 | .270 | 116. | 10.0 | 135. |

DAY = 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 10.0 | 135. |
| 2 | .280 | 120. | 10.0 | 135. |
| 3 | .280 | 120. | 10.0 | 135. |
| 4 | .280 | 120. | 10.0 | 135. |
| 5 | .290 | 125. | 10.0 | 135. |
| 6 | .290 | 125. | 10.0 | 135. |
| 7 | .300 | 129. | 10.0 | 135. |
| 8 | .300 | 129. | 10.0 | 136. |
| 9 | .310 | 133. | 10.0 | 136. |
| 10 | .320 | 137. | 10.0 | 136. |
| 11 | .310 | 133. | 10.0 | 136. |
| 12 | .310 | 133. | 10.0 | 136. |
| 13 | .310 | 133. | 10.0 | 136. |
| 14 | .300 | 129. | 10.0 | 136. |
| 15 | .290 | 125. | 10.0 | 135. |
| 16 | .280 | 120. | 10.0 | 135. |
| 17 | .380 | 163. | 10.0 | 162. |
| 18 | .440 | 189. | 8.2 | 305. |
| 19 | .340 | 146. | 6.2 | 435. |
| 20 | .350 | 150. | 6.1 | 432. |
| 21 | .380 | 163. | 6.2 | 430. |
| 22 | .400 | 172. | 6.2 | 438. |
| 23 | .480 | 206. | 7.3 | 305. |
| 24 | .620 | 266. | 9.6 | 230. |

DAY = 77



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .670 | 288. | 9.8 | 230. |
| 2 | .690 | 296. | 9.8 | 230. |
| 3 | .690 | 296. | 9.8 | 230. |
| 4 | .690 | 296. | 9.8 | 230. |
| 5 | .680 | 292. | 9.8 | 230. |
| 6 | .500 | 215. | 8.5 | 350. |
| 7 | .340 | 146. | 6.1 | 475. |
| 8 | .350 | 150. | 5.7 | 465. |
| 9 | .360 | 155. | 5.7 | 465. |
| 10 | .360 | 155. | 5.7 | 469. |
| 11 | .370 | 159. | 5.7 | 465. |
| 12 | .360 | 155. | 5.7 | 465. |
| 13 | .370 | 159. | 5.7 | 465. |
| 14 | .350 | 150. | 5.6 | 465. |
| 15 | .360 | 155. | 5.9 | 455. |
| 16 | .370 | 159. | 5.9 | 446. |
| 17 | .370 | 159. | 6.0 | 446. |
| 18 | .320 | 137. | 6.1 | 446. |
| 19 | .270 | 116. | 6.1 | 446. |
| 20 | .270 | 116. | 6.0 | 440. |
| 21 | .280 | 120. | 6.0 | 440. |
| 22 | .290 | 125. | 6.0 | 440. |
| 23 | .280 | 120. | 6.1 | 440. |
| 24 | .300 | 129. | 6.3 | 430. |

DAY = 78

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 8.5 | 230. |
| 2 | .650 | 279. | 10.0 | 230. |
| 3 | .650 | 279. | 10.0 | 230. |
| 4 | .660 | 284. | 10.0 | 230. |
| 5 | .650 | 279. | 10.0 | 230. |
| 6 | .330 | 142. | 8.1 | 350. |
| 7 | .420 | 180. | 7.5 | 360. |
| 8 | .310 | 133. | 6.6 | 450. |
| 9 | .360 | 155. | 6.1 | 450. |
| 10 | .440 | 189. | 6.1 | 450. |
| 11 | .450 | 193. | 6.4 | 428. |
| 12 | .510 | 219. | 6.9 | 350. |
| 13 | .500 | 215. | 7.9 | 328. |
| 14 | .700 | 301. | 9.0 | 278. |
| 15 | .690 | 296. | 10.0 | 178. |
| 16 | .660 | 284. | 10.0 | 175. |
| 17 | .680 | 292. | 10.0 | 175. |
| 18 | .670 | 288. | 10.0 | 175. |
| 19 | .670 | 288. | 10.0 | 175. |
| 20 | .670 | 288. | 10.0 | 175. |
| 21 | .660 | 284. | 10.0 | 175. |
| 22 | .680 | 292. | 10.0 | 175. |
| 23 | .670 | 288. | 10.0 | 175. |
| 24 | .670 | 288. | 10.0 | 175. |

DAY = 79



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .670 | 288. | 10.0 | 175. |
| 2 | .670 | 288. | 10.0 | 175. |
| 3 | .670 | 288. | 10.0 | 175. |
| 4 | .670 | 288. | 10.0 | 175. |
| 5 | .660 | 284. | 10.0 | 175. |
| 6 | .650 | 279. | 10.0 | 175. |
| 7 | .640 | 275. | 10.0 | 175. |
| 8 | .630 | 271. | 10.0 | 175. |
| 9 | .620 | 266. | 10.0 | 175. |
| 10 | .590 | 253. | 10.0 | 175. |
| 11 | .610 | 262. | 10.0 | 175. |
| 12 | .650 | 279. | 9.7 | 225. |
| 13 | .690 | 296. | 9.7 | 225. |
| 14 | .670 | 288. | 10.0 | 180. |
| 15 | .610 | 262. | 10.0 | 180. |
| 16 | .630 | 271. | 10.0 | 180. |
| 17 | .640 | 275. | 10.0 | 180. |
| 18 | .630 | 271. | 10.0 | 180. |
| 19 | .630 | 271. | 10.0 | 180. |
| 20 | .640 | 275. | 10.0 | 180. |
| 21 | .630 | 271. | 10.0 | 180. |
| 22 | .620 | 266. | 10.0 | 180. |
| 23 | .590 | 253. | 10.0 | 180. |
| 24 | .610 | 262. | 10.0 | 180. |

DAY = 80

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 10.0 | 180. |
| 2 | .630 | 271. | 10.0 | 180. |
| 3 | .620 | 266. | 10.0 | 180. |
| 4 | .620 | 266. | 10.0 | 180. |
| 5 | .610 | 262. | 10.0 | 180. |
| 6 | .670 | 288. | 9.6 | 300. |
| 7 | .510 | 219. | 7.6 | 375. |
| 8 | .420 | 180. | 6.0 | 460. |
| 9 | .430 | 185. | 5.8 | 460. |
| 10 | .420 | 180. | 5.7 | 460. |
| 11 | .450 | 193. | 5.8 | 460. |
| 12 | .460 | 198. | 5.8 | 463. |
| 13 | .490 | 210. | 6.0 | 463. |
| 14 | .590 | 253. | 7.4 | 356. |
| 15 | .570 | 245. | 9.0 | 265. |
| 16 | .590 | 253. | 9.1 | 265. |
| 17 | .620 | 266. | 9.2 | 265. |
| 18 | .620 | 266. | 9.1 | 265. |
| 19 | .640 | 275. | 9.1 | 265. |
| 20 | .650 | 279. | 9.1 | 265. |
| 21 | .650 | 279. | 9.1 | 265. |
| 22 | .650 | 279. | 9.1 | 265. |
| 23 | .660 | 284. | 9.2 | 265. |
| 24 | .640 | 275. | 9.0 | 285. |

DAY = A1



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 8.2 | 305. |
| 2 | .620 | 266. | 8.2 | 305. |
| 3 | .620 | 266. | 8.2 | 305. |
| 4 | .610 | 262. | 8.2 | 305. |
| 5 | .610 | 262. | 8.2 | 305. |
| 6 | .620 | 266. | 8.2 | 305. |
| 7 | .640 | 275. | 8.2 | 305. |
| 8 | .640 | 275. | 8.2 | 305. |
| 9 | .530 | 228. | 7.6 | 340. |
| 10 | .430 | 185. | 7.3 | 358. |
| 11 | .460 | 198. | 7.3 | 358. |
| 12 | .470 | 202. | 7.3 | 358. |
| 13 | .480 | 206. | 7.3 | 358. |
| 14 | .520 | 223. | 7.8 | 322. |
| 15 | .460 | 198. | 8.8 | 226. |
| 16 | .500 | 215. | 8.9 | 265. |
| 17 | .510 | 219. | 8.9 | 265. |
| 18 | .510 | 219. | 8.9 | 290. |
| 19 | .480 | 206. | 7.9 | 320. |
| 20 | .560 | 241. | 7.9 | 320. |
| 21 | .590 | 253. | 8.0 | 320. |
| 22 | .590 | 253. | 8.0 | 320. |
| 23 | .580 | 249. | 8.0 | 320. |
| 24 | .570 | 245. | 7.9 | 320. |

DAY = A2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 8.0 | 320. |
| 2 | .740 | 318. | 9.0 | 270. |
| 3 | .760 | 326. | 9.1 | 270. |
| 4 | .760 | 326. | 9.1 | 270. |
| 5 | .770 | 331. | 9.1 | 270. |
| 6 | .590 | 253. | 8.1 | 320. |
| 7 | .590 | 253. | 8.0 | 320. |
| 8 | .590 | 253. | 8.1 | 320. |
| 9 | .480 | 206. | 7.5 | 340. |
| 10 | .420 | 180. | 7.3 | 370. |
| 11 | .510 | 219. | 7.8 | 338. |
| 12 | .560 | 241. | 8.1 | 324. |
| 13 | .590 | 253. | 8.0 | 324. |
| 14 | .590 | 253. | 8.1 | 324. |
| 15 | .590 | 253. | 8.1 | 324. |
| 16 | .580 | 249. | 8.2 | 325. |
| 17 | .590 | 253. | 8.1 | 325. |
| 18 | .570 | 245. | 7.9 | 350. |
| 19 | .430 | 185. | 7.1 | 400. |
| 20 | .390 | 168. | 6.8 | 400. |
| 21 | .400 | 172. | 6.9 | 400. |
| 22 | .400 | 172. | 6.9 | 400. |
| 23 | .410 | 176. | 6.9 | 400. |
| 24 | .420 | 180. | 6.8 | 400. |

DAY = A3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 6.9 | 400. |
| 2 | .420 | 180. | 6.9 | 400. |
| 3 | .420 | 180. | 6.9 | 400. |
| 4 | .440 | 189. | 6.9 | 400. |
| 5 | .430 | 185. | 6.9 | 400. |
| 6 | .500 | 215. | 7.4 | 320. |
| 7 | .630 | 271. | 8.1 | 345. |
| 8 | .440 | 189. | 6.9 | 402. |
| 9 | .410 | 176. | 6.6 | 430. |
| 10 | .380 | 163. | 6.4 | 430. |
| 11 | .370 | 159. | 6.5 | 430. |
| 12 | .360 | 155. | 6.5 | 426. |
| 13 | .380 | 163. | 6.4 | 426. |
| 14 | .520 | 223. | 6.4 | 426. |
| 15 | .520 | 223. | 6.4 | 426. |
| 16 | .510 | 219. | 6.4 | 430. |
| 17 | .510 | 219. | 6.2 | 425. |
| 18 | .520 | 223. | 6.1 | 455. |
| 19 | .530 | 228. | 6.3 | 425. |
| 20 | .530 | 228. | 6.5 | 420. |
| 21 | .610 | 262. | 7.3 | 370. |
| 22 | .630 | 271. | 7.3 | 370. |
| 23 | .560 | 241. | 6.7 | 420. |
| 24 | .600 | 258. | 7.0 | 350. |

DAY = A4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .690 | 296. | 8.2 | 315. |
| 2 | .700 | 301. | 8.3 | 315. |
| 3 | .730 | 314. | 9.0 | 260. |
| 4 | .700 | 301. | 9.7 | 245. |
| 5 | .720 | 309. | 9.7 | 245. |
| 6 | .570 | 245. | 8.6 | 305. |
| 7 | .550 | 236. | 8.4 | 305. |
| 8 | .530 | 228. | 7.3 | 368. |
| 9 | .570 | 245. | 7.6 | 332. |
| 10 | .540 | 232. | 7.8 | 335. |
| 11 | .590 | 253. | 8.3 | 285. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .620 | 266. | 9.2 | 255. |
| 14 | .600 | 258. | 9.2 | 255. |
| 15 | .630 | 271. | 9.2 | 255. |
| 16 | .640 | 275. | 9.2 | 260. |
| 17 | .640 | 275. | 9.3 | 260. |
| 18 | .630 | 271. | 9.2 | 260. |
| 19 | .580 | 249. | 8.5 | 280. |
| 20 | .600 | 258. | 8.9 | 275. |
| 21 | .610 | 262. | 9.0 | 275. |
| 22 | .580 | 249. | 8.5 | 300. |
| 23 | .630 | 271. | 8.1 | 325. |
| 24 | .690 | 296. | 8.6 | 275. |

DAY = 85



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 9.0 | 275. |
| 2 | .660 | 284. | 9.1 | 275. |
| 3 | .650 | 279. | 9.1 | 275. |
| 4 | .640 | 275. | 9.1 | 275. |
| 5 | .640 | 275. | 9.0 | 275. |
| 6 | .670 | 288. | 8.2 | 325. |
| 7 | .640 | 275. | 7.8 | 375. |
| 8 | .550 | 236. | 7.3 | 365. |
| 9 | .570 | 245. | 8.0 | 322. |
| 10 | .480 | 206. | 8.5 | 274. |
| 11 | .570 | 245. | 8.8 | 274. |
| 12 | .590 | 253. | 8.9 | 274. |
| 13 | .600 | 258. | 8.9 | 274. |
| 14 | .570 | 245. | 8.9 | 276. |
| 15 | .580 | 249. | 8.9 | 275. |
| 16 | .570 | 245. | 8.9 | 280. |
| 17 | .600 | 258. | 8.9 | 280. |
| 18 | .610 | 262. | 8.7 | 330. |
| 19 | .600 | 258. | 7.9 | 330. |
| 20 | .600 | 258. | 7.8 | 330. |
| 21 | .600 | 258. | 7.8 | 330. |
| 22 | .580 | 249. | 7.8 | 330. |
| 23 | .570 | 245. | 7.9 | 330. |
| 24 | .590 | 253. | 7.9 | 325. |

DAY = 86

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 7.8 | 325. |
| 2 | .590 | 253. | 7.8 | 325. |
| 3 | .580 | 249. | 7.8 | 325. |
| 4 | .580 | 249. | 7.8 | 325. |
| 5 | .600 | 258. | 7.8 | 325. |
| 6 | .630 | 271. | 7.8 | 325. |
| 7 | .680 | 292. | 8.5 | 275. |
| 8 | .600 | 258. | 7.8 | 332. |
| 9 | .530 | 228. | 7.1 | 370. |
| 10 | .550 | 236. | 7.4 | 350. |
| 11 | .610 | 262. | 7.9 | 326. |
| 12 | .590 | 253. | 8.1 | 324. |
| 13 | .650 | 279. | 9.5 | 236. |
| 14 | .560 | 241. | 8.7 | 274. |
| 15 | .560 | 241. | 8.8 | 274. |
| 16 | .550 | 236. | 8.8 | 275. |
| 17 | .570 | 245. | 8.8 | 275. |
| 18 | .580 | 249. | 8.7 | 330. |
| 19 | .580 | 249. | 7.7 | 330. |
| 20 | .590 | 253. | 7.7 | 330. |
| 21 | .610 | 262. | 7.7 | 330. |
| 22 | .650 | 279. | 7.8 | 330. |
| 23 | .640 | 275. | 7.8 | 330. |
| 24 | .620 | 266. | 7.8 | 325. |

DAY = 87



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 7.8 | 325. |
| 2 | .620 | 266. | 7.8 | 325. |
| 3 | .620 | 266. | 7.8 | 325. |
| 4 | .620 | 266. | 7.8 | 325. |
| 5 | .630 | 271. | 7.8 | 325. |
| 6 | .610 | 262. | 7.8 | 325. |
| 7 | .620 | 266. | 7.8 | 325. |
| 8 | .620 | 266. | 6.7 | 400. |
| 9 | .620 | 266. | 6.6 | 405. |
| 10 | .630 | 271. | 6.6 | 395. |
| 11 | .620 | 266. | 6.9 | 360. |
| 12 | .520 | 223. | 7.2 | 350. |
| 13 | .560 | 241. | 7.4 | 330. |
| 14 | .570 | 245. | 7.6 | 330. |
| 15 | .580 | 249. | 7.7 | 330. |
| 16 | .580 | 249. | 7.7 | 330. |
| 17 | .610 | 262. | 7.8 | 330. |
| 18 | .590 | 253. | 7.6 | 360. |
| 19 | .500 | 215. | 7.0 | 380. |
| 20 | .510 | 219. | 6.9 | 380. |
| 21 | .510 | 219. | 7.0 | 380. |
| 22 | .520 | 223. | 7.0 | 380. |
| 23 | .540 | 232. | 6.9 | 380. |
| 24 | .540 | 232. | 6.9 | 380. |

DAY = 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 6.9 | 372. |
| 2 | .530 | 228. | 7.0 | 372. |
| 3 | .510 | 219. | 7.0 | 372. |
| 4 | .520 | 223. | 7.0 | 372. |
| 5 | .540 | 232. | 7.0 | 374. |
| 6 | .540 | 232. | 7.0 | 374. |
| 7 | .550 | 236. | 7.0 | 374. |
| 8 | .550 | 236. | 7.0 | 374. |
| 9 | .560 | 241. | 7.0 | 374. |
| 10 | .560 | 241. | 6.3 | 430. |
| 11 | .550 | 236. | 6.4 | 430. |
| 12 | .550 | 236. | 6.6 | 410. |
| 13 | .570 | 245. | 6.7 | 410. |
| 14 | .620 | 266. | 6.7 | 410. |
| 15 | .620 | 266. | 6.8 | 410. |
| 16 | .630 | 271. | 6.8 | 410. |
| 17 | .640 | 275. | 6.7 | 410. |
| 18 | .640 | 275. | 6.7 | 410. |
| 19 | .680 | 292. | 8.0 | 280. |
| 20 | .790 | 339. | 9.1 | 280. |
| 21 | .790 | 339. | 9.1 | 280. |
| 22 | .790 | 339. | 9.1 | 280. |
| 23 | .800 | 344. | 9.1 | 280. |
| 24 | .820 | 352. | 9.1 | 280. |

DAY = 89



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .730 | 314. | 9.0 | 272. |
| 2 | .690 | 296. | 9.1 | 272. |
| 3 | .690 | 296. | 9.1 | 272. |
| 4 | .690 | 296. | 9.0 | 272. |
| 5 | .700 | 301. | 9.1 | 274. |
| 6 | .690 | 296. | 9.0 | 279. |
| 7 | .680 | 292. | 9.0 | 272. |
| 8 | .650 | 279. | 8.3 | 325. |
| 9 | .670 | 288. | 8.0 | 325. |
| 10 | .660 | 284. | 8.7 | 280. |
| 11 | .680 | 292. | 9.0 | 280. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .250 | 107. | 10.0 | 230. |
| 17 | .760 | 326. | 9.7 | 240. |
| 18 | .730 | 314. | 9.4 | 310. |
| 19 | .520 | 223. | 7.4 | 400. |
| 20 | .450 | 193. | 6.7 | 400. |
| 21 | .530 | 228. | 7.3 | 330. |
| 22 | .590 | 253. | 7.7 | 330. |
| 23 | .600 | 258. | 7.7 | 330. |
| 24 | .590 | 253. | 7.8 | 330. |

DAY = 90

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.8 | 330. |
| 2 | .610 | 262. | 7.8 | 330. |
| 3 | .640 | 275. | 7.9 | 330. |
| 4 | .620 | 266. | 7.9 | 330. |
| 5 | .630 | 271. | 7.9 | 330. |
| 6 | .630 | 271. | 7.9 | 330. |
| 7 | .600 | 258. | 7.7 | 332. |
| 8 | .500 | 215. | 6.3 | 450. |
| 9 | .530 | 228. | 6.2 | 450. |
| 10 | .530 | 228. | 6.1 | 450. |
| 11 | .520 | 223. | 6.1 | 450. |
| 12 | .500 | 215. | 6.3 | 450. |
| 13 | .520 | 223. | 6.3 | 450. |
| 14 | .530 | 228. | 6.2 | 450. |
| 15 | .520 | 223. | 6.2 | 450. |
| 16 | .510 | 219. | 6.2 | 450. |
| 17 | .510 | 219. | 6.2 | 455. |
| 18 | .490 | 210. | 6.0 | 465. |
| 19 | .490 | 210. | 5.8 | 465. |
| 20 | .480 | 206. | 5.8 | 465. |
| 21 | .500 | 215. | 5.8 | 465. |
| 22 | .510 | 219. | 6.0 | 465. |
| 23 | .510 | 219. | 5.9 | 460. |
| 24 | .540 | 232. | 6.1 | 460. |

DAY = 91

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 6.3 | 442. |
| 2 | .510 | 219. | 6.3 | 442. |
| 3 | .530 | 228. | 6.2 | 442. |
| 4 | .550 | 236. | 6.2 | 442. |
| 5 | .560 | 241. | 6.3 | 442. |
| 6 | .530 | 228. | 6.3 | 442. |
| 7 | .530 | 228. | 6.3 | 442. |
| 8 | .530 | 228. | 6.3 | 450. |
| 9 | .520 | 223. | 6.3 | 450. |
| 10 | .550 | 236. | 6.2 | 450. |
| 11 | .580 | 249. | 6.2 | 450. |
| 12 | .550 | 236. | 6.2 | 450. |
| 13 | .500 | 215. | 6.3 | 450. |
| 14 | .570 | 245. | 6.9 | 365. |
| 15 | .600 | 258. | 8.0 | 335. |
| 16 | .570 | 245. | 7.8 | 395. |
| 17 | .510 | 219. | 6.2 | 454. |
| 18 | .500 | 215. | 6.1 | 450. |
| 19 | .530 | 228. | 6.3 | 400. |
| 20 | .440 | 189. | 7.4 | 370. |
| 21 | .500 | 215. | 7.5 | 370. |
| 22 | .510 | 219. | 7.5 | 370. |
| 23 | .540 | 232. | 7.7 | 310. |
| 24 | .630 | 271. | 9.9 | 212. |

DAY = 92

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 10.0 | 200. |
| 2 | .670 | 288. | 10.0 | 178. |
| 3 | .650 | 279. | 10.0 | 176. |
| 4 | .640 | 275. | 10.0 | 178. |
| 5 | .640 | 275. | 10.0 | 175. |
| 6 | .650 | 279. | 9.9 | 216. |
| 7 | .470 | 202. | 7.1 | 368. |
| 8 | .400 | 172. | 6.2 | 450. |
| 9 | .390 | 168. | 6.2 | 450. |
| 10 | .420 | 180. | 6.3 | 450. |
| 11 | .420 | 180. | 6.2 | 450. |
| 12 | .430 | 185. | 6.3 | 450. |
| 13 | .440 | 189. | 6.3 | 450. |
| 14 | .430 | 185. | 6.3 | 450. |
| 15 | .430 | 185. | 6.3 | 450. |
| 16 | .490 | 210. | 6.5 | 410. |
| 17 | .570 | 245. | 6.7 | 410. |
| 18 | .570 | 245. | 6.7 | 420. |
| 19 | .480 | 206. | 6.2 | 450. |
| 20 | .470 | 202. | 6.2 | 450. |
| 21 | .490 | 210. | 6.2 | 450. |
| 22 | .550 | 236. | 6.6 | 380. |
| 23 | .570 | 245. | 7.9 | 330. |
| 24 | .670 | 288. | 9.4 | 242. |

DAY = 93



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 10.0 | 176. |
| 2 | .640 | 275. | 10.0 | 176. |
| 3 | .640 | 275. | 10.0 | 176. |
| 4 | .640 | 275. | 10.0 | 178. |
| 5 | .640 | 275. | 10.0 | 176. |
| 6 | .570 | 245. | 9.6 | 220. |
| 7 | .440 | 189. | 7.7 | 340. |
| 8 | .430 | 185. | 6.3 | 450. |
| 9 | .430 | 185. | 6.2 | 450. |
| 10 | .430 | 185. | 6.2 | 450. |
| 11 | .440 | 189. | 6.2 | 450. |
| 12 | .470 | 202. | 6.7 | 380. |
| 13 | .560 | 241. | 7.3 | 330. |
| 14 | .510 | 219. | 8.0 | 330. |
| 15 | .510 | 219. | 8.0 | 330. |
| 16 | .510 | 219. | 8.1 | 330. |
| 17 | .510 | 219. | 8.1 | 330. |
| 18 | .630 | 271. | 8.6 | 330. |
| 19 | .520 | 223. | 8.0 | 330. |
| 20 | .510 | 219. | 8.0 | 330. |
| 21 | .520 | 223. | 8.0 | 330. |
| 22 | .530 | 228. | 8.0 | 330. |
| 23 | .530 | 228. | 8.0 | 330. |
| 24 | .670 | 288. | 8.7 | 280. |

DAY = 94

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .750 | 322. | 8.9 | 282. |
| 2 | .730 | 314. | 8.8 | 282. |
| 3 | .710 | 305. | 8.9 | 282. |
| 4 | .720 | 309. | 8.9 | 280. |
| 5 | .730 | 314. | 8.9 | 280. |
| 6 | .530 | 228. | 7.9 | 330. |
| 7 | .450 | 193. | 7.4 | 430. |
| 8 | .430 | 185. | 6.1 | 458. |
| 9 | .430 | 185. | 6.0 | 455. |
| 10 | .440 | 189. | 6.1 | 460. |
| 11 | .420 | 180. | 6.2 | 460. |
| 12 | .430 | 185. | 6.1 | 460. |
| 13 | .470 | 202. | 6.1 | 460. |
| 14 | .450 | 193. | 6.1 | 460. |
| 15 | .420 | 180. | 6.2 | 460. |
| 16 | .440 | 189. | 6.1 | 458. |
| 17 | .460 | 198. | 6.1 | 458. |
| 18 | .460 | 198. | 6.1 | 458. |
| 19 | .460 | 198. | 6.2 | 458. |
| 20 | .450 | 193. | 6.1 | 458. |
| 21 | .470 | 202. | 6.1 | 458. |
| 22 | .480 | 206. | 6.1 | 458. |
| 23 | .490 | 210. | 6.0 | 458. |
| 24 | .510 | 219. | 6.1 | 458. |

APPENDIX E

OKLAHOMA GAS & ELECTRIC

MUSKOGEE STATION - UNIT 5

Input Data - Revised Analysis

**PULVERIZED COAL-FIRED UTILITY BOILER NOx EMISSION MONITORING**

DATA SUBMITTED BY OKLAHOMA GAS AND ELECTRIC

MUSKOGEE STATION UNIT 5  SUBBITUMINOUS COAL  MON. REL. ACC. = 18.2 PC

DAY 1 IS OCTOBER 15, 1980

550 MWE, COMBUSTION ENGINEERING BOILER WITH OVERFIRE AIR

COAL PROPERTIES IDENTICAL TO UNIT 4

BOILER OFF-LINE FROM DEC. 13, 1980 TO DEC. 24, 1980 INCLUSIVE

**INPUT DATA**

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.8 | 325. |
| 2 | .350 | 150. | 7.7 | 280. |
| 3 | .370 | 159. | 9.0 | 180. |
| 4 | .400 | 172. | 10.0 | 180. |
| 5 | .390 | 168. | 10.0 | 180. |
| 6 | .370 | 159. | 9.3 | 265. |
| 7 | .220 | 95. | 5.4 | 425. |
| 8 | .180 | 77. | 2.5 | 469. |
| 9 | .180 | 77. | 2.8 | 471. |
| 10 | .190 | 82. | 3.3 | 472. |
| 11 | .180 | 77. | 3.4 | 490. |
| 12 | -1.000 | -430. | 1.8 | 509. |
| 13 | -1.000 | -430. | 1.5 | 508. |
| 14 | .190 | 82. | 2.5 | 514. |
| 15 | .230 | 99. | 2.8 | 514. |
| 16 | .220 | 95. | 2.7 | 514. |
| 17 | .200 | 86. | 2.6 | 515. |
| 18 | .230 | 99. | 3.4 | 500. |
| 19 | .260 | 112. | 4.2 | 480. |
| 20 | .240 | 103. | 4.1 | 400. |
| 21 | .320 | 137. | 7.5 | 325. |
| 22 | .350 | 150. | 7.8 | 325. |
| 23 | .360 | 155. | 8.1 | 325. |
| 24 | .370 | 159. | 8.0 | 325. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 10.0 | 180. |
| 2 | .510 | 219. | 10.0 | 181. |
| 3 | .510 | 219. | 10.0 | 180. |
| 4 | .520 | 223. | 10.0 | 180. |
| 5 | .500 | 215. | 10.0 | 180. |
| 6 | .510 | 219. | 10.0 | 180. |
| 7 | .500 | 215. | 9.6 | 231. |
| 8 | .460 | 198. | 8.2 | 325. |
| 9 | .480 | 206. | 8.2 | 325. |
| 10 | .470 | 202. | 8.2 | 325. |
| 11 | .490 | 210. | 8.3 | 325. |
| 12 | .490 | 210. | 8.4 | 325. |
| 13 | .490 | 210. | 8.3 | 325. |
| 14 | .460 | 198. | 8.3 | 325. |
| 15 | .470 | 202. | 8.4 | 325. |
| 16 | .470 | 202. | 8.4 | 330. |
| 17 | .490 | 210. | 8.4 | 330. |
| 18 | -1.000 | -430. | 8.4 | 330. |
| 19 | -1.000 | -430. | 8.4 | 330. |
| 20 | .500 | 215. | 8.4 | 330. |

| | | | | |
|---|---|---|---|---|
| 21 | .510 | 219. | 8.4 | 330. |
| 22 | .530 | 228. | 9.2 | 230. |
| 23 | .640 | 275. | 10.0 | 230. |
| 24 | .610 | 262. | 10.0 | 227. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.0 | 180. |
| 2 | .380 | 163. | 10.0 | 180. |
| 3 | .450 | 193. | 10.0 | 180. |
| 4 | .460 | 198. | 10.0 | 180. |
| 5 | .470 | 202. | 10.0 | 180. |
| 6 | .480 | 206. | 10.0 | 186. |
| 7 | .580 | 249. | 10.0 | 226. |
| 8 | .600 | 258. | 10.0 | 225. |
| 9 | .540 | 232. | 9.6 | 280. |
| 10 | .490 | 210. | 8.7 | 355. |
| 11 | .430 | 185. | 7.7 | 355. |
| 12 | .440 | 189. | 7.8 | 350. |
| 13 | .450 | 193. | 7.9 | 350. |
| 14 | .450 | 193. | 7.8 | 350. |
| 15 | .440 | 189. | 7.7 | 350. |
| 16 | .000 | 0. | 7.8 | 350. |
| 17 | .000 | 0. | 8.1 | 330. |
| 18 | .000 | 0. | 8.2 | 330. |
| 19 | .000 | 0. | 8.2 | 325. |
| 20 | .000 | 0. | 8.2 | 325. |
| 21 | .000 | 0. | 8.2 | 325. |
| 22 | .570 | 245. | 9.5 | 200. |
| 23 | .540 | 232. | 10.0 | 182. |
| 24 | .570 | 245. | 9.9 | 181. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 10.0 | 180. |
| 2 | .560 | 241. | 10.0 | 180. |
| 3 | .560 | 241. | 10.0 | 180. |
| 4 | .540 | 232. | 10.0 | 180. |
| 5 | .520 | 223. | 10.0 | 180. |
| 6 | .530 | 228. | 10.0 | 181. |
| 7 | .550 | 236. | 10.0 | 180. |
| 8 | .500 | 215. | 9.6 | 280. |
| 9 | .420 | 180. | 8.7 | 330. |
| 10 | .430 | 185. | 8.1 | 330. |
| 11 | .460 | 198. | 8.2 | 340. |
| 12 | .440 | 189. | 7.1 | 430. |
| 13 | .470 | 202. | 7.0 | 430. |
| 14 | .470 | 202. | 7.0 | 430. |
| 15 | .480 | 206. | 7.0 | 430. |
| 16 | .490 | 210. | 7.0 | 425. |
| 17 | .480 | 206. | 6.9 | 428. |
| 18 | .480 | 206. | 6.9 | 428. |
| 19 | .480 | 206. | 7.0 | 426. |

| | | | | |
|---|---|---|---|---|
| 20 | .500 | 215. | 7.0 | 426. |
| 21 | .510 | 219. | 7.0 | 426. |
| 22 | .540 | 232. | 7.3 | 345. |
| 23 | .540 | 232. | 8.6 | 312. |
| 24 | -1.000 | -430. | 8.9 | 290. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 10.0 | 180. |
| 2 | .000 | 0. | 10.0 | 180. |
| 3 | .000 | 0. | 10.0 | 180. |
| 4 | .000 | 0. | 10.0 | 180. |
| 5 | .000 | 0. | 10.0 | 180. |
| 6 | .000 | 0. | 10.0 | 180. |
| 7 | .000 | 0. | 10.0 | 350. |
| 8 | .530 | 228. | 8.7 | 430. |
| 9 | .420 | 180. | 6.8 | 430. |
| 10 | .420 | 180. | 6.5 | 480. |
| 11 | .330 | 142. | 5.4 | 480. |
| 12 | .320 | 137. | 5.3 | 480. |
| 13 | .330 | 142. | 5.3 | 480. |
| 14 | .360 | 155. | 5.3 | 480. |
| 15 | .360 | 155. | 5.3 | 480. |
| 16 | .360 | 155. | 5.5 | 468. |
| 17 | .390 | 168. | 5.7 | 468. |
| 18 | .390 | 168. | 5.6 | 468. |
| 19 | .360 | 155. | 5.7 | 470. |
| 20 | .360 | 155. | 5.9 | 465. |
| 21 | .370 | 159. | 6.3 | 426. |
| 22 | .380 | 163. | 6.7 | 375. |
| 23 | .400 | 172. | 7.6 | 328. |
| 24 | .410 | 176. | 8.4 | 278. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 9.8 | 180. |
| 2 | .460 | 198. | 10.0 | 180. |
| 3 | .450 | 193. | 10.0 | 180. |
| 4 | .450 | 193. | 10.0 | 180. |
| 5 | .460 | 198. | 10.0 | 180. |
| 6 | .450 | 193. | 9.9 | 220. |
| 7 | .240 | 103. | 6.8 | 425. |
| 8 | .240 | 103. | 5.1 | 460. |
| 9 | .360 | 155. | 6.2 | 345. |
| 10 | .290 | 125. | 6.9 | 330. |
| 11 | .300 | 129. | 6.8 | 330. |
| 12 | .300 | 129. | 6.8 | 330. |
| 13 | .310 | 133. | 6.8 | 330. |
| 14 | .350 | 150. | 6.9 | 330. |
| 15 | .000 | 0. | 7.0 | 330. |
| 16 | .000 | 0. | 7.0 | 330. |
| 17 | .340 | 146. | 6.7 | 375. |
| 18 | .300 | 129. | 5.3 | 460. |

| | | | | |
|---|---|---|---|---|
| 19 | .290 | 125. | 5.3 | 455. |
| 20 | .290 | 125. | 5.2 | 455. |
| 21 | .310 | 133. | 5.6 | 375. |
| 22 | .270 | 116. | 6.6 | 315. |
| 23 | .370 | 159. | 8.1 | 230. |
| 24 | .520 | 223. | 9.6 | 180. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 10.0 | 175. |
| 2 | .580 | 249. | 10.0 | 175. |
| 3 | .570 | 245. | 10.0 | 175. |
| 4 | .580 | 249. | 10.0 | 175. |
| 5 | .580 | 249. | 10.0 | 175. |
| 6 | .570 | 245. | 10.0 | 185. |
| 7 | .000 | 0. | 7.5 | 312. |
| 8 | .000 | 0. | 5.7 | 440. |
| 9 | .280 | 120. | 4.4 | 518. |
| 10 | .280 | 120. | 3.9 | 525. |
| 11 | .290 | 125. | 4.0 | 515. |
| 12 | .280 | 120. | 4.1 | 515. |
| 13 | .300 | 129. | 4.3 | 515. |
| 14 | .280 | 120. | 4.4 | 515. |
| 15 | .290 | 125. | 4.3 | 515. |
| 16 | .290 | 125. | 4.3 | 505. |
| 17 | .340 | 146. | 4.7 | 485. |
| 18 | .340 | 146. | 4.8 | 480. |
| 19 | .290 | 125. | 4.7 | 485. |
| 20 | .240 | 103. | 4.8 | 485. |
| 21 | .250 | 107. | 4.7 | 470. |
| 22 | .320 | 137. | 5.7 | 375. |
| 23 | .360 | 155. | 7.8 | 235. |
| 24 | .580 | 249. | 10.0 | 180. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 10.0 | 180. |
| 2 | .550 | 236. | 10.0 | 180. |
| 3 | .550 | 236. | 10.0 | 180. |
| 4 | .560 | 241. | 10.0 | 180. |
| 5 | .540 | 232. | 9.9 | 205. |
| 6 | .350 | 150. | 7.2 | 305. |
| 7 | .270 | 116. | 5.1 | 427. |
| 8 | .270 | 116. | 5.0 | 433. |
| 9 | .280 | 120. | 5.1 | 434. |
| 10 | .260 | 112. | 4.5 | 484. |
| 11 | .250 | 107. | 4.1 | 509. |
| 12 | .230 | 99. | 4.0 | 508. |
| 13 | .240 | 103. | 4.0 | 507. |
| 14 | .260 | 112. | 4.2 | 510. |
| 15 | .250 | 107. | 4.4 | 508. |
| 16 | .260 | 112. | 4.7 | 485. |
| 17 | .260 | 112. | 4.3 | 500. |

| | | | | |
|---|---|---|---|---|
| 18 | .270 | 116. | 4.3 | 500. |
| 19 | .270 | 116. | 4.5 | 495. |
| 20 | .280 | 120. | 4.6 | 470. |
| 21 | .300 | 129. | 5.4 | 430. |
| 22 | .320 | 137. | 5.5 | 410. |
| 23 | .320 | 137. | 6.5 | 300. |
| 24 | .420 | 180. | 7.7 | 278. |

DAY = 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 6.9 | 404. |
| 2 | .400 | 172. | 7.1 | 400. |
| 3 | .410 | 176. | 7.1 | 400. |
| 4 | .420 | 180. | 7.1 | 400. |
| 5 | .420 | 180. | 7.1 | 402. |
| 6 | .450 | 193. | 6.3 | 450. |
| 7 | .440 | 189. | 6.2 | 455. |
| 8 | .450 | 193. | 6.2 | 450. |
| 9 | .400 | 172. | 6.1 | 450. |
| 10 | .380 | 163. | 6.0 | 450. |
| 11 | .380 | 163. | 6.0 | 450. |
| 12 | .380 | 163. | 6.1 | 450. |
| 13 | .400 | 172. | 6.1 | 450. |
| 14 | .430 | 185. | 6.1 | 450. |
| 15 | .000 | 0. | 6.0 | 450. |
| 16 | .000 | 0. | 6.0 | 450. |
| 17 | .380 | 163. | 6.0 | 450. |
| 18 | .390 | 168. | 6.0 | 450. |
| 19 | .380 | 163. | 6.2 | 450. |
| 20 | .390 | 168. | 6.2 | 450. |
| 21 | .390 | 168. | 6.1 | 450. |
| 22 | .360 | 155. | 6.2 | 450. |
| 23 | .390 | 168. | 6.2 | 450. |
| 24 | .410 | 176. | 6.1 | 452. |

DAY = 39

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 6.1 | 450. |
| 2 | .390 | 168. | 6.2 | 445. |
| 3 | .440 | 189. | 6.8 | 400. |
| 4 | .440 | 189. | 6.9 | 400. |
| 5 | .450 | 193. | 6.9 | 400. |
| 6 | .450 | 193. | 6.8 | 410. |
| 7 | .410 | 176. | 6.2 | 445. |
| 8 | .420 | 180. | 6.2 | 449. |
| 9 | .420 | 180. | 6.2 | 445. |
| 10 | .390 | 168. | 6.2 | 445. |
| 11 | .400 | 172. | 6.3 | 445. |
| 12 | .400 | 172. | 6.3 | 445. |
| 13 | .410 | 176. | 6.2 | 445. |
| 14 | .390 | 168. | 6.2 | 445. |
| 15 | .380 | 163. | 6.3 | 445. |
| 16 | .400 | 172. | 6.3 | 450. |

| | | | | |
|---|---|---|---|---|
| 17 | .410 | 176. | 6.2 | 445. |
| 18 | .420 | 180. | 6.2 | 448. |
| 19 | .000 | 0. | 6.1 | 445. |
| 20 | .000 | 0. | 6.2 | 443. |
| 21 | .380 | 163. | 6.8 | 445. |
| 22 | .390 | 168. | 6.2 | 448. |
| 23 | .400 | 172. | 6.3 | 420. |
| 24 | .450 | 193. | 9.1 | 205. |

DAY = 40

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 10.1 | 180. |
| 2 | .620 | 266. | 10.1 | 180. |
| 3 | .610 | 262. | 10.1 | 180. |
| 4 | .610 | 262. | 10.1 | 175. |
| 5 | .620 | 266. | 10.1 | 175. |
| 6 | .610 | 262. | 10.1 | 175. |
| 7 | .620 | 266. | 10.1 | 175. |
| 8 | .600 | 258. | 10.0 | 230. |
| 9 | .420 | 180. | 7.3 | 435. |
| 10 | .330 | 142. | 6.2 | 435. |
| 11 | .330 | 142. | 6.0 | 440. |
| 12 | .330 | 142. | 6.0 | 440. |
| 13 | .300 | 129. | 5.9 | 440. |
| 14 | .280 | 120. | 5.8 | 440. |
| 15 | .290 | 125. | 5.8 | 440. |
| 16 | .320 | 137. | 5.9 | 445. |
| 17 | .360 | 155. | 6.1 | 447. |
| 18 | .340 | 146. | 6.1 | 447. |
| 19 | .350 | 150. | 6.1 | 448. |
| 20 | .380 | 163. | 6.1 | 445. |
| 21 | .380 | 163. | 6.1 | 448. |
| 22 | .350 | 150. | 6.1 | 447. |
| 23 | .380 | 163. | 6.3 | 390. |
| 24 | .390 | 168. | 7.9 | 275. |

DAY = 41

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 8.9 | 275. |
| 2 | .420 | 180. | 9.1 | 180. |
| 3 | .530 | 228. | 10.0 | 180. |
| 4 | .540 | 232. | 10.0 | 180. |
| 5 | .540 | 232. | 10.0 | 180. |
| 6 | .450 | 193. | 9.1 | 330. |
| 7 | .350 | 150. | 6.2 | 460. |
| 8 | .380 | 163. | 5.8 | 460. |
| 9 | .380 | 163. | 5.8 | 460. |
| 10 | .370 | 159. | 6.0 | 460. |
| 11 | .380 | 163. | 6.0 | 462. |
| 12 | .380 | 163. | 5.9 | 469. |
| 13 | .380 | 163. | 5.8 | 469. |
| 14 | .360 | 155. | 5.8 | 470. |
| 15 | .360 | 155. | 5.7 | 468. |

| | | | | |
|---|---|---|---|---|
| 16 | .340 | 146. | 5.8 | 460. |
| 17 | .320 | 137. | 5.9 | 465. |
| 18 | .350 | 150. | 5.8 | 465. |
| 19 | .370 | 159. | 5.8 | 465. |
| 20 | .370 | 159. | 5.7 | 465. |
| 21 | .380 | 163. | 5.7 | 465. |
| 22 | .380 | 163. | 5.8 | 470. |
| 23 | .340 | 146. | 5.9 | 460. |
| 24 | .380 | 163. | 6.2 | 405. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 9.6 | 255. |
| 2 | .530 | 228. | 9.6 | 255. |
| 3 | .530 | 228. | 9.6 | 255. |
| 4 | .520 | 223. | 9.5 | 262. |
| 5 | .440 | 189. | 9.2 | 360. |
| 6 | .340 | 146. | 6.8 | 440. |
| 7 | .330 | 142. | 5.9 | 460. |
| 8 | .340 | 146. | 6.0 | 460. |
| 9 | .340 | 146. | 5.9 | 460. |
| 10 | .350 | 150. | 5.9 | 460. |
| 11 | .350 | 150. | 5.9 | 465. |
| 12 | .350 | 150. | 5.8 | 465. |
| 13 | .350 | 150. | 5.7 | 465. |
| 14 | .350 | 150. | 5.7 | 465. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .330 | 142. | 6.0 | 467. |
| 17 | .330 | 142. | 5.9 | 466. |
| 18 | .340 | 146. | 5.9 | 466. |
| 19 | .330 | 142. | 6.0 | 466. |
| 20 | .330 | 142. | 6.0 | 466. |
| 21 | .350 | 150. | 5.9 | 466. |
| 22 | .350 | 150. | 5.9 | 465. |
| 23 | .340 | 146. | 6.0 | 467. |
| 24 | .350 | 150. | 5.9 | 460. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 6.0 | 458. |
| 2 | .360 | 155. | 5.9 | 455. |
| 3 | .360 | 155. | 6.1 | 453. |
| 4 | .360 | 155. | 6.1 | 450. |
| 5 | .350 | 150. | 6.2 | 450. |
| 6 | .350 | 150. | 6.1 | 452. |
| 7 | .360 | 155. | 6.1 | 452. |
| 8 | .360 | 155. | 6.0 | 450. |
| 9 | .360 | 155. | 6.0 | 455. |
| 10 | .350 | 150. | 6.0 | 455. |
| 11 | .370 | 159. | 6.1 | 455. |
| 12 | .370 | 159. | 6.2 | 455. |
| 13 | .370 | 159. | 6.2 | 450. |
| 14 | .370 | 159. | 6.2 | 450. |

| | | | | |
|---|---|---|---|---|
| 15 | .370 | 159. | 6.2 | 445. |
| 16 | .380 | 163. | 6.2 | 453. |
| 17 | .380 | 163. | 6.2 | 453. |
| 18 | .370 | 159. | 6.2 | 453. |
| 19 | .310 | 133. | 6.2 | 452. |
| 20 | .310 | 133. | 6.3 | 452. |
| 21 | .320 | 137. | 6.3 | 452. |
| 22 | .320 | 137. | 6.2 | 451. |
| 23 | .320 | 137. | 6.3 | 451. |
| 24 | .340 | 146. | 6.3 | 445. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 6.9 | 370. |
| 2 | .370 | 159. | 7.6 | 320. |
| 3 | .420 | 180. | 8.2 | 320. |
| 4 | .420 | 180. | 8.2 | 320. |
| 5 | .420 | 180. | 8.2 | 320. |
| 6 | .420 | 180. | 8.2 | 340. |
| 7 | .340 | 146. | 7.4 | 360. |
| 8 | .340 | 146. | 6.6 | 424. |
| 9 | .350 | 150. | 6.2 | 447. |
| 10 | .350 | 150. | 6.2 | 445. |
| 11 | .340 | 146. | 6.4 | 440. |
| 12 | .340 | 146. | 6.2 | 453. |
| 13 | .360 | 155. | 6.2 | 450. |
| 14 | .350 | 150. | 6.1 | 449. |
| 15 | .360 | 155. | 6.8 | 350. |
| 16 | .430 | 185. | 8.2 | 329. |
| 17 | .000 | 0. | 8.2 | 328. |
| 18 | .000 | 0. | 8.2 | 329. |
| 19 | .000 | 0. | 8.2 | 328. |
| 20 | .000 | 0. | 8.2 | 328. |
| 21 | .000 | 0. | 8.2 | 328. |
| 22 | .000 | 0. | 8.2 | 328. |
| 23 | .450 | 193. | 8.3 | 317. |
| 24 | .480 | 206. | 10.0 | 180. |

DAY = 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 6.2 | 445. |
| 2 | .370 | 159. | 6.2 | 450. |
| 3 | .370 | 159. | 6.2 | 448. |
| 4 | .380 | 163. | 6.1 | 448. |
| 5 | .380 | 163. | 6.2 | 450. |
| 6 | .380 | 163. | 6.2 | 455. |
| 7 | .380 | 163. | 6.1 | 450. |
| 8 | .400 | 172. | 6.1 | 448. |
| 9 | .420 | 180. | 6.1 | 448. |
| 10 | .440 | 189. | 6.1 | 448. |
| 11 | .410 | 176. | 6.1 | 450. |
| 12 | .380 | 163. | 6.1 | 450. |
| 13 | .380 | 163. | 6.1 | 450. |

| | | | | |
|---|---|---|---|---|
| 14 | .370 | 159. | 6.1 | 450. |
| 15 | .380 | 163. | 6.1 | 450. |
| 16 | .360 | 155. | 6.1 | 450. |
| 17 | .330 | 142. | 6.3 | 445. |
| 18 | .330 | 142. | 6.2 | 445. |
| 19 | .340 | 146. | 6.2 | 445. |
| 20 | .340 | 146. | 6.2 | 400. |
| 21 | .400 | 172. | 6.9 | 410. |
| 22 | .390 | 168. | 6.8 | 405. |
| 23 | .390 | 168. | 6.8 | 410. |
| 24 | .390 | 168. | 6.9 | 405. |

DAY = 57

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 6.9 | 405. |
| 2 | .400 | 172. | 6.8 | 405. |
| 3 | .390 | 168. | 6.8 | 425. |
| 4 | .350 | 150. | 6.2 | 442. |
| 5 | .350 | 150. | 6.2 | 445. |
| 6 | .370 | 159. | 6.2 | 448. |
| 7 | .400 | 172. | 6.2 | 448. |
| 8 | .380 | 163. | 6.2 | 450. |
| 9 | .360 | 155. | 6.1 | 449. |
| 10 | .360 | 155. | 6.1 | 448. |
| 11 | .380 | 163. | 6.2 | 448. |
| 12 | .440 | 189. | 6.4 | 451. |
| 13 | .450 | 193. | 6.3 | 452. |
| 14 | .500 | 215. | 6.2 | 448. |
| 15 | .470 | 202. | 6.2 | 438. |
| 16 | .410 | 176. | 6.2 | 450. |
| 17 | .440 | 189. | 6.2 | 450. |
| 18 | .430 | 185. | 6.1 | 450. |
| 19 | .440 | 189. | 6.3 | 450. |
| 20 | .440 | 189. | 6.3 | 450. |
| 21 | .450 | 193. | 6.2 | 450. |
| 22 | .450 | 193. | 6.2 | 450. |
| 23 | .450 | 193. | 6.2 | 450. |
| 24 | .440 | 189. | 6.4 | 428. |

DAY = 72

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .170 | 73. | 9.2 | 105. |
| 4 | .260 | 112. | 7.3 | 140. |
| 5 | .360 | 155. | 11.5 | 140. |
| 6 | .400 | 172. | 12.3 | 140. |
| 7 | .400 | 172. | 12.3 | 140. |
| 8 | .420 | 180. | 12.3 | 140. |
| 9 | .310 | 133. | 10.0 | 140. |
| 10 | .300 | 129. | 10.0 | 140. |
| 11 | .310 | 133. | 10.0 | 140. |
| 12 | .290 | 125. | 10.0 | 140. |

| | | | | |
|---|---|---|---|---|
| 13 | .270 | 116. | 10.0 | 140. |
| 14 | .270 | 116. | 10.0 | 140. |
| 15 | .260 | 112. | 10.0 | 140. |
| 16 | .260 | 112. | 10.0 | 140. |
| 17 | .250 | 107. | 10.0 | 140. |
| 18 | .250 | 107. | 10.0 | 140. |
| 19 | .240 | 103. | 10.0 | 140. |
| 20 | .250 | 107. | 10.0 | 140. |
| 21 | .260 | 112. | 10.0 | 140. |
| 22 | .240 | 103. | 10.0 | 140. |
| 23 | .230 | 99. | 10.0 | 140. |
| 24 | .240 | 103. | 10.0 | 135. |

DAY = 73

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 10.0 | 135. |
| 2 | .240 | 103. | 10.0 | 135. |
| 3 | .250 | 107. | 10.0 | 135. |
| 4 | .250 | 107. | 10.0 | 135. |
| 5 | .240 | 103. | 10.0 | 135. |
| 6 | .240 | 103. | 10.0 | 135. |
| 7 | .230 | 99. | 10.0 | 135. |
| 8 | .240 | 103. | 10.0 | 138. |
| 9 | .240 | 103. | 10.0 | 134. |
| 10 | .260 | 112. | 10.0 | 138. |
| 11 | .420 | 180. | 10.0 | 135. |
| 12 | .310 | 133. | 10.0 | 138. |
| 13 | .290 | 125. | 10.0 | 138. |
| 14 | .260 | 112. | 10.0 | 138. |
| 15 | .280 | 120. | 10.0 | 136. |
| 16 | .290 | 125. | 10.0 | 134. |
| 17 | .000 | 0. | 10.0 | 136. |
| 18 | .000 | 0. | 10.0 | 134. |
| 19 | .000 | 0. | 10.0 | 134. |
| 20 | .000 | 0. | 10.0 | 134. |
| 21 | .290 | 125. | 10.0 | 134. |
| 22 | .280 | 120. | 10.0 | 134. |
| 23 | .280 | 120. | 10.0 | 134. |
| 24 | .300 | 129. | 10.0 | 134. |

DAY = 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .540 | 232. | 6.9 | 372. |
| 2 | .530 | 228. | 7.0 | 372. |
| 3 | .510 | 219. | 7.0 | 372. |
| 4 | .520 | 223. | 7.0 | 372. |
| 5 | .540 | 232. | 7.0 | 374. |
| 6 | .540 | 232. | 7.0 | 374. |
| 7 | .550 | 236. | 7.0 | 374. |
| 8 | .550 | 236. | 7.0 | 374. |
| 9 | .560 | 241. | 7.0 | 374. |
| 10 | .560 | 241. | 6.3 | 430. |
| 11 | .550 | 236. | 6.4 | 430. |

| | | | | |
|---|---|---|---|---|
| 12 | .550 | 236. | 6.6 | 410. |
| 13 | .570 | 245. | 6.7 | 410. |
| 14 | .620 | 266. | 6.7 | 410. |
| 15 | .000 | 0. | 6.8 | 410. |
| 16 | .000 | 0. | 6.8 | 410. |
| 17 | .000 | 0. | 6.7 | 410. |
| 18 | .000 | 0. | 6.7 | 410. |
| 19 | .000 | 0. | 8.0 | 280. |
| 20 | .000 | 0. | 9.1 | 280. |
| 21 | .790 | 339. | 9.1 | 280. |
| 22 | .790 | 339. | 9.1 | 280. |
| 23 | .800 | 344. | 9.1 | 280. |
| 24 | .820 | 352. | 9.1 | 280. |

DAY = 89

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .730 | 314. | 9.0 | 272. |
| 2 | .690 | 296. | 9.1 | 272. |
| 3 | .690 | 296. | 9.1 | 272. |
| 4 | .690 | 296. | 9.0 | 272. |
| 5 | .700 | 301. | 9.1 | 274. |
| 6 | .690 | 296. | 9.0 | 279. |
| 7 | .680 | 292. | 9.0 | 272. |
| 8 | .650 | 279. | 8.3 | 325. |
| 9 | .670 | 288. | 8.0 | 325. |
| 10 | .660 | 284. | 8.7 | 280. |
| 11 | .680 | 292. | 9.0 | 280. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .250 | 107. | 10.0 | 230. |
| 17 | .760 | 326. | 9.7 | 240. |
| 18 | .730 | 314. | 9.4 | 310. |
| 19 | .520 | 223. | 7.4 | 400. |
| 20 | .450 | 193. | 6.7 | 400. |
| 21 | .530 | 228. | 7.3 | 330. |
| 22 | .590 | 253. | 7.7 | 330. |
| 23 | .600 | 258. | 7.7 | 330. |
| 24 | .590 | 253. | 7.8 | 330. |

APPENDIX F

OMAHA PUBLIC POWER DISTRICT

NEBRASKA CITY STATION - UNIT 1

Input Data

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

OMAHA PUBLIC POWER DISTRICT NEBRASKA CITY STATION UNIT 1

575 MWE, FOSTER WHEELER BOILER OPPOSED FACE FIRED WITH INTERSTAGE AIR

NOX MONITOR RELATIVE ACCURACY = 18.2 PC SUBBITUMINOUS (C) COAL

DUE TO MONITOR INOPERATIVENESS OR INACCURACY ONLY 31 DAYS OF DATA HAVE

BEEN OBTAINED FROM AUGUST 25, 1979 TO MAY 24, 1980.

DAY 1 = 8-25-79, DAY 15 = 3-12-80, DAY 22 = 5-15-80, DAY 31 = 5-24-80

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 7.3 | 317. |
| 2 | .630 | 271. | 7.4 | 261. |
| 3 | .640 | 275. | 7.5 | 248. |
| 4 | .660 | 284. | 7.6 | 247. |
| 5 | .660 | 284. | 7.7 | 247. |
| 6 | .670 | 288. | 7.6 | 247. |
| 7 | .660 | 284. | 7.5 | 247. |
| 8 | .650 | 279. | 7.4 | 255. |
| 9 | .590 | 253. | 7.3 | 300. |
| 10 | .590 | 253. | 7.3 | 292. |
| 11 | .600 | 258. | 7.3 | 293. |
| 12 | .600 | 258. | 7.3 | 293. |
| 13 | .600 | 258. | 7.4 | 296. |
| 14 | .610 | 262. | 7.4 | 295. |
| 15 | .590 | 253. | 7.4 | 303. |
| 16 | .570 | 245. | 7.2 | 347. |
| 17 | .570 | 245. | 7.2 | 346. |
| 18 | .580 | 249. | 7.2 | 331. |
| 19 | .590 | 253. | 7.3 | 323. |
| 20 | .570 | 245. | 7.1 | 359. |
| 21 | .580 | 249. | 7.1 | 359. |
| 22 | .580 | 249. | 7.1 | 361. |
| 23 | .590 | 253. | 7.2 | 334. |
| 24 | .620 | 266. | 7.3 | 299. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 7.5 | 268. |
| 2 | .650 | 279. | 7.9 | 220. |
| 3 | .690 | 296. | 8.4 | 207. |
| 4 | .690 | 296. | 8.5 | 209. |
| 5 | .700 | 301. | 8.7 | 206. |
| 6 | .710 | 305. | 8.6 | 206. |
| 7 | .690 | 296. | 8.4 | 208. |
| 8 | .690 | 296. | 8.4 | 209. |
| 9 | .660 | 284. | 8.1 | 217. |
| 10 | .570 | 245. | 7.1 | 249. |
| 11 | .590 | 253. | 7.4 | 274. |
| 12 | .570 | 245. | 7.3 | 293. |
| 13 | .560 | 241. | 7.3 | 309. |
| 14 | .570 | 245. | 7.3 | 308. |
| 15 | .580 | 249. | 7.4 | 308. |
| 16 | .590 | 253. | 7.4 | 312. |
| 17 | .580 | 249. | 7.3 | 327. |
| 18 | .570 | 245. | 9.2 | 272. |
| 19 | .560 | 241. | 9.3 | 252. |
| 20 | .590 | 253. | 9.2 | 253. |

| | | | | |
|---|---|---|---|---|
| 21 | .610 | 262. | 9.3 | 250. |
| 22 | .610 | 262. | 9.3 | 252. |
| 23 | .620 | 266. | 9.4 | 250. |
| 24 | .600 | 258. | 9.0 | 229. |

DAY = 3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 8.9 | 218. |
| 2 | .570 | 245. | 8.6 | 203. |
| 3 | .580 | 249. | 8.7 | 205. |
| 4 | .590 | 253. | 8.7 | 207. |
| 5 | .580 | 249. | 8.7 | 208. |
| 6 | .580 | 249. | 8.7 | 207. |
| 7 | .570 | 245. | 8.5 | 236. |
| 8 | .540 | 232. | 8.3 | 291. |
| 9 | .510 | 219. | 8.1 | 304. |
| 10 | .450 | 193. | 7.4 | 307. |
| 11 | .490 | 210. | 7.2 | 319. |
| 12 | .580 | 249. | 7.0 | 386. |
| 13 | .590 | 253. | 7.0 | 408. |
| 14 | .590 | 253. | 7.0 | 411. |
| 15 | .710 | 305. | 7.0 | 479. |
| 16 | .740 | 318. | 7.1 | 482. |
| 17 | .720 | 309. | 7.0 | 478. |
| 18 | .710 | 305. | 7.0 | 473. |
| 19 | .710 | 305. | 7.1 | 470. |
| 20 | .710 | 305. | 7.0 | 472. |
| 21 | .710 | 305. | 7.0 | 476. |
| 22 | .720 | 309. | 7.0 | 489. |
| 23 | .720 | 309. | 7.0 | 481. |
| 24 | .710 | 305. | 7.0 | 422. |

DAY = 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 7.2 | 306. |
| 2 | .520 | 223. | 7.2 | 267. |
| 3 | .500 | 215. | 7.2 | 265. |
| 4 | .510 | 219. | 7.3 | 264. |
| 5 | .500 | 215. | 7.3 | 282. |
| 6 | .490 | 210. | 7.2 | 282. |
| 7 | .470 | 202. | 7.1 | 302. |
| 8 | .580 | 249. | 7.1 | 364. |
| 9 | .520 | 223. | 7.9 | 350. |
| 10 | .400 | 172. | 9.4 | 185. |
| 11 | .340 | 146. | 9.4 | 151. |
| 12 | .470 | 202. | 9.5 | 141. |
| 13 | .560 | 241. | 9.2 | 195. |
| 14 | .470 | 202. | 7.7 | 242. |
| 15 | .530 | 228. | 7.4 | 294. |
| 16 | .540 | 232. | 7.7 | 323. |
| 17 | .490 | 210. | 7.4 | 342. |
| 18 | .520 | 223. | 7.0 | 402. |
| 19 | .550 | 236. | 7.0 | 442. |

| | | | | |
|---|---|---|---|---|
| 20 | .540 | 232. | 6.9 | 454. |
| 21 | .620 | 266. | 7.6 | 438. |
| 22 | .650 | 279. | 7.8 | 437. |
| 23 | .620 | 266. | 7.7 | 416. |
| 24 | .610 | 262. | 7.3 | 319. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 7.6 | 254. |
| 2 | .600 | 258. | 7.9 | 238. |
| 3 | .600 | 258. | 8.0 | 254. |
| 4 | .600 | 258. | 8.0 | 253. |
| 5 | .610 | 262. | 8.1 | 248. |
| 6 | .600 | 258. | 8.0 | 252. |
| 7 | .560 | 241. | 7.7 | 275. |
| 8 | .520 | 223. | 7.4 | 292. |
| 9 | .490 | 210. | 7.3 | 288. |
| 10 | .580 | 249. | 7.0 | 351. |
| 11 | .570 | 245. | 6.8 | 388. |
| 12 | .580 | 249. | 6.9 | 407. |
| 13 | .580 | 249. | 6.9 | 409. |
| 14 | .580 | 249. | 6.9 | 410. |
| 15 | .580 | 249. | 6.9 | 409. |
| 16 | .620 | 266. | 6.7 | 427. |
| 17 | .650 | 279. | 6.8 | 437. |
| 18 | .730 | 314. | 6.7 | 502. |
| 19 | .750 | 322. | 6.7 | 536. |
| 20 | .730 | 314. | 6.4 | 546. |
| 21 | .720 | 309. | 6.3 | 543. |
| 22 | .720 | 309. | 6.3 | 540. |
| 23 | .720 | 309. | 6.3 | 544. |
| 24 | .710 | 305. | 6.3 | 526. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.5 | 444. |
| 2 | .670 | 288. | 6.4 | 413. |
| 3 | .670 | 288. | 6.5 | 404. |
| 4 | .680 | 292. | 6.5 | 384. |
| 5 | .700 | 301. | 6.6 | 368. |
| 6 | .730 | 314. | 6.7 | 327. |
| 7 | .680 | 292. | 6.4 | 396. |
| 8 | .700 | 301. | 6.4 | 461. |
| 9 | .710 | 305. | 6.3 | 519. |
| 10 | .720 | 309. | 6.3 | 535. |
| 11 | .710 | 305. | 6.1 | 529. |
| 12 | .710 | 305. | 6.1 | 530. |
| 13 | .710 | 305. | 6.1 | 533. |
| 14 | .690 | 296. | 6.1 | 531. |
| 15 | .670 | 288. | 6.1 | 529. |
| 16 | .650 | 279. | 6.0 | 530. |
| 17 | .590 | 253. | 6.0 | 528. |
| 18 | .580 | 249. | 6.0 | 527. |

| | | | | |
|---|---|---|---|---|
| 19 | .570 | 245. | 6.0 | 530. |
| 20 | .570 | 245. | 6.0 | 529. |
| 21 | .560 | 241. | 6.0 | 524. |
| 22 | .530 | 228. | 5.8 | 518. |
| 23 | .580 | 249. | 6.0 | 517. |
| 24 | .590 | 253. | 6.1 | 524. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 6.2 | 482. |
| 2 | .550 | 236. | 6.3 | 426. |
| 3 | .550 | 236. | 6.3 | 406. |
| 4 | .450 | 193. | 6.3 | 378. |
| 5 | .440 | 189. | 6.4 | 371. |
| 6 | .450 | 193. | 6.4 | 370. |
| 7 | .500 | 215. | 6.3 | 414. |
| 8 | .610 | 262. | 6.1 | 500. |
| 9 | .630 | 271. | 6.1 | 527. |
| 10 | .580 | 249. | 6.2 | 526. |
| 11 | .560 | 241. | 6.0 | 529. |
| 12 | .560 | 241. | 6.0 | 533. |
| 13 | .540 | 232. | 6.1 | 534. |
| 14 | .520 | 223. | 6.0 | 529. |
| 15 | .490 | 210. | 6.1 | 527. |
| 16 | .420 | 180. | 6.1 | 476. |
| 17 | .430 | 185. | 6.0 | 487. |
| 18 | .530 | 228. | 6.1 | 481. |
| 19 | .580 | 249. | 6.1 | 493. |
| 20 | .620 | 266. | 6.1 | 494. |
| 21 | .650 | 279. | 6.1 | 490. |
| 22 | .630 | 271. | 6.2 | 427. |
| 23 | .490 | 210. | 6.3 | 350. |
| 24 | .390 | 168. | 6.3 | 317. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 6.6 | 285. |
| 2 | .350 | 150. | 6.4 | 275. |
| 3 | .350 | 150. | 7.6 | 232. |
| 4 | .290 | 125. | 7.4 | 209. |
| 5 | .280 | 120. | 7.6 | 205. |
| 6 | .280 | 120. | 7.5 | 204. |
| 7 | .280 | 120. | 7.4 | 207. |
| 8 | .280 | 120. | 7.4 | 204. |
| 9 | .250 | 107. | 7.3 | 224. |
| 10 | .430 | 185. | 7.5 | 278. |
| 11 | .500 | 215. | 6.7 | 357. |
| 12 | .490 | 210. | 6.5 | 401. |
| 13 | .490 | 210. | 6.6 | 396. |
| 14 | .490 | 210. | 6.6 | 404. |
| 15 | .600 | 258. | 6.5 | 468. |
| 16 | .680 | 292. | 6.6 | 500. |
| 17 | .680 | 292. | 6.6 | 446. |

| | | | | |
|---|---|---|---|---|
| 18 | .680 | 292. | 6.6 | 440. |
| 19 | .680 | 292. | 6.6 | 446. |
| 20 | .690 | 296. | 6.6 | 445. |
| 21 | .690 | 296. | 6.6 | 448. |
| 22 | .690 | 296. | 6.6 | 443. |
| 23 | .600 | 258. | 6.7 | 370. |
| 24 | .550 | 236. | 6.7 | 311. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 6.7 | 309. |
| 2 | .450 | 193. | 6.8 | 287. |
| 3 | .430 | 185. | 7.1 | 239. |
| 4 | .360 | 155. | 7.5 | 203. |
| 5 | .380 | 163. | 7.7 | 198. |
| 6 | .370 | 159. | 7.6 | 198. |
| 7 | .350 | 150. | 7.5 | 201. |
| 8 | .350 | 150. | 7.5 | 199. |
| 9 | .380 | 163. | 7.0 | 215. |
| 10 | .420 | 180. | 7.0 | 260. |
| 11 | .400 | 172. | 6.8 | 300. |
| 12 | .410 | 176. | 6.9 | 296. |
| 13 | .440 | 189. | 6.8 | 296. |
| 14 | .570 | 245. | 6.6 | 350. |
| 15 | .580 | 249. | 6.7 | 353. |
| 16 | .570 | 245. | 6.6 | 411. |
| 17 | .590 | 253. | 6.7 | 440. |
| 18 | .590 | 253. | 6.6 | 441. |
| 19 | .570 | 245. | 6.5 | 441. |
| 20 | .560 | 241. | 6.5 | 425. |
| 21 | .560 | 241. | 6.7 | 363. |
| 22 | .560 | 241. | 6.7 | 364. |
| 23 | .560 | 241. | 6.7 | 361. |
| 24 | .580 | 249. | 6.8 | 319. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 206. | 7.1 | 282. |
| 2 | .510 | 219. | 7.0 | 251. |
| 3 | .330 | 142. | 7.8 | 213. |
| 4 | .340 | 146. | 7.8 | 196. |
| 5 | .340 | 146. | 7.7 | 198. |
| 6 | .370 | 159. | 7.7 | 199. |
| 7 | .360 | 155. | 7.6 | 201. |
| 8 | .360 | 155. | 7.6 | 201. |
| 9 | .310 | 133. | 7.2 | 216. |
| 10 | .290 | 125. | 7.1 | 231. |
| 11 | .290 | 125. | 7.2 | 235. |
| 12 | .400 | 172. | 7.1 | 261. |
| 13 | .510 | 219. | 7.0 | 317. |
| 14 | .560 | 241. | 7.0 | 349. |
| 15 | .570 | 245. | 7.0 | 356. |
| 16 | .580 | 249. | 6.9 | 405. |

| | | | | |
|---|---|---|---|---|
| 17 | .670 | 288. | 6.8 | 464. |
| 18 | .710 | 305. | 6.9 | 488. |
| 19 | .720 | 309. | 6.9 | 491. |
| 20 | .720 | 309. | 6.9 | 470. |
| 21 | .700 | 301. | 6.9 | 430. |
| 22 | .690 | 296. | 6.9 | 426. |
| 23 | .580 | 249. | 6.9 | 371. |
| 24 | .580 | 249. | 6.9 | 320. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .490 | 210. | 7.2 | 277. |
| 2 | .360 | 155. | 7.5 | 216. |
| 3 | .360 | 155. | 7.7 | 197. |
| 4 | .370 | 159. | 7.6 | 199. |
| 5 | .360 | 155. | 7.5 | 202. |
| 6 | .390 | 168. | 7.9 | 196. |
| 7 | .340 | 146. | 7.6 | 216. |
| 8 | .460 | 198. | 8.1 | 278. |
| 9 | .520 | 223. | 7.1 | 302. |
| 10 | .550 | 236. | 7.3 | 309. |
| 11 | .520 | 223. | 7.1 | 341. |
| 12 | .510 | 219. | 7.0 | 348. |
| 13 | .520 | 223. | 7.0 | 334. |
| 14 | .520 | 223. | 7.0 | 333. |
| 15 | .570 | 245. | 7.0 | 401. |
| 16 | .610 | 262. | 7.1 | 460. |
| 17 | .610 | 262. | 6.9 | 476. |
| 18 | .590 | 253. | 6.8 | 472. |
| 19 | .560 | 241. | 6.8 | 469. |
| 20 | .550 | 236. | 6.8 | 470. |
| 21 | .530 | 228. | 6.9 | 450. |
| 22 | .540 | 232. | 7.1 | 414. |
| 23 | .530 | 228. | 7.0 | 373. |
| 24 | .520 | 223. | 7.0 | 378. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 7.2 | 345. |
| 2 | .480 | 206. | 7.6 | 277. |
| 3 | .480 | 206. | 7.6 | 242. |
| 4 | .460 | 198. | 7.3 | 274. |
| 5 | .450 | 193. | 7.2 | 290. |
| 6 | .450 | 193. | 7.2 | 277. |
| 7 | .460 | 198. | 7.1 | 308. |
| 8 | .520 | 223. | 7.2 | 353. |
| 9 | .570 | 245. | 6.9 | 457. |
| 10 | .560 | 241. | 6.9 | 461. |
| 11 | .550 | 236. | 7.0 | 459. |
| 12 | .520 | 223. | 7.1 | 458. |
| 13 | .510 | 219. | 7.1 | 458. |
| 14 | .470 | 202. | 7.0 | 458. |
| 15 | .450 | 193. | 7.0 | 458. |

| | | | | |
|---|---|---|---|---|
| 16 | .440 | 189. | 7.0 | 458. |
| 17 | .430 | 185. | 7.0 | 457. |
| 18 | .430 | 185. | 7.1 | 454. |
| 19 | .450 | 193. | 7.2 | 456. |
| 20 | .430 | 185. | 7.1 | 449. |
| 21 | .440 | 189. | 7.2 | 439. |
| 22 | .450 | 193. | 7.2 | 453. |
| 23 | .460 | 198. | 7.2 | 461. |
| 24 | .460 | 198. | 7.1 | 442. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 7.3 | 347. |
| 2 | .460 | 198. | 7.2 | 344. |
| 3 | .340 | 146. | 7.2 | 290. |
| 4 | .330 | 142. | 7.4 | 238. |
| 5 | .290 | 125. | 7.5 | 220. |
| 6 | .300 | 129. | 7.5 | 227. |
| 7 | .350 | 150. | 7.3 | 264. |
| 8 | .450 | 193. | 7.4 | 281. |
| 9 | .470 | 202. | 7.5 | 300. |
| 10 | .540 | 232. | 7.8 | 318. |
| 11 | .550 | 236. | 7.6 | 386. |
| 12 | .510 | 219. | 6.9 | 429. |
| 13 | .510 | 219. | 6.9 | 431. |
| 14 | .500 | 215. | 6.9 | 430. |
| 15 | .520 | 223. | 7.2 | 431. |
| 16 | .560 | 241. | 6.9 | 438. |
| 17 | .620 | 266. | 6.8 | 466. |
| 18 | .620 | 266. | 6.8 | 462. |
| 19 | .610 | 262. | 6.8 | 450. |
| 20 | .620 | 266. | 6.8 | 443. |
| 21 | .640 | 275. | 6.8 | 432. |
| 22 | .640 | 275. | 6.8 | 428. |
| 23 | .490 | 210. | 6.8 | 384. |
| 24 | .410 | 176. | 6.9 | 315. |

DAY = 14

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 7.5 | 232. |
| 2 | .370 | 159. | 8.6 | 191. |
| 3 | .440 | 189. | 9.3 | 175. |
| 4 | .470 | 202. | 9.5 | 167. |
| 5 | .450 | 193. | 9.5 | 170. |
| 6 | .410 | 176. | 9.5 | 170. |
| 7 | .330 | 142. | 8.7 | 193. |
| 8 | .260 | 112. | 7.9 | 233. |
| 9 | .380 | 163. | 7.1 | 292. |
| 10 | .590 | 253. | 7.6 | 284. |
| 11 | .450 | 193. | 7.3 | 326. |
| 12 | .400 | 172. | 7.2 | 306. |
| 13 | .400 | 172. | 7.1 | 314. |
| 14 | .410 | 176. | 7.0 | 313. |

| | | | | |
|---|---|---|---|---|
| 15 | .410 | 176. | 6.9 | 306. |
| 16 | .460 | 198. | 7.4 | 276. |
| 17 | .410 | 176. | 7.0 | 326. |
| 18 | .390 | 168. | 6.8 | 358. |
| 19 | .390 | 168. | 6.9 | 353. |
| 20 | .390 | 168. | 6.8 | 355. |
| 21 | .390 | 168. | 6.8 | 355. |
| 22 | .390 | 168. | 6.9 | 348. |
| 23 | .400 | 172. | 7.0 | 336. |
| 24 | .410 | 176. | 7.0 | 306. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 7.5 | 302. |
| 2 | .440 | 189. | 7.7 | 278. |
| 3 | .280 | 120. | 9.9 | 112. |
| 4 | -1.000 | -430. | -1.0 | -1. |
| 5 | .080 | 34. | 10.0 | 6. |
| 6 | .300 | 129. | 10.0 | 110. |
| 7 | .300 | 129. | 8.1 | 256. |
| 8 | .310 | 133. | 7.0 | 350. |
| 9 | .460 | 198. | 7.2 | 434. |
| 10 | .460 | 198. | 7.3 | 458. |
| 11 | .470 | 202. | 7.2 | 480. |
| 12 | .470 | 202. | 7.2 | 484. |
| 13 | .440 | 189. | 7.2 | 450. |
| 14 | .460 | 198. | 7.2 | 468. |
| 15 | .440 | 189. | 7.3 | 458. |
| 16 | .420 | 180. | 8.5 | 326. |
| 17 | .430 | 185. | 7.5 | 316. |
| 18 | .510 | 219. | 7.6 | 326. |
| 19 | .490 | 210. | 7.4 | 392. |
| 20 | .480 | 206. | 7.5 | 388. |
| 21 | .430 | 185. | 7.2 | 394. |
| 22 | .430 | 185. | 7.2 | 380. |
| 23 | .480 | 206. | 7.5 | 324. |
| 24 | .560 | 241. | 7.6 | 304. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 7.6 | 302. |
| 2 | .630 | 271. | 7.6 | 300. |
| 3 | .630 | 271. | 7.6 | 302. |
| 4 | .630 | 271. | 7.6 | 302. |
| 5 | .660 | 284. | 7.6 | 304. |
| 6 | .640 | 275. | 7.4 | 340. |
| 7 | .600 | 258. | 7.0 | 430. |
| 8 | .590 | 253. | 6.6 | 484. |
| 9 | .570 | 245. | 6.5 | 508. |
| 10 | .570 | 245. | 6.5 | 552. |
| 11 | .560 | 241. | 6.5 | 558. |
| 12 | .560 | 241. | 6.4 | 564. |
| 13 | .560 | 241. | 6.4 | 570. |

| | | | | |
|---|---|---|---|---|
| 14 | .570 | 245. | 6.5 | 564. |
| 15 | .560 | 241. | 6.5 | 530. |
| 16 | .560 | 241. | 6.6 | 532. |
| 17 | .550 | 236. | 6.5 | 560. |
| 18 | .560 | 241. | 6.4 | 576. |
| 19 | .560 | 241. | 6.4 | 578. |
| 20 | .540 | 232. | 6.3 | 574. |
| 21 | .540 | 232. | 6.3 | 552. |
| 22 | .550 | 236. | 6.3 | 550. |
| 23 | .550 | 236. | 6.4 | 506. |
| 24 | .570 | 245. | 6.6 | 454. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.8 | 392. |
| 2 | .440 | 189. | 6.9 | 356. |
| 3 | .430 | 185. | 6.9 | 350. |
| 4 | .430 | 185. | 6.8 | 348. |
| 5 | .440 | 189. | 6.9 | 352. |
| 6 | .430 | 185. | 6.8 | 356. |
| 7 | .420 | 180. | 6.9 | 442. |
| 8 | .600 | 258. | 6.9 | 528. |
| 9 | .610 | 262. | 6.9 | 550. |
| 10 | .600 | 258. | 6.9 | 552. |
| 11 | .600 | 258. | 6.9 | 550. |
| 12 | .590 | 253. | 6.8 | 538. |
| 13 | .590 | 253. | 6.8 | 520. |
| 14 | .600 | 258. | 6.8 | 510. |
| 15 | .590 | 253. | 6.7 | 512. |
| 16 | .600 | 258. | 6.8 | 510. |
| 17 | .590 | 253. | 6.8 | 462. |
| 18 | .600 | 258. | 6.9 | 450. |
| 19 | .590 | 253. | 6.8 | 470. |
| 20 | .580 | 249. | 6.7 | 504. |
| 21 | .590 | 253. | 6.8 | 480. |
| 22 | .590 | 253. | 6.8 | 476. |
| 23 | .600 | 258. | 6.8 | 460. |
| 24 | .600 | 258. | 6.8 | 458. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 7.0 | 396. |
| 2 | .480 | 206. | 7.1 | 354. |
| 3 | .480 | 206. | 7.2 | 348. |
| 4 | .480 | 206. | 7.2 | 348. |
| 5 | .490 | 210. | 7.2 | 348. |
| 6 | .490 | 210. | 7.2 | 352. |
| 7 | .480 | 206. | 7.1 | 368. |
| 8 | .450 | 193. | 6.9 | 410. |
| 9 | .560 | 241. | 6.8 | 478. |
| 10 | .600 | 258. | 6.7 | 548. |
| 11 | .600 | 258. | 6.7 | 558. |
| 12 | .590 | 253. | 6.7 | 534. |

| | | | | |
|---|---|---|---|---|
| 13 | .590 | 253. | 6.7 | 474. |
| 14 | .600 | 258. | 6.8 | 456. |
| 15 | .590 | 253. | 6.7 | 456. |
| 16 | .600 | 258. | 6.8 | 454. |
| 17 | .610 | 262. | 6.9 | 408. |
| 18 | .600 | 258. | 6.8 | 402. |
| 19 | .590 | 253. | 6.8 | 434. |
| 20 | .590 | 253. | 6.8 | 458. |
| 21 | .590 | 253. | 6.7 | 458. |
| 22 | .590 | 253. | 6.8 | 440. |
| 23 | .460 | 198. | 6.9 | 408. |
| 24 | .430 | 185. | 7.0 | 382. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 7.1 | 358. |
| 2 | .480 | 206. | 7.2 | 334. |
| 3 | .470 | 202. | 7.2 | 336. |
| 4 | .460 | 198. | 7.2 | 334. |
| 5 | .470 | 202. | 7.2 | 338. |
| 6 | .450 | 193. | 7.1 | 342. |
| 7 | .460 | 198. | 7.2 | 342. |
| 8 | .450 | 193. | 7.1 | 356. |
| 9 | .410 | 176. | 6.9 | 412. |
| 10 | .540 | 232. | 6.7 | 470. |
| 11 | .580 | 249. | 6.7 | 516. |
| 12 | .580 | 249. | 6.8 | 512. |
| 13 | .570 | 245. | 6.7 | 508. |
| 14 | .570 | 245. | 6.7 | 512. |
| 15 | .580 | 249. | 6.7 | 508. |
| 16 | .580 | 249. | 6.8 | 492. |
| 17 | .570 | 245. | 6.8 | 476. |
| 18 | .570 | 245. | 6.8 | 486. |
| 19 | .590 | 253. | 6.7 | 542. |
| 20 | .590 | 253. | 6.7 | 538. |
| 21 | .590 | 253. | 6.7 | 532. |
| 22 | .590 | 253. | 6.8 | 502. |
| 23 | .590 | 253. | 6.9 | 474. |
| 24 | .580 | 249. | 6.9 | 450. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 7.1 | 410. |
| 2 | .580 | 249. | 7.0 | 406. |
| 3 | .590 | 253. | 7.1 | 390. |
| 4 | .590 | 253. | 7.2 | 386. |
| 5 | .590 | 253. | 7.2 | 382. |
| 6 | .600 | 258. | 7.3 | 378. |
| 7 | .580 | 249. | 7.0 | 466. |
| 8 | .550 | 236. | 6.2 | 510. |
| 9 | .540 | 232. | 6.0 | 572. |
| 10 | .550 | 236. | 6.2 | 574. |
| 11 | .550 | 236. | 6.1 | 578. |

| | | | | |
|---|---|---|---|---|
| 12 | .540 | 232. | 6.1 | 576. |
| 13 | .530 | 228. | 6.0 | 568. |
| 14 | .540 | 232. | 6.1 | 516. |
| 15 | .530 | 228. | 6.1 | 496. |
| 16 | .520 | 223. | 6.1 | 502. |
| 17 | .470 | 202. | 5.9 | 504. |
| 18 | .530 | 228. | 6.0 | 554. |
| 19 | .530 | 228. | 5.8 | 586. |
| 20 | .540 | 232. | 5.8 | 590. |
| 21 | .530 | 228. | 5.9 | 562. |
| 22 | .530 | 228. | 6.0 | 514. |
| 23 | .500 | 215. | 6.2 | 450. |
| 24 | .350 | 150. | 6.2 | 432. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 6.3 | 415. |
| 2 | .340 | 146. | 6.4 | 381. |
| 3 | .350 | 150. | 6.4 | 385. |
| 4 | .350 | 150. | 6.5 | 380. |
| 5 | .350 | 150. | 6.5 | 387. |
| 6 | .350 | 150. | 6.4 | 397. |
| 7 | .340 | 146. | 6.1 | 462. |
| 8 | .510 | 219. | 6.0 | 515. |
| 9 | .470 | 202. | 6.0 | 539. |
| 10 | .430 | 185. | 6.0 | 536. |
| 11 | .520 | 223. | 6.0 | 535. |
| 12 | .490 | 210. | 6.0 | 512. |
| 13 | .510 | 219. | 5.8 | 498. |
| 14 | .510 | 219. | 5.8 | 503. |
| 15 | .500 | 215. | 5.3 | 504. |
| 16 | .480 | 206. | 5.8 | 504. |
| 17 | .520 | 223. | 5.9 | 475. |
| 18 | .530 | 228. | 6.1 | 443. |
| 19 | .510 | 219. | 5.9 | 506. |
| 20 | .490 | 210. | 5.8 | 557. |
| 21 | .450 | 193. | 6.0 | 505. |
| 22 | .400 | 172. | 6.2 | 424. |
| 23 | .380 | 163. | 6.4 | 391. |
| 24 | .380 | 163. | 6.4 | 394. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 7.7 | 256. |
| 2 | .540 | 232. | 7.8 | 252. |
| 3 | .530 | 228. | 7.8 | 252. |
| 4 | .520 | 223. | 7.8 | 252. |
| 5 | .510 | 219. | 7.7 | 252. |
| 6 | .520 | 223. | 7.7 | 252. |
| 7 | .510 | 219. | 7.6 | 264. |
| 8 | .420 | 180. | 6.7 | 372. |
| 9 | .580 | 249. | 5.6 | 524. |
| 10 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .270 | 116. | 9.8 | 10. |
| 16 | .420 | 180. | 9.9 | 126. |
| 17 | .370 | 159. | 8.2 | 272. |
| 18 | .510 | 219. | 7.7 | 362. |
| 19 | .370 | 159. | 6.2 | 404. |
| 20 | .360 | 155. | 6.0 | 406. |
| 21 | .370 | 159. | 6.1 | 408. |
| 22 | .410 | 176. | 6.8 | 406. |
| 23 | .370 | 159. | 6.2 | 346. |
| 24 | .450 | 193. | 6.7 | 300. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 8.6 | 242. |
| 2 | .500 | 215. | 9.0 | 228. |
| 3 | .490 | 210. | 8.9 | 232. |
| 4 | .480 | 206. | 8.9 | 230. |
| 5 | .500 | 215. | 9.1 | 234. |
| 6 | .510 | 219. | 9.0 | 232. |
| 7 | .420 | 180. | 8.8 | 238. |
| 8 | .410 | 176. | 6.9 | 344. |
| 9 | .430 | 185. | 6.4 | 428. |
| 10 | .440 | 189. | 6.4 | 428. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .430 | 185. | 5.3 | 578. |
| 13 | .430 | 185. | 5.2 | 592. |
| 14 | .420 | 180. | 5.1 | 596. |
| 15 | .420 | 180. | 5.1 | 594. |
| 16 | .440 | 189. | 5.3 | 578. |
| 17 | .440 | 189. | 5.6 | 534. |
| 18 | .430 | 185. | 5.4 | 534. |
| 19 | .470 | 202. | 5.9 | 480. |
| 20 | .470 | 202. | 6.0 | 474. |
| 21 | .470 | 202. | 5.9 | 478. |
| 22 | .440 | 189. | 6.2 | 440. |
| 23 | .400 | 172. | 7.0 | 376. |
| 24 | .340 | 146. | 7.2 | 300. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 7.5 | 262. |
| 2 | .310 | 133. | 7.2 | 276. |
| 3 | .340 | 146. | 7.8 | 254. |
| 4 | .340 | 146. | 7.9 | 252. |
| 5 | .360 | 155. | 8.2 | 252. |
| 6 | .350 | 150. | 8.1 | 252. |
| 7 | .350 | 150. | 8.1 | 252. |
| 8 | .350 | 150. | 7.9 | 256. |
| 9 | .310 | 133. | 6.8 | 328. |

| | | | | |
|---|---|---|---|---|
| 10 | .360 | 155. | 5.8 | 444. |
| 11 | .390 | 168. | 5.2 | 536. |
| 12 | .390 | 168. | 5.1 | 540. |
| 13 | .400 | 172. | 5.1 | 538. |
| 14 | .440 | 189. | 5.2 | 526. |
| 15 | .440 | 189. | 5.4 | 502. |
| 16 | .520 | 223. | 6.3 | 500. |
| 17 | .590 | 253. | 6.9 | 498. |
| 18 | .410 | 176. | 5.3 | 488. |
| 19 | .450 | 193. | 5.9 | 426. |
| 20 | .420 | 180. | 5.9 | 428. |
| 21 | .450 | 193. | 5.9 | 428. |
| 22 | .390 | 168. | 6.0 | 408. |
| 23 | .300 | 129. | 6.7 | 336. |
| 24 | .320 | 137. | 7.6 | 266. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 9.0 | 232. |
| 2 | .450 | 193. | 9.0 | 226. |
| 3 | .450 | 193. | 9.0 | 228. |
| 4 | .430 | 185. | 8.9 | 228. |
| 5 | .450 | 193. | 9.1 | 230. |
| 6 | .460 | 198. | 9.1 | 230. |
| 7 | .460 | 198. | 9.1 | 230. |
| 8 | .470 | 202. | 9.1 | 230. |
| 9 | .450 | 193. | 8.9 | 228. |
| 10 | .410 | 176. | 8.6 | 236. |
| 11 | .330 | 142. | 8.0 | 244. |
| 12 | .350 | 150. | 7.8 | 252. |
| 13 | .290 | 125. | 7.3 | 266. |
| 14 | .320 | 137. | 7.3 | 268. |
| 15 | .320 | 137. | 7.2 | 266. |
| 16 | .310 | 133. | 7.3 | 266. |
| 17 | .280 | 120. | 7.2 | 266. |
| 18 | .360 | 155. | 7.7 | 256. |
| 19 | .340 | 146. | 8.0 | 246. |
| 20 | .390 | 168. | 8.2 | 244. |
| 21 | .380 | 163. | 8.2 | 242. |
| 22 | .430 | 185. | 8.3 | 246. |
| 23 | .430 | 185. | 8.4 | 246. |
| 24 | .470 | 202. | 8.4 | 246. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .500 | 215. | 8.5 | 244. |
| 2 | .530 | 228. | 8.5 | 230. |
| 3 | .520 | 223. | 8.8 | 232. |
| 4 | .570 | 245. | 8.9 | 232. |
| 5 | .540 | 232. | 8.9 | 230. |
| 6 | .560 | 241. | 8.9 | 252. |
| 7 | .530 | 228. | 7.5 | 312. |
| 8 | .640 | 275. | 7.1 | 358. |

| | | | | |
|---|---|---|---|---|
| 9 | .740 | 318. | 7.2 | 370. |
| 10 | .740 | 318. | 6.9 | 408. |
| 11 | .690 | 296. | 6.4 | 472. |
| 12 | .600 | 258. | 6.2 | 482. |
| 13 | .630 | 271. | 6.3 | 462. |
| 14 | .640 | 275. | 6.4 | 462. |
| 15 | .630 | 271. | 6.2 | 386. |
| 16 | .670 | 288. | 6.6 | 456. |
| 17 | .630 | 271. | 6.5 | 442. |
| 18 | .640 | 275. | 6.4 | 440. |
| 19 | .690 | 296. | 6.6 | 470. |
| 20 | .720 | 309. | 6.7 | 498. |
| 21 | .720 | 309. | 6.5 | 456. |
| 22 | .690 | 296. | 6.3 | 372. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .660 | 284. | 7.2 | 336. |
| 2 | .800 | 344. | 8.6 | 250. |
| 3 | .870 | 374. | 9.1 | 236. |
| 4 | .860 | 369. | 9.0 | 234. |
| 5 | .880 | 378. | 9.1 | 236. |
| 6 | .820 | 352. | 8.8 | 244. |
| 7 | .640 | 275. | 7.2 | 336. |
| 8 | .650 | 279. | 6.8 | 384. |
| 9 | .630 | 271. | 6.5 | 430. |
| 10 | .610 | 262. | 5.8 | 508. |
| 11 | .640 | 275. | 5.9 | 506. |
| 12 | .620 | 266. | 5.8 | 530. |
| 13 | .640 | 275. | 5.9 | 506. |
| 14 | .590 | 253. | 5.8 | 532. |
| 15 | .600 | 258. | 5.7 | 536. |
| 16 | .600 | 258. | 5.8 | 524. |
| 17 | .620 | 266. | 6.0 | 522. |
| 18 | .680 | 292. | 6.6 | 524. |
| 19 | .680 | 292. | 6.8 | 496. |
| 20 | .670 | 288. | 6.9 | 468. |
| 21 | .710 | 305. | 7.1 | 452. |
| 22 | .690 | 296. | 7.1 | 440. |
| 23 | .680 | 292. | 7.6 | 360. |
| 24 | .540 | 232. | 7.1 | 342. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 7.0 | 324. |
| 2 | .530 | 228. | 7.2 | 294. |
| 3 | .600 | 258. | 7.8 | 268. |
| 4 | .650 | 279. | 8.2 | 260. |
| 5 | .710 | 305. | 8.6 | 238. |
| 6 | .750 | 322. | 8.9 | 234. |
| 7 | .590 | 253. | 7.9 | 272. |

| | | | | |
|---|---|---|---|---|
| 8 | .600 | 258. | 7.0 | 352. |
| 9 | .610 | 262. | 6.2 | 472. |
| 10 | .630 | 271. | 6.1 | 486. |
| 11 | .620 | 266. | 6.2 | 490. |
| 12 | .620 | 266. | 5.9 | 542. |
| 13 | .630 | 271. | 5.6 | 602. |
| 14 | .650 | 279. | 5.6 | 602. |
| 15 | .650 | 279. | 5.5 | 600. |
| 16 | .650 | 279. | 5.6 | 588. |
| 17 | .650 | 279. | 5.7 | 576. |
| 18 | .640 | 275. | 5.7 | 574. |
| 19 | .650 | 279. | 5.6 | 568. |
| 20 | .650 | 279. | 5.8 | 546. |
| 21 | .660 | 284. | 6.3 | 480. |
| 22 | .660 | 284. | 6.2 | 490. |
| 23 | .530 | 228. | 6.6 | 424. |
| 24 | .370 | 159. | 6.8 | 370. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 6.9 | 332. |
| 2 | .340 | 146. | 6.8 | 332. |
| 3 | .470 | 202. | 7.8 | 280. |
| 4 | .650 | 279. | 9.3 | 226. |
| 5 | .660 | 284. | 9.4 | 232. |
| 6 | .470 | 202. | 7.9 | 286. |
| 7 | .610 | 262. | 7.5 | 358. |
| 8 | .580 | 249. | 6.9 | 392. |
| 9 | .570 | 245. | 6.8 | 388. |
| 10 | .580 | 249. | 6.8 | 392. |
| 11 | .590 | 253. | 6.2 | 474. |
| 12 | .600 | 258. | 5.6 | 550. |
| 13 | .600 | 258. | 5.6 | 558. |
| 14 | .610 | 262. | 5.6 | 580. |
| 15 | .620 | 266. | 5.6 | 546. |
| 16 | .620 | 266. | 5.8 | 534. |
| 17 | .620 | 266. | 6.0 | 496. |
| 18 | .640 | 275. | 6.2 | 466. |
| 19 | .640 | 275. | 6.3 | 458. |
| 20 | .490 | 210. | 6.6 | 394. |
| 21 | .480 | 206. | 6.6 | 392. |
| 22 | .480 | 206. | 6.6 | 388. |
| 23 | .440 | 189. | 7.1 | 326. |
| 24 | .630 | 271. | 8.5 | 250. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .660 | 284. | 8.7 | 238. |
| 2 | .640 | 275. | 8.7 | 240. |
| 3 | .660 | 284. | 8.7 | 238. |
| 4 | .670 | 288. | 8.8 | 238. |
| 5 | .660 | 284. | 8.8 | 240. |
| 6 | .650 | 279. | 8.7 | 242. |

| | | | | |
|---|---|---|---|---|
| 7 | .630 | 271. | 8.8 | 266. |
| 8 | .470 | 202. | 7.3 | 324. |
| 9 | .500 | 215. | 6.4 | 318. |
| 10 | .660 | 284. | 5.9 | 576. |
| 11 | .670 | 288. | 5.6 | 634. |
| 12 | .650 | 279. | 5.5 | 632. |
| 13 | .660 | 284. | 5.7 | 598. |
| 14 | .650 | 279. | 6.4 | 492. |
| 15 | .630 | 271. | 6.5 | 462. |
| 16 | .630 | 271. | 6.7 | 460. |
| 17 | .490 | 210. | 6.8 | 454. |
| 18 | .640 | 275. | 6.7 | 454. |
| 19 | .660 | 284. | 6.7 | 450. |
| 20 | .670 | 288. | 7.0 | 404. |
| 21 | .490 | 210. | 7.1 | 362. |
| 22 | .440 | 189. | 7.0 | 362. |
| 23 | .420 | 180. | 7.1 | 354. |
| 24 | .530 | 228. | 8.2 | 266. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 8.7 | 238. |
| 2 | .570 | 245. | 8.5 | 240. |
| 3 | .550 | 236. | 8.4 | 240. |
| 4 | .540 | 232. | 8.3 | 240. |
| 5 | .570 | 245. | 8.4 | 240. |
| 6 | .560 | 241. | 8.5 | 242. |
| 7 | .560 | 241. | 8.7 | 240. |
| 8 | .540 | 232. | 8.7 | 238. |
| 9 | .450 | 193. | 8.0 | 270. |
| 10 | .560 | 241. | 7.6 | 308. |
| 11 | .480 | 206. | 7.2 | 342. |
| 12 | .450 | 193. | 7.2 | 340. |
| 13 | .450 | 193. | 7.2 | 340. |
| 14 | .460 | 198. | 7.3 | 328. |
| 15 | .460 | 198. | 7.3 | 306. |
| 16 | .500 | 215. | 7.7 | 290. |
| 17 | .490 | 210. | 7.6 | 288. |
| 18 | .490 | 210. | 7.6 | 290. |
| 19 | .480 | 206. | 7.6 | 296. |
| 20 | .570 | 245. | 8.1 | 260. |
| 21 | .560 | 241. | 8.0 | 262. |
| 22 | .520 | 223. | 7.7 | 268. |
| 23 | .500 | 215. | 7.6 | 290. |
| 24 | .570 | 245. | 8.1 | 258. |

APPENDIX G

IOWA POWER & LIGHT

COUNCIL BLUFFS STATION - UNIT 3

Input Data - Initial Analysis

**PULVERIZED COAL-FIRED UTILITY BOILER NOx EMISSION MONITORING**

IOWA POWER AND LIGHT - COUNCIL BLUFFS UNIT 3

***NOTE - CO2 USED FOR DILUTION CORRECTION, NOT O2***

BABCOCK AND WILCOX BOILER WITH DUAL REGISTER BURNERS 720 GROSS MWE

WYOMING SUBBITUMINOUS COAL NOX MON. REL. ACC. = 9.53PC

DAY 44 = 13 FEBRUARY 1981

PERFORMANCE NOX = 0.34 LB/10**6BTU (146 NG/J)

**INPUT DATA**

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .270 | 116. | 14.7 | 485. |
| 2 | .330 | 142. | 15.3 | 608. |
| 3 | .360 | 155. | 15.0 | 622. |
| 4 | .370 | 159. | 15.1 | 639. |
| 5 | .380 | 163. | 15.2 | 640. |
| 6 | .390 | 168. | 15.1 | 650. |
| 7 | .410 | 176. | 15.1 | 678. |
| 8 | .410 | 176. | 15.3 | 702. |
| 9 | .410 | 176. | 15.3 | 709. |
| 10 | .420 | 180. | 15.2 | 709. |
| 11 | .420 | 180. | 15.3 | 709. |
| 12 | .420 | 180. | 15.4 | 709. |
| 13 | .410 | 176. | 15.4 | 709. |
| 14 | .400 | 172. | 15.6 | 708. |
| 15 | .390 | 168. | 15.5 | 700. |
| 16 | .380 | 163. | 15.8 | 700. |
| 17 | .380 | 163. | 15.8 | 701. |
| 18 | .380 | 163. | 15.8 | 685. |
| 19 | .390 | 168. | 15.7 | 683. |
| 20 | .400 | 172. | 15.5 | 683. |
| 21 | .400 | 172. | 15.5 | 683. |
| 22 | .400 | 172. | 15.5 | 680. |
| 23 | .380 | 163. | 15.4 | 624. |
| 24 | .360 | 155. | 15.4 | 598. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .310 | 133. | 15.0 | 507. |
| 2 | .260 | 112. | 15.0 | 447. |
| 3 | .250 | 107. | 15.3 | 461. |
| 4 | .260 | 112. | 15.3 | 469. |
| 5 | .260 | 112. | 15.2 | 459. |
| 6 | .300 | 129. | 15.5 | 539. |
| 7 | .340 | 146. | 15.3 | 585. |
| 8 | .340 | 146. | 15.3 | 601. |
| 9 | .360 | 155. | 15.5 | 647. |
| 10 | .380 | 163. | 15.4 | 676. |
| 11 | .380 | 163. | 15.4 | 679. |
| 12 | .370 | 159. | 15.4 | 660. |
| 13 | .360 | 155. | 15.4 | 635. |
| 14 | .340 | 146. | 15.3 | 609. |
| 15 | .330 | 142. | 15.3 | 590. |
| 16 | .330 | 142. | 15.5 | 578. |
| 17 | .320 | 137. | 15.6 | 584. |
| 18 | .370 | 159. | 15.1 | 628. |
| 19 | .400 | 172. | 14.8 | 680. |
| 20 | .430 | 185. | 13.7 | 678. |

| | | | | |
|---|---|---|---|---|
| 21 | .410 | 189. | 12.8 | 628. |
| 22 | .460 | 198. | 12.6 | 611. |
| 23 | .410 | 176. | 12.4 | 551. |
| 24 | .380 | 163. | 12.4 | 486. |

DAY = 46

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 12.3 | 441. |
| 2 | .350 | 150. | 12.1 | 423. |
| 3 | .340 | 146. | 12.1 | 402. |
| 4 | .320 | 137. | 12.3 | 418. |
| 5 | .310 | 133. | 12.3 | 421. |
| 6 | .320 | 137. | 12.4 | 449. |
| 7 | .320 | 137. | 12.4 | 456. |
| 8 | .330 | 142. | 12.5 | 480. |
| 9 | .330 | 142. | 12.6 | 507. |
| 10 | .330 | 142. | 12.7 | 555. |
| 11 | .350 | 150. | 12.7 | 600. |
| 12 | .380 | 163. | 12.7 | 645. |
| 13 | .410 | 176. | 12.7 | 645. |
| 14 | .400 | 172. | 12.5 | 543. |
| 15 | .380 | 163. | 12.5 | 511. |
| 16 | .350 | 150. | 12.5 | 492. |
| 17 | .340 | 146. | 12.7 | 541. |
| 18 | .380 | 163. | 13.2 | 696. |
| 19 | .410 | 176. | 13.2 | 692. |
| 20 | .440 | 189. | 13.1 | 690. |
| 21 | .440 | 189. | 13.2 | 690. |
| 22 | .440 | 189. | 13.3 | 679. |
| 23 | .420 | 180. | 12.6 | 562. |
| 24 | .380 | 163. | 12.1 | 499. |



DAY = 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 11.6 | 435. |
| 2 | .320 | 137. | 11.4 | 404. |
| 3 | .310 | 133. | 11.4 | 383. |
| 4 | .320 | 137. | 11.2 | 359. |
| 5 | .310 | 133. | 11.3 | 372. |
| 6 | .330 | 142. | 11.8 | 462. |
| 7 | .390 | 168. | 12.1 | 561. |
| 8 | .450 | 193. | 12.1 | 621. |
| 9 | .470 | 202. | 12.2 | 671. |
| 10 | .440 | 189. | 12.4 | 678. |
| 11 | .430 | 185. | 12.6 | 678. |
| 12 | .430 | 185. | 12.6 | 685. |
| 13 | .440 | 189. | 12.4 | 667. |
| 14 | .440 | 189. | 12.4 | 653. |
| 15 | .430 | 185. | 12.5 | 641. |
| 16 | .440 | 189. | 12.6 | 643. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .410 | 176. | 13.7 | 664. |
| 19 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 20 | .400 | 172. | 14.0 | 650. |
| 21 | .410 | 176. | 14.1 | 668. |
| 22 | -1.000 | -430. | -1.0 | -1. |
| 23 | .340 | 146. | 13.9 | 537. |
| 24 | .280 | 120. | 13.5 | 416. |

DAY = 48

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 13.6 | 359. |
| 2 | .240 | 103. | 13.4 | 339. |
| 3 | .250 | 107. | 13.2 | 327. |
| 4 | .240 | 103. | 13.2 | 314. |
| 5 | .240 | 103. | 13.1 | 325. |
| 6 | .260 | 112. | 13.7 | 391. |
| 7 | .300 | 129. | 14.5 | 549. |
| 8 | .380 | 163. | 15.4 | 687. |
| 9 | .400 | 172. | 15.8 | 734. |
| 10 | .390 | 168. | 16.0 | 750. |
| 11 | .380 | 163. | 16.1 | 748. |
| 12 | .370 | 159. | 16.2 | 751. |
| 13 | .370 | 159. | 16.0 | 739. |
| 14 | .360 | 155. | 15.5 | 683. |
| 15 | .360 | 155. | 15.6 | 676. |
| 16 | .350 | 150. | 15.7 | 674. |
| 17 | .350 | 150. | 15.9 | 675. |
| 18 | .350 | 150. | 16.6 | 676. |
| 19 | .350 | 150. | 16.7 | 674. |
| 20 | .350 | 150. | 16.3 | 665. |
| 21 | .320 | 137. | 15.9 | 578. |
| 22 | .290 | 125. | 15.7 | 527. |
| 23 | .260 | 112. | 15.5 | 465. |
| 24 | .210 | 90. | 15.6 | 377. |

DAY = 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .190 | 82. | 15.8 | 366. |
| 2 | .190 | 82. | 15.8 | 357. |
| 3 | .200 | 86. | 15.4 | 375. |
| 4 | .200 | 86. | 15.5 | 369. |
| 5 | .210 | 90. | 15.4 | 364. |
| 6 | .220 | 95. | 15.4 | 395. |
| 7 | .270 | 116. | 15.8 | 523. |
| 8 | .340 | 146. | 16.3 | 663. |
| 9 | .370 | 159. | 16.4 | 730. |
| 10 | .360 | 155. | 16.4 | 728. |
| 11 | .360 | 155. | 16.5 | 729. |
| 12 | .360 | 155. | 16.5 | 729. |
| 13 | .360 | 155. | 16.5 | 730. |
| 14 | .370 | 159. | 16.5 | 731. |
| 15 | .360 | 155. | 16.4 | 721. |
| 16 | .370 | 159. | 16.5 | 718. |
| 17 | .370 | 159. | 16.5 | 719. |
| 18 | .360 | 155. | 16.6 | 724. |

| | | | | |
|---|---|---|---|---|
| 19 | .350 | 150. | 17.0 | 728. |
| 20 | .350 | 150. | 16.8 | 701. |
| 21 | .370 | 159. | 16.6 | 686. |
| 22 | .320 | 137. | 16.4 | 610. |
| 23 | .270 | 116. | 16.3 | 557. |
| 24 | .240 | 103. | 16.1 | 497. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 15.9 | 432. |
| 2 | .250 | 107. | 15.8 | 435. |
| 3 | .240 | 103. | 15.7 | 413. |
| 4 | .230 | 99. | 15.9 | 418. |
| 5 | .220 | 95. | 15.9 | 424. |
| 6 | .230 | 99. | 15.9 | 469. |
| 7 | .280 | 120. | 16.4 | 583. |
| 8 | .330 | 142. | 16.5 | 679. |
| 9 | .340 | 146. | 16.5 | 692. |
| 10 | .340 | 146. | 16.3 | 684. |
| 11 | .330 | 142. | 16.3 | 679. |
| 12 | .340 | 146. | 16.4 | 686. |
| 13 | .340 | 146. | 16.3 | 664. |
| 14 | .340 | 146. | 16.5 | 681. |
| 15 | .340 | 146. | 16.4 | 682. |
| 16 | .340 | 146. | 16.5 | 685. |
| 17 | .330 | 142. | 16.5 | 663. |
| 18 | .330 | 142. | 16.5 | 664. |
| 19 | .330 | 142. | 16.5 | 636. |
| 20 | .330 | 142. | 16.6 | 651. |
| 21 | .330 | 142. | 16.5 | 629. |
| 22 | .340 | 146. | 16.6 | 672. |
| 23 | .320 | 137. | 16.3 | 611. |
| 24 | .260 | 112. | 15.8 | 493. |

DAY = 51

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 16.0 | 474. |
| 2 | .240 | 103. | 16.1 | 502. |
| 3 | .240 | 103. | 15.9 | 493. |
| 4 | .240 | 103. | 15.8 | 488. |
| 5 | .240 | 103. | 15.7 | 472. |
| 6 | .250 | 107. | 15.7 | 511. |
| 7 | .340 | 146. | 16.2 | 652. |
| 8 | .370 | 159. | 16.0 | 690. |
| 9 | .360 | 155. | 16.1 | 696. |
| 10 | .350 | 150. | 16.2 | 692. |
| 11 | .360 | 155. | 16.1 | 689. |
| 12 | .350 | 150. | 16.1 | 667. |
| 13 | .360 | 155. | 16.2 | 670. |
| 14 | .360 | 155. | 16.2 | 674. |
| 15 | .340 | 146. | 16.3 | 656. |
| 16 | .340 | 146. | 16.3 | 652. |
| 17 | .330 | 142. | 16.3 | 645. |

| | | | | |
|---|---|---|---|---|
| 18 | .330 | 142. | 16.2 | 632. |
| 19 | .340 | 146. | 16.3 | 661. |
| 20 | .360 | 155. | 15.9 | 672. |
| 21 | .380 | 163. | 15.7 | 692. |
| 22 | .320 | 137. | 15.6 | 593. |
| 23 | .230 | 99. | 15.1 | 435. |
| 24 | .200 | 86. | 15.2 | 369. |

DAY # 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 15.0 | 338. |
| 2 | .200 | 86. | 14.8 | 322. |
| 3 | .210 | 90. | 14.8 | 322. |
| 4 | .200 | 86. | 14.8 | 313. |
| 5 | .210 | 90. | 14.6 | 304. |
| 6 | .220 | 95. | 14.5 | 308. |
| 7 | .220 | 95. | 15.0 | 352. |
| 8 | .250 | 107. | 15.3 | 487. |
| 9 | .310 | 133. | 15.8 | 655. |
| 10 | .340 | 146. | 15.9 | 693. |
| 11 | .340 | 146. | 15.8 | 693. |
| 12 | .330 | 142. | 15.7 | 675. |
| 13 | .320 | 137. | 15.7 | 661. |
| 14 | .310 | 133. | 15.6 | 623. |
| 15 | .290 | 125. | 15.6 | 594. |
| 16 | .290 | 125. | 15.6 | 573. |
| 17 | .300 | 129. | 15.7 | 594. |
| 18 | .320 | 137. | 15.7 | 637. |
| 19 | .310 | 133. | 15.6 | 627. |
| 20 | .340 | 146. | 15.7 | 667. |
| 21 | .330 | 142. | 15.2 | 590. |
| 22 | .320 | 137. | 15.3 | 580. |
| 23 | .310 | 133. | 15.4 | 578. |
| 24 | .270 | 116. | 15.1 | 497. |

DAY # 53

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 15.1 | 460. |
| 2 | .240 | 103. | 15.1 | 442. |
| 3 | .190 | 82. | 14.6 | 334. |
| 4 | .180 | 77. | 14.8 | 327. |
| 5 | .170 | 73. | 15.0 | 326. |
| 6 | .170 | 73. | 15.0 | 332. |
| 7 | .180 | 77. | 15.0 | 333. |
| 8 | .240 | 103. | 15.3 | 462. |
| 9 | .280 | 120. | 15.2 | 540. |
| 10 | .310 | 133. | 15.2 | 567. |
| 11 | .320 | 137. | 15.1 | 591. |
| 12 | .350 | 150. | 15.3 | 653. |
| 13 | .360 | 155. | 15.4 | 661. |
| 14 | .340 | 146. | 15.3 | 625. |
| 15 | .320 | 137. | 15.1 | 596. |
| 16 | .320 | 137. | 15.3 | 610. |

| | | | | |
|---|---|---|---|---|
| 17 | .330 | 142. | 15.4 | 627. |
| 18 | .330 | 142. | 15.6 | 632. |
| 19 | .320 | 137. | 15.6 | 617. |
| 20 | .330 | 142. | 15.6 | 627. |
| 21 | .340 | 146. | 15.6 | 636. |
| 22 | .340 | 146. | 15.6 | 634. |
| 23 | .320 | 137. | 15.3 | 587. |
| 24 | .280 | 120. | 15.1 | 511. |

DAY = 54

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.3 | 514. |
| 2 | .270 | 116. | 15.2 | 532. |
| 3 | .270 | 116. | 15.1 | 519. |
| 4 | .270 | 116. | 15.2 | 526. |
| 5 | .260 | 112. | 15.1 | 525. |
| 6 | .270 | 116. | 15.1 | 522. |
| 7 | .300 | 129. | 15.2 | 597. |
| 8 | .350 | 150. | 15.4 | 679. |
| 9 | .370 | 159. | 15.3 | 705. |
| 10 | .380 | 163. | 15.2 | 692. |
| 11 | .390 | 168. | 15.2 | 699. |
| 12 | .390 | 168. | 15.2 | 700. |
| 13 | .380 | 163. | 15.3 | 689. |
| 14 | .380 | 163. | 15.4 | 694. |
| 15 | .380 | 163. | 15.4 | 692. |
| 16 | .380 | 163. | 15.4 | 685. |
| 17 | .370 | 159. | 15.5 | 679. |
| 18 | .380 | 163. | 15.5 | 680. |
| 19 | .390 | 168. | 15.5 | 683. |
| 20 | .390 | 168. | 15.5 | 678. |
| 21 | .390 | 168. | 15.6 | 686. |
| 22 | .400 | 172. | 15.6 | 690. |
| 23 | .380 | 163. | 15.5 | 665. |
| 24 | .310 | 133. | 15.3 | 542. |

DAY = 55

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 15.4 | 536. |
| 2 | .310 | 133. | 15.5 | 556. |
| 3 | .320 | 137. | 15.4 | 557. |
| 4 | .330 | 142. | 15.4 | 563. |
| 5 | .310 | 133. | 15.5 | 562. |
| 6 | .300 | 129. | 15.6 | 570. |
| 7 | .320 | 137. | 15.5 | 596. |
| 8 | .350 | 150. | 15.5 | 662. |
| 9 | .350 | 150. | 15.5 | 664. |
| 10 | .340 | 146. | 15.4 | 652. |
| 11 | .360 | 155. | 15.5 | 664. |
| 12 | .380 | 163. | 15.5 | 683. |
| 13 | .380 | 163. | 15.5 | 694. |
| 14 | .390 | 168. | 15.5 | 691. |
| 15 | .370 | 159. | 15.5 | 684. |

| | | | | |
|---|---|---|---|---|
| 16 | .380 | 163. | 14.5 | 666. |
| 17 | .380 | 163. | 14.7 | 665. |
| 18 | .380 | 163. | 15.5 | 662. |
| 19 | .370 | 159. | 15.6 | 675. |
| 20 | .390 | 168. | 15.7 | 694. |
| 21 | .390 | 168. | 15.8 | 690. |
| 22 | .360 | 155. | 15.9 | 642. |
| 23 | .360 | 155. | 16.0 | 646. |
| 24 | .320 | 137. | 15.7 | 580. |

DAY # 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.7 | 532. |
| 2 | .290 | 125. | 15.6 | 524. |
| 3 | .280 | 120. | 15.6 | 504. |
| 4 | .260 | 112. | 15.5 | 485. |
| 5 | .270 | 116. | 15.6 | 501. |
| 6 | .310 | 133. | 15.8 | 588. |
| 7 | .350 | 150. | 15.8 | 640. |
| 8 | .370 | 159. | 15.7 | 664. |
| 9 | .390 | 168. | 15.6 | 681. |
| 10 | .390 | 168. | 15.6 | 671. |
| 11 | .390 | 168. | 15.6 | 683. |
| 12 | .380 | 163. | 15.7 | 689. |
| 13 | .360 | 155. | 15.6 | 659. |
| 14 | .360 | 155. | 15.8 | 668. |
| 15 | .360 | 155. | 15.8 | 670. |
| 16 | .360 | 155. | 15.8 | 674. |
| 17 | .340 | 146. | 15.8 | 642. |
| 18 | .370 | 159. | 15.9 | 677. |
| 19 | .360 | 155. | 15.9 | 673. |
| 20 | .360 | 155. | 15.9 | 675. |
| 21 | .370 | 159. | 16.0 | 678. |
| 22 | .360 | 155. | 15.6 | 649. |
| 23 | .320 | 137. | 15.5 | 571. |
| 24 | .280 | 120. | 15.2 | 485. |

DAY # 57

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.5 | 468. |
| 2 | .260 | 112. | 15.4 | 462. |
| 3 | .260 | 112. | 15.3 | 459. |
| 4 | .260 | 112. | 15.4 | 469. |
| 5 | .260 | 112. | 15.3 | 467. |
| 6 | .280 | 120. | 15.4 | 500. |
| 7 | .350 | 150. | 15.5 | 639. |
| 8 | .370 | 159. | 15.3 | 642. |
| 9 | .370 | 159. | 15.5 | 682. |
| 10 | .370 | 159. | 15.6 | 692. |
| 11 | .370 | 159. | 15.6 | 693. |
| 12 | .390 | 168. | 15.5 | 690. |
| 13 | .380 | 163. | 15.5 | 671. |
| 14 | .380 | 163. | 15.6 | 684. |

| | | | | |
|---|---|---|---|---|
| 15 | .380 | 163. | 15.6 | 686. |
| 16 | .380 | 163. | 15.5 | 684. |
| 17 | .380 | 163. | 15.5 | 682. |
| 18 | .370 | 159. | 15.5 | 665. |
| 19 | .370 | 159. | 15.6 | 676. |
| 20 | .370 | 159. | 15.6 | 678. |
| 21 | .360 | 155. | 15.6 | 675. |
| 22 | .370 | 159. | 15.6 | 693. |
| 23 | .370 | 159. | 15.6 | 688. |
| 24 | .340 | 146. | 15.4 | 617. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 15.4 | 553. |
| 2 | .290 | 125. | 15.3 | 529. |
| 3 | .280 | 120. | 15.3 | 515. |
| 4 | .280 | 120. | 15.3 | 511. |
| 5 | .270 | 116. | 15.3 | 508. |
| 6 | .290 | 125. | 15.6 | 558. |
| 7 | .310 | 133. | 15.6 | 603. |
| 8 | .350 | 150. | 15.5 | 641. |
| 9 | .340 | 146. | 15.6 | 651. |
| 10 | .350 | 150. | 15.7 | 670. |
| 11 | .360 | 155. | 15.6 | 683. |
| 12 | .370 | 159. | 15.6 | 678. |
| 13 | .360 | 155. | 15.6 | 671. |
| 14 | .370 | 159. | 15.7 | 688. |
| 15 | .370 | 159. | 15.6 | 678. |
| 16 | .370 | 159. | 15.7 | 685. |
| 17 | .380 | 163. | 15.7 | 693. |
| 18 | .390 | 168. | 15.5 | 679. |
| 19 | .380 | 163. | 15.5 | 678. |
| 20 | .370 | 159. | 15.6 | 686. |
| 21 | .350 | 150. | 15.7 | 683. |
| 22 | .340 | 146. | 15.6 | 659. |
| 23 | .310 | 133. | 15.4 | 597. |
| 24 | .280 | 120. | 15.2 | 531. |

DAY = 59

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.3 | 520. |
| 2 | .270 | 116. | 15.3 | 519. |
| 3 | .260 | 112. | 15.3 | 507. |
| 4 | .260 | 112. | 15.3 | 518. |
| 5 | .260 | 112. | 15.3 | 517. |
| 6 | .270 | 116. | 15.3 | 537. |
| 7 | .280 | 120. | 15.2 | 542. |
| 8 | .290 | 125. | 15.3 | 577. |
| 9 | .320 | 137. | 15.5 | 637. |
| 10 | .350 | 150. | 15.3 | 673. |
| 11 | .350 | 150. | 15.3 | 677. |
| 12 | .350 | 150. | 15.3 | 672. |
| 13 | .360 | 155. | 15.4 | 665. |

| | | | | |
|---|---|---|---|---|
| 14 | .370 | 159. | 15.5 | 679. |
| 15 | .360 | 155. | 15.4 | 671. |
| 16 | .360 | 155. | 15.5 | 680. |
| 17 | .360 | 155. | 15.5 | 684. |
| 18 | .360 | 155. | 15.6 | 689. |
| 19 | .350 | 150. | 15.6 | 683. |
| 20 | .350 | 150. | 15.5 | 675. |
| 21 | .340 | 146. | 15.4 | 661. |
| 22 | .340 | 146. | 15.5 | 665. |
| 23 | .320 | 137. | 15.4 | 623. |
| 24 | .290 | 125. | 15.3 | 564. |

DAY = 60

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.3 | 536. |
| 2 | .290 | 125. | 15.4 | 547. |
| 3 | .270 | 116. | 15.2 | 518. |
| 4 | .270 | 116. | 15.2 | 510. |
| 5 | .270 | 116. | 15.2 | 510. |
| 6 | .270 | 116. | 15.2 | 515. |
| 7 | .300 | 129. | 15.2 | 542. |
| 8 | .310 | 133. | 15.2 | 575. |
| 9 | .320 | 137. | 15.3 | 603. |
| 10 | .330 | 142. | 15.3 | 623. |
| 11 | .330 | 142. | 15.3 | 620. |
| 12 | .330 | 142. | 15.2 | 611. |
| 13 | .330 | 142. | 15.2 | 606. |
| 14 | .320 | 137. | 15.2 | 589. |
| 15 | .300 | 129. | 14.9 | 545. |
| 16 | .290 | 125. | 15.1 | 534. |
| 17 | .290 | 125. | 15.2 | 546. |
| 18 | .310 | 133. | 15.4 | 586. |
| 19 | .350 | 150. | 15.4 | 653. |
| 20 | .340 | 146. | 15.3 | 642. |
| 21 | .340 | 146. | 15.3 | 640. |
| 22 | .340 | 146. | 15.4 | 635. |
| 23 | .320 | 137. | 15.2 | 603. |
| 24 | .270 | 116. | 15.1 | 510. |

DAY = 61

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.1 | 451. |
| 2 | .250 | 107. | 15.2 | 445. |
| 3 | .240 | 103. | 15.3 | 455. |
| 4 | .240 | 103. | 15.2 | 474. |
| 5 | .250 | 107. | 15.1 | 488. |
| 6 | .270 | 116. | 15.1 | 526. |
| 7 | .300 | 129. | 15.3 | 617. |
| 8 | .330 | 142. | 15.3 | 658. |
| 9 | .360 | 155. | 15.4 | 694. |
| 10 | .370 | 159. | 15.3 | 693. |
| 11 | .380 | 163. | 15.2 | 693. |
| 12 | .380 | 163. | 15.2 | 687. |

| | | | | |
|---|---|---|---|---|
| 13 | .380 | 163. | 15.3 | 684. |
| 14 | .370 | 159. | 15.3 | 691. |
| 15 | .370 | 159. | 15.2 | 670. |
| 16 | .360 | 155. | 15.4 | 680. |
| 17 | .350 | 150. | 15.3 | 671. |
| 18 | .350 | 150. | 15.4 | 688. |
| 19 | .350 | 150. | 15.4 | 688. |
| 20 | .360 | 155. | 15.5 | 695. |
| 21 | .360 | 155. | 15.4 | 686. |
| 22 | .370 | 159. | 15.4 | 689. |
| 23 | .360 | 155. | 15.3 | 654. |
| 24 | .340 | 146. | 15.0 | 540. |

DAY # 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.1 | 524. |
| 2 | .280 | 120. | 15.1 | 517. |
| 3 | .290 | 125. | 15.1 | 515. |
| 4 | .290 | 125. | 15.1 | 514. |
| 5 | .290 | 125. | 15.1 | 525. |
| 6 | .280 | 120. | 15.3 | 547. |
| 7 | .320 | 137. | 15.5 | 639. |
| 8 | .350 | 150. | 15.4 | 683. |
| 9 | .360 | 155. | 15.3 | 689. |
| 10 | .370 | 159. | 15.3 | 689. |
| 11 | .360 | 155. | 15.2 | 672. |
| 12 | .370 | 159. | 15.3 | 683. |
| 13 | .370 | 159. | 15.3 | 689. |
| 14 | .350 | 150. | 15.5 | 690. |
| 15 | .340 | 146. | 15.5 | 672. |
| 16 | .340 | 146. | 15.5 | 681. |
| 17 | .340 | 146. | 15.4 | 685. |
| 18 | .350 | 150. | 15.3 | 679. |
| 19 | .360 | 155. | 15.4 | 691. |
| 20 | .350 | 150. | 15.3 | 669. |
| 21 | .360 | 155. | 15.4 | 692. |
| 22 | .360 | 155. | 15.3 | 682. |
| 23 | .320 | 137. | 15.1 | 598. |
| 24 | .280 | 120. | 14.8 | 508. |

DAY # 63

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 14.7 | 469. |
| 2 | .250 | 107. | 15.0 | 467. |
| 3 | .240 | 103. | 15.0 | 452. |
| 4 | .240 | 103. | 15.0 | 444. |
| 5 | .230 | 99. | 15.1 | 453. |
| 6 | .240 | 103. | 15.1 | 483. |
| 7 | .280 | 120. | 15.4 | 577. |
| 8 | .330 | 142. | 15.4 | 648. |
| 9 | .340 | 146. | 15.5 | 685. |
| 10 | .350 | 150. | 15.4 | 683. |
| 11 | .340 | 146. | 15.4 | 698. |

| | | | | |
|---|---|---|---|---|
| 12 | .340 | 146. | 15.4 | 696. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .350 | 150. | 15.3 | 684. |
| 18 | .350 | 150. | 15.3 | 686. |
| 19 | .350 | 150. | 15.4 | 698. |
| 20 | .360 | 155. | 15.3 | 698. |
| 21 | .360 | 155. | 15.3 | 698. |
| 22 | .350 | 150. | 15.3 | 698. |
| 23 | .340 | 146. | 15.2 | 668. |
| 24 | .260 | 112. | 14.6 | 474. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .190 | 82. | 14.6 | 377. |
| 2 | .170 | 73. | 14.9 | 361. |
| 3 | .170 | 73. | 14.9 | 380. |
| 4 | .170 | 73. | 15.1 | 399. |
| 5 | .220 | 95. | 15.0 | 452. |
| 6 | .290 | 125. | 15.0 | 533. |
| 7 | .310 | 133. | 15.2 | 591. |
| 8 | .340 | 146. | 15.4 | 674. |
| 9 | .360 | 155. | 15.3 | 699. |
| 10 | .360 | 155. | 15.3 | 699. |
| 11 | .360 | 155. | 15.2 | 698. |
| 12 | .370 | 159. | 15.2 | 698. |
| 13 | .370 | 159. | 15.2 | 687. |
| 14 | .360 | 155. | 15.3 | 686. |
| 15 | .350 | 150. | 15.3 | 686. |
| 16 | .350 | 150. | 15.3 | 684. |
| 17 | .350 | 150. | 15.3 | 659. |
| 18 | .350 | 150. | 15.3 | 667. |
| 19 | .360 | 155. | 15.5 | 698. |
| 20 | .350 | 150. | 15.5 | 699. |
| 21 | .350 | 150. | 15.5 | 694. |
| 22 | .340 | 146. | 15.3 | 665. |
| 23 | .310 | 133. | 14.7 | 564. |
| 24 | .260 | 112. | 14.4 | 466. |

DAY = 65

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 14.6 | 445. |
| 2 | .240 | 103. | 14.8 | 471. |
| 3 | .230 | 99. | 14.7 | 464. |
| 4 | .240 | 103. | 14.7 | 458. |
| 5 | .240 | 103. | 14.8 | 476. |
| 6 | .260 | 112. | 15.1 | 551. |
| 7 | .330 | 142. | 15.1 | 622. |
| 8 | .360 | 155. | 15.2 | 677. |
| 9 | .360 | 155. | 15.2 | 689. |
| 10 | .360 | 155. | 15.3 | 688. |

| | | | | |
|---|---|---|---|---|
| 11 | .360 | 155. | 15.3 | 688. |
| 12 | .350 | 150. | 15.4 | 689. |
| 13 | .340 | 146. | 15.5 | 689. |
| 14 | .340 | 146. | 15.5 | 688. |
| 15 | .350 | 150. | 15.5 | 688. |
| 16 | .350 | 150. | 15.5 | 688. |
| 17 | .360 | 155. | 15.5 | 688. |
| 18 | .360 | 155. | 15.5 | 689. |
| 19 | .370 | 159. | 15.4 | 688. |
| 20 | .370 | 159. | 15.5 | 689. |
| 21 | .370 | 159. | 15.4 | 689. |
| 22 | .360 | 155. | 15.3 | 664. |
| 23 | .330 | 142. | 15.0 | 583. |
| 24 | .300 | 129. | 14.9 | 520. |

DAY # 66

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 14.8 | 467. |
| 2 | .240 | 103. | 14.9 | 460. |
| 3 | .230 | 99. | 14.8 | 459. |
| 4 | .230 | 99. | 14.9 | 444. |
| 5 | .240 | 103. | 15.1 | 451. |
| 6 | .260 | 112. | 15.2 | 506. |
| 7 | .300 | 129. | 15.0 | 528. |
| 8 | .310 | 133. | 15.0 | 553. |
| 9 | .340 | 146. | 15.3 | 640. |
| 10 | .360 | 155. | 15.4 | 688. |
| 11 | .380 | 163. | 15.3 | 688. |
| 12 | .380 | 163. | 15.4 | 688. |
| 13 | .370 | 159. | 15.4 | 667. |
| 14 | .370 | 159. | 15.4 | 656. |
| 15 | .350 | 150. | 15.4 | 636. |
| 16 | .330 | 142. | 15.4 | 610. |
| 17 | .330 | 142. | 15.5 | 618. |
| 18 | .350 | 150. | 15.6 | 671. |
| 19 | .360 | 155. | 15.5 | 683. |
| 20 | .380 | 163. | 15.5 | 682. |
| 21 | .380 | 163. | 15.5 | 682. |
| 22 | .360 | 155. | 15.4 | 659. |
| 23 | .350 | 150. | 15.3 | 625. |
| 24 | .330 | 142. | 15.0 | 574. |

DAY # 67

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 15.1 | 590. |
| 2 | .320 | 137. | 14.9 | 552. |
| 3 | .320 | 137. | 14.9 | 549. |
| 4 | .310 | 133. | 14.8 | 538. |
| 5 | .310 | 133. | 14.9 | 559. |
| 6 | .310 | 133. | 15.0 | 567. |
| 7 | .320 | 137. | 14.9 | 571. |
| 8 | .320 | 137. | 15.0 | 590. |
| 9 | .330 | 142. | 15.1 | 634. |

| | | | | |
|---|---|---|---|---|
| 10 | .350 | 150. | 15.1 | 648. |
| 11 | .350 | 150. | 14.8 | 588. |
| 12 | .340 | 146. | 15.0 | 582. |
| 13 | .330 | 142. | 15.0 | 572. |
| 14 | .320 | 137. | 14.9 | 547. |
| 15 | .320 | 137. | 14.9 | 535. |
| 16 | .310 | 133. | 14.9 | 502. |
| 17 | .300 | 129. | 15.1 | 515. |
| 18 | .300 | 129. | 15.3 | 557. |
| 19 | .310 | 133. | 15.4 | 614. |
| 20 | .340 | 146. | 15.4 | 646. |
| 21 | .360 | 155. | 15.3 | 643. |
| 22 | .360 | 155. | 15.2 | 615. |
| 23 | .360 | 155. | 15.0 | 592. |
| 24 | .340 | 146. | 14.6 | 508. |

DAY = 68

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 14.8 | 467. |
| 2 | .270 | 116. | 14.8 | 459. |
| 3 | .250 | 107. | 14.9 | 434. |
| 4 | .250 | 107. | 15.0 | 452. |
| 5 | .260 | 112. | 15.1 | 468. |
| 6 | .310 | 133. | 15.1 | 542. |
| 7 | .350 | 150. | 15.2 | 628. |
| 8 | .380 | 163. | 15.3 | 676. |
| 9 | .380 | 163. | 15.2 | 679. |
| 10 | .380 | 163. | 15.2 | 685. |
| 11 | .390 | 168. | 15.2 | 688. |
| 12 | .390 | 168. | 15.2 | 686. |
| 13 | .400 | 172. | 15.2 | 688. |
| 14 | .390 | 168. | 15.3 | 690. |
| 15 | .400 | 172. | 15.4 | 693. |
| 16 | .400 | 172. | 15.4 | 695. |
| 17 | .390 | 168. | 15.4 | 693. |
| 18 | .380 | 163. | 15.3 | 671. |
| 19 | .380 | 163. | 15.4 | 664. |
| 20 | .380 | 163. | 15.3 | 662. |
| 21 | .390 | 168. | 15.4 | 684. |
| 22 | .390 | 168. | 15.3 | 665. |
| 23 | .360 | 155. | 15.0 | 610. |
| 24 | .300 | 129. | 14.6 | 510. |

DAY = 69

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 14.3 | 419. |
| 2 | .260 | 112. | 14.3 | 392. |
| 3 | .240 | 103. | 14.1 | 374. |
| 4 | .230 | 99. | 14.1 | 382. |
| 5 | .230 | 99. | 14.2 | 402. |
| 6 | .230 | 99. | 14.9 | 461. |
| 7 | .250 | 107. | 15.4 | 581. |
| 8 | .290 | 125. | 15.3 | 670. |

| | | | | |
|---|---|---|---|---|
| 9 | .340 | 146. | 15.2 | 688. |
| 10 | .370 | 159. | 15.2 | 682. |
| 11 | .370 | 159. | 15.3 | 690. |
| 12 | .370 | 159. | 15.4 | 691. |
| 13 | .370 | 159. | 15.3 | 688. |
| 14 | .360 | 155. | 15.3 | 682. |
| 15 | .360 | 155. | 15.4 | 679. |
| 16 | .360 | 155. | 15.4 | 690. |
| 17 | .360 | 155. | 15.4 | 691. |
| 18 | .360 | 155. | 15.6 | 689. |
| 19 | .360 | 155. | 15.4 | 668. |
| 20 | .350 | 150. | 15.5 | 666. |
| 21 | .350 | 150. | 15.6 | 675. |
| 22 | .340 | 146. | 15.6 | 672. |
| 23 | .330 | 142. | 15.5 | 621. |
| 24 | .300 | 129. | 15.2 | 531. |

DAY = 70

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 14.8 | 488. |
| 2 | .240 | 103. | 15.1 | 466. |
| 3 | .230 | 99. | 15.0 | 466. |
| 4 | .230 | 99. | 14.9 | 447. |
| 5 | .230 | 99. | 15.0 | 458. |
| 6 | .240 | 103. | 15.2 | 529. |
| 7 | .260 | 112. | 15.4 | 587. |
| 8 | .300 | 129. | 15.6 | 673. |
| 9 | .330 | 142. | 15.5 | 680. |
| 10 | =1.000 | =430. | =1.0 | =1. |
| 11 | .350 | 150. | 15.5 | 688. |
| 12 | .360 | 155. | 15.5 | 689. |
| 13 | .360 | 155. | 15.5 | 692. |
| 14 | .360 | 155. | 15.5 | 691. |
| 15 | .370 | 159. | 15.5 | 679. |
| 16 | .360 | 155. | 15.5 | 675. |
| 17 | .360 | 155. | 15.4 | 671. |
| 18 | .360 | 155. | 15.6 | 666. |
| 19 | .360 | 155. | 15.5 | 649. |
| 20 | .360 | 155. | 15.6 | 670. |
| 21 | .360 | 155. | 15.6 | 677. |
| 22 | .360 | 155. | 15.6 | 653. |
| 23 | .350 | 150. | 15.2 | 566. |
| 24 | .310 | 133. | 14.8 | 487. |

DAY = 71

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 14.9 | 458. |
| 2 | .250 | 107. | 15.1 | 488. |
| 3 | .250 | 107. | 15.0 | 485. |
| 4 | .250 | 107. | 15.0 | 488. |
| 5 | .250 | 107. | 15.1 | 499. |
| 6 | .270 | 116. | 15.1 | 528. |
| 7 | .290 | 125. | 15.4 | 582. |

| | | | | |
|---|---|---|---|---|
| 8 | .320 | 137. | 15.5 | 645. |
| 9 | .340 | 146. | 15.4 | 663. |
| 10 | .330 | 142. | 15.5 | 643. |
| 11 | .340 | 146. | 15.8 | 684. |
| 12 | .350 | 150. | 15.8 | 692. |
| 13 | .350 | 150. | 15.8 | 689. |
| 14 | .350 | 150. | 15.9 | 686. |
| 15 | .340 | 146. | 15.8 | 661. |
| 16 | .340 | 146. | 15.8 | 650. |
| 17 | .350 | 150. | 15.9 | 676. |
| 18 | .360 | 155. | 15.8 | 675. |
| 19 | .370 | 159. | 15.9 | 671. |
| 20 | .360 | 155. | 16.0 | 668. |
| 21 | .360 | 155. | 16.0 | 665. |
| 22 | .320 | 137. | 15.8 | 598. |
| 23 | .270 | 116. | 15.2 | 494. |
| 24 | .240 | 103. | 15.1 | 458. |

DAY = 72

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 15.3 | 421. |
| 2 | .230 | 99. | 15.5 | 454. |
| 3 | .210 | 90. | 15.3 | 414. |
| 4 | .200 | 86. | 15.2 | 399. |
| 5 | .210 | 90. | 15.3 | 416. |
| 6 | .230 | 99. | 15.6 | 484. |
| 7 | .260 | 112. | 15.6 | 553. |
| 8 | .320 | 137. | 15.9 | 655. |
| 9 | .340 | 146. | 15.6 | 661. |
| 10 | .340 | 146. | 15.5 | 650. |
| 11 | .350 | 150. | 15.7 | 675. |
| 12 | .350 | 150. | 15.6 | 673. |
| 13 | .350 | 150. | 15.5 | 653. |
| 14 | .350 | 150. | 15.6 | 658. |
| 15 | .340 | 146. | 15.6 | 636. |
| 16 | .360 | 155. | 15.8 | 666. |
| 17 | .370 | 159. | 15.6 | 676. |
| 18 | .360 | 155. | 15.6 | 660. |
| 19 | .370 | 159. | 15.8 | 670. |
| 20 | .370 | 159. | 15.7 | 674. |
| 21 | .370 | 159. | 15.7 | 655. |
| 22 | .360 | 155. | 15.6 | 626. |
| 23 | .320 | 137. | 15.2 | 569. |
| 24 | .260 | 112. | 14.9 | 499. |

DAY = 73

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 14.8 | 474. |
| 2 | .250 | 107. | 14.8 | 473. |
| 3 | .260 | 112. | 14.9 | 478. |
| 4 | .240 | 103. | 14.8 | 438. |
| 5 | .240 | 103. | 15.1 | 458. |
| 6 | .250 | 107. | 15.1 | 492. |

| | | | | |
|---|---|---|---|---|
| 7 | .250 | 107. | 15.1 | 484. |
| 8 | .280 | 120. | 15.4 | 566. |
| 9 | .340 | 146. | 15.5 | 625. |
| 10 | .370 | 159. | 15.6 | 669. |
| 11 | .370 | 159. | 15.7 | 671. |
| 12 | .370 | 159. | 15.6 | 667. |
| 13 | .360 | 155. | 15.5 | 653. |
| 14 | .360 | 155. | 15.6 | 647. |
| 15 | .340 | 146. | 15.5 | 619. |
| 16 | .320 | 137. | 15.3 | 579. |
| 17 | .310 | 133. | 15.6 | 597. |
| 18 | .340 | 146. | 15.6 | 630. |
| 19 | .370 | 159. | 15.8 | 675. |
| 20 | .380 | 163. | 15.7 | 676. |
| 21 | .380 | 163. | 15.7 | 668. |
| 22 | .380 | 163. | 15.6 | 652. |
| 23 | .330 | 142. | 15.5 | 583. |
| 24 | .270 | 116. | 15.1 | 500. |

DAY # 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 14.5 | 383. |
| 2 | .230 | 99. | 15.1 | 397. |
| 3 | .200 | 86. | 15.0 | 398. |
| 4 | .200 | 86. | 14.9 | 373. |
| 5 | .190 | 82. | 14.8 | 388. |
| 6 | .190 | 82. | 14.8 | 352. |
| 7 | .180 | 77. | 15.3 | 426. |
| 8 | .190 | 82. | 15.3 | 420. |
| 9 | .210 | 90. | 15.4 | 470. |
| 10 | .230 | 99. | 15.6 | 556. |
| 11 | .260 | 112. | 15.5 | 591. |
| 12 | .280 | 120. | 15.5 | 602. |
| 13 | .290 | 125. | 15.5 | 622. |
| 14 | .300 | 129. | 15.4 | 609. |
| 15 | .300 | 129. | 15.4 | 597. |
| 16 | .300 | 129. | 15.5 | 596. |
| 17 | .300 | 129. | 15.5 | 581. |
| 18 | .310 | 133. | 15.6 | 604. |
| 19 | .310 | 133. | 15.9 | 617. |
| 20 | .330 | 142. | 15.7 | 671. |
| 21 | .350 | 150. | 15.6 | 669. |
| 22 | .360 | 155. | 15.5 | 641. |
| 23 | .350 | 150. | 15.3 | 551. |
| 24 | .320 | 137. | 15.2 | 495. |

DAY # 75

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.2 | 456. |
| 2 | .280 | 120. | 15.3 | 490. |
| 3 | .280 | 120. | 15.2 | 487. |
| 4 | .290 | 125. | 15.3 | 489. |
| 5 | .290 | 125. | 15.2 | 506. |

| | | | | |
|---|---|---|---|---|
| 6 | .330 | 142. | 15.5 | 600. |
| 7 | .370 | 159. | 15.3 | 651. |
| 8 | .390 | 168. | 15.4 | 677. |
| 9 | .390 | 168. | 15.5 | 685. |
| 10 | .390 | 168. | 15.5 | 695. |
| 11 | .390 | 168. | 15.5 | 697. |
| 12 | .390 | 168. | 15.4 | 691. |
| 13 | .390 | 168. | 15.4 | 688. |
| 14 | .390 | 168. | 15.4 | 688. |
| 15 | .390 | 168. | 15.3 | 669. |
| 16 | .400 | 172. | 15.4 | 681. |
| 17 | .380 | 163. | 15.4 | 657. |
| 18 | .370 | 159. | 15.5 | 657. |
| 19 | .380 | 163. | 15.6 | 673. |
| 20 | .390 | 168. | 15.6 | 677. |
| 21 | .370 | 159. | 15.7 | 668. |
| 22 | .360 | 155. | 15.6 | 647. |
| 23 | .330 | 142. | 15.4 | 587. |
| 24 | .300 | 129. | 15.3 | 526. |

DAY # 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.3 | 501. |
| 2 | .270 | 116. | 15.3 | 501. |
| 3 | .250 | 107. | 15.3 | 478. |
| 4 | .250 | 107. | 15.3 | 469. |
| 5 | .250 | 107. | 15.4 | 482. |
| 6 | .300 | 129. | 15.6 | 577. |
| 7 | .350 | 150. | 15.7 | 643. |
| 8 | .370 | 159. | 15.7 | 683. |
| 9 | .350 | 150. | 15.7 | 680. |
| 10 | .360 | 155. | 15.8 | 694. |
| 11 | .370 | 159. | 16.0 | 703. |
| 12 | .370 | 159. | 16.0 | 704. |
| 13 | .380 | 163. | 16.0 | 702. |
| 14 | .370 | 159. | 16.0 | 698. |
| 15 | .370 | 159. | 16.1 | 699. |
| 16 | .370 | 159. | 16.2 | 704. |
| 17 | .370 | 159. | 16.2 | 697. |
| 18 | .370 | 159. | 16.1 | 676. |
| 19 | .380 | 163. | 16.2 | 698. |
| 20 | .380 | 163. | 16.2 | 701. |
| 21 | .370 | 159. | 16.1 | 692. |
| 22 | .370 | 159. | 15.9 | 670. |
| 23 | .350 | 150. | 15.8 | 643. |
| 24 | .320 | 137. | 15.7 | 596. |

DAY # 77

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 15.6 | 558. |
| 2 | .260 | 112. | 15.5 | 502. |
| 3 | .250 | 107. | 15.7 | 510. |
| 4 | .240 | 103. | 15.3 | 467. |

| | | | | |
|---|---|---|---|---|
| 5 | .250 | 107. | 15.5 | 487. |
| 6 | .270 | 116. | 15.6 | 531. |
| 7 | .350 | 150. | 15.6 | 647. |
| 8 | .370 | 159. | 15.8 | 686. |
| 9 | .370 | 159. | 15.7 | 700. |
| 10 | .380 | 163. | 15.8 | 695. |
| 11 | .380 | 163. | 15.7 | 697. |
| 12 | .390 | 168. | 15.4 | 700. |
| 13 | .400 | 172. | 15.5 | 700. |
| 14 | .400 | 172. | 15.5 | 700. |
| 15 | .400 | 172. | 15.5 | 699. |
| 16 | .400 | 172. | 15.5 | 700. |
| 17 | .400 | 172. | 15.6 | 699. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .410 | 176. | 15.6 | 706. |
| 21 | .410 | 176. | 15.6 | 709. |
| 22 | .400 | 172. | 15.4 | 690. |
| 23 | .370 | 159. | 15.2 | 639. |
| 24 | .320 | 137. | 15.1 | 559. |

DAY # 78

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 15.3 | 573. |
| 2 | .320 | 137. | 15.1 | 559. |
| 3 | .310 | 133. | 15.1 | 543. |
| 4 | .300 | 129. | 15.1 | 540. |
| 5 | .310 | 133. | 15.2 | 554. |
| 6 | .330 | 142. | 15.4 | 605. |
| 7 | .370 | 159. | 15.5 | 681. |
| 8 | .390 | 168. | 15.4 | 689. |
| 9 | .400 | 172. | 15.4 | 693. |
| 10 | .400 | 172. | 15.4 | 703. |
| 11 | .380 | 163. | 15.4 | 702. |
| 12 | .380 | 163. | 15.5 | 702. |
| 13 | .380 | 163. | 14.8 | 703. |
| 14 | .370 | 159. | 15.5 | 702. |
| 15 | .340 | 146. | 15.4 | 689. |
| 16 | .340 | 146. | 15.6 | 694. |
| 17 | .350 | 150. | 15.6 | 687. |
| 18 | .350 | 150. | 15.7 | 682. |
| 19 | .360 | 155. | 15.6 | 681. |
| 20 | .370 | 159. | 15.7 | 699. |
| 21 | .370 | 159. | 15.7 | 691. |
| 22 | .370 | 159. | 15.6 | 688. |
| 23 | .340 | 146. | 15.4 | 625. |
| 24 | .250 | 107. | 14.9 | 477. |

DAY # 79

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 15.2 | 439. |
| 2 | .210 | 90. | 15.2 | 433. |
| 3 | .200 | 86. | 15.2 | 422. |

| | | | | |
|---|---|---|---|---|
| 4 | .200 | 86. | 15.2 | 431. |
| 5 | .210 | 90. | 15.3 | 445. |
| 6 | .250 | 107. | 15.5 | 531. |
| 7 | .320 | 137. | 15.6 | 636. |
| 8 | .350 | 150. | 15.5 | 677. |
| 9 | .360 | 155. | 15.5 | 693. |
| 10 | .360 | 155. | 15.3 | 677. |
| 11 | .360 | 155. | 15.3 | 686. |
| 12 | .350 | 150. | 15.4 | 683. |
| 13 | .330 | 142. | 15.4 | 658. |
| 14 | .340 | 146. | 15.5 | 674. |
| 15 | .340 | 146. | 15.4 | 679. |
| 16 | .340 | 146. | 15.4 | 669. |
| 17 | .340 | 146. | 15.3 | 664. |
| 18 | .350 | 150. | 15.4 | 674. |
| 19 | .360 | 155. | 15.4 | 683. |
| 20 | .350 | 150. | 15.4 | 671. |
| 21 | .340 | 146. | 15.5 | 669. |
| 22 | .350 | 150. | 15.4 | 666. |
| 23 | .330 | 142. | 15.5 | 644. |
| 24 | .300 | 129. | 15.1 | 563. |

DAY # 80

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 14.8 | 445. |
| 2 | .220 | 95. | 15.0 | 414. |
| 3 | .210 | 90. | 15.2 | 413. |
| 4 | .200 | 86. | 15.2 | 417. |
| 5 | .220 | 95. | 15.4 | 479. |
| 6 | .290 | 125. | 15.5 | 581. |
| 7 | .310 | 133. | 15.6 | 618. |
| 8 | .320 | 137. | 15.7 | 644. |
| 9 | .340 | 146. | 15.7 | 697. |
| 10 | .350 | 150. | 15.6 | 700. |
| 11 | .350 | 150. | 15.7 | 700. |
| 12 | .360 | 155. | 15.5 | 698. |
| 13 | .350 | 150. | 15.4 | 682. |
| 14 | .360 | 155. | 15.4 | 683. |
| 15 | .350 | 150. | 15.4 | 678. |
| 16 | .350 | 150. | 15.4 | 688. |
| 17 | .350 | 150. | 15.5 | 695. |
| 18 | .360 | 155. | 15.5 | 699. |
| 19 | .360 | 155. | 15.4 | 692. |
| 20 | .370 | 159. | 15.3 | 681. |
| 21 | .370 | 159. | 15.4 | 681. |
| 22 | .360 | 155. | 15.4 | 681. |
| 23 | .360 | 155. | 15.2 | 663. |
| 24 | .350 | 150. | 15.3 | 666. |

DAY # 81

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 15.3 | 625. |
| 2 | .330 | 142. | 15.4 | 613. |

| | | | | |
|---|---|---|---|---|
| 3 | .290 | 125. | 15.1 | 554. |
| 4 | .280 | 120. | 15.2 | 533. |
| 5 | .270 | 116. | 15.2 | 534. |
| 6 | .270 | 116. | 15.3 | 547. |
| 7 | .270 | 116. | 15.2 | 523. |
| 8 | .270 | 116. | 15.4 | 548. |
| 9 | .300 | 129. | 15.4 | 596. |
| 10 | .300 | 129. | 15.3 | 589. |
| 11 | .320 | 137. | 15.4 | 605. |
| 12 | .300 | 129. | 15.4 | 599. |
| 13 | .280 | 120. | 15.3 | 584. |
| 14 | .270 | 116. | 15.2 | 563. |
| 15 | .260 | 112. | 15.2 | 538. |
| 16 | .260 | 112. | 15.1 | 526. |
| 17 | .260 | 112. | 15.2 | 531. |
| 18 | .300 | 129. | 15.6 | 585. |
| 19 | .350 | 150. | 15.8 | 666. |
| 20 | .370 | 159. | 15.7 | 698. |
| 21 | .360 | 155. | 15.8 | 684. |
| 22 | .350 | 150. | 15.7 | 659. |
| 23 | .310 | 133. | 15.4 | 586. |
| 24 | .280 | 120. | 15.3 | 503. |

DAY = 82

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 15.0 | 415. |
| 2 | .230 | 99. | 15.0 | 398. |
| 3 | .230 | 99. | 15.1 | 415. |
| 4 | .270 | 116. | 15.1 | 451. |
| 5 | .270 | 116. | 15.1 | 454. |
| 6 | .330 | 142. | 15.3 | 560. |
| 7 | .370 | 159. | 15.3 | 625. |
| 8 | .390 | 168. | 15.4 | 673. |
| 9 | .390 | 168. | 15.4 | 687. |
| 10 | .380 | 163. | 15.5 | 685. |
| 11 | .380 | 163. | 15.4 | 692. |
| 12 | .390 | 168. | 15.2 | 662. |
| 13 | .390 | 168. | 15.2 | 647. |
| 14 | .400 | 172. | 15.4 | 677. |
| 15 | .390 | 168. | 15.4 | 668. |
| 16 | .390 | 168. | 15.4 | 664. |
| 17 | .390 | 168. | 15.3 | 649. |
| 18 | .390 | 168. | 15.4 | 651. |
| 19 | .390 | 168. | 15.5 | 666. |
| 20 | .400 | 172. | 15.4 | 665. |
| 21 | .390 | 168. | 15.5 | 660. |
| 22 | .370 | 159. | 15.5 | 631. |
| 23 | .360 | 155. | 15.5 | 608. |
| 24 | .300 | 129. | 15.1 | 495. |

DAY = 83

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.0 | 418. |

| | | | | |
|---|---|---|---|---|
| 2 | .240 | 103. | 15.1 | 395. |
| 3 | .230 | 99. | 15.2 | 389. |
| 4 | .230 | 99. | 15.0 | 360. |
| 5 | .230 | 99. | 15.3 | 400. |
| 6 | .270 | 116. | 15.5 | 497. |
| 7 | .340 | 146. | 15.5 | 588. |
| 8 | .380 | 163. | 15.6 | 664. |
| 9 | .380 | 163. | 15.4 | 672. |
| 10 | .380 | 163. | 15.4 | 661. |
| 11 | .360 | 155. | 15.4 | 647. |
| 12 | .360 | 155. | 15.5 | 651. |
| 13 | .360 | 155. | 15.5 | 630. |
| 14 | .370 | 159. | 15.6 | 654. |
| 15 | .370 | 159. | 15.6 | 641. |
| 16 | .360 | 155. | 15.6 | 644. |
| 17 | .320 | 137. | 15.9 | 645. |
| 18 | .320 | 137. | 15.9 | 647. |
| 19 | .330 | 142. | 16.0 | 656. |
| 20 | .340 | 146. | 16.1 | 678. |
| 21 | .340 | 146. | 15.8 | 661. |
| 22 | .350 | 150. | 15.5 | 628. |
| 23 | .330 | 142. | 15.8 | 612. |
| 24 | .290 | 125. | 16.0 | 559. |

DAY # 84

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.8 | 520. |
| 2 | .260 | 112. | 15.7 | 497. |
| 3 | .260 | 112. | 15.8 | 505. |
| 4 | .270 | 116. | 15.7 | 502. |
| 5 | .280 | 120. | 15.8 | 529. |
| 6 | .290 | 125. | 16.0 | 576. |
| 7 | .300 | 129. | 16.1 | 609. |
| 8 | .320 | 137. | 16.4 | 665. |
| 9 | .340 | 146. | 16.2 | 680. |
| 10 | .330 | 142. | 16.4 | 676. |
| 11 | .320 | 137. | 16.4 | 677. |
| 12 | .340 | 146. | 16.3 | 677. |
| 13 | .350 | 150. | 16.2 | 672. |
| 14 | .350 | 150. | 16.2 | 665. |
| 15 | .360 | 155. | 15.9 | 641. |
| 16 | .360 | 155. | 15.9 | 645. |
| 17 | .360 | 155. | 16.0 | 646. |
| 18 | .380 | 163. | 16.1 | 675. |
| 19 | .380 | 163. | 16.2 | 679. |
| 20 | .380 | 163. | 16.2 | 678. |
| 21 | .370 | 159. | 16.3 | 663. |
| 22 | .350 | 150. | 16.2 | 636. |
| 23 | .330 | 142. | 16.1 | 601. |
| 24 | .300 | 129. | 16.0 | 526. |

DAY # 85

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .250 | 107. | 15.8 | 457. |
| 2 | .230 | 99. | 16.0 | 435. |
| 3 | .230 | 99. | 16.2 | 452. |
| 4 | .230 | 99. | 16.0 | 447. |
| 5 | .230 | 99. | 15.9 | 434. |
| 6 | .250 | 107. | 16.2 | 491. |
| 7 | .300 | 129. | 16.6 | 604. |
| 8 | .340 | 146. | 16.5 | 662. |
| 9 | .360 | 155. | 16.3 | 678. |
| 10 | .350 | 150. | 16.3 | 678. |
| 11 | .350 | 150. | 16.4 | 684. |
| 12 | .360 | 155. | 16.3 | 693. |
| 13 | .370 | 159. | 16.3 | 689. |
| 14 | .360 | 155. | 16.5 | 693. |
| 15 | .360 | 155. | 16.7 | 697. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | .380 | 163. | 16.6 | 688. |
| 20 | .380 | 163. | 16.7 | 680. |
| 21 | .380 | 163. | 16.6 | 676. |
| 22 | .380 | 163. | 16.2 | 654. |
| 23 | .350 | 150. | 16.2 | 629. |
| 24 | .310 | 133. | 15.6 | 520. |

DAY = 86

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.9 | 448. |
| 2 | .250 | 107. | 15.8 | 414. |
| 3 | .240 | 103. | 15.8 | 394. |
| 4 | .230 | 99. | 15.6 | 370. |
| 5 | .220 | 95. | 15.9 | 379. |
| 6 | .230 | 99. | 16.1 | 436. |
| 7 | .290 | 125. | 16.5 | 588. |
| 8 | .340 | 146. | 16.5 | 669. |
| 9 | .360 | 155. | 16.3 | 688. |
| 10 | .350 | 150. | 16.2 | 681. |
| 11 | .360 | 155. | 16.3 | 692. |
| 12 | .360 | 155. | 16.3 | 693. |
| 13 | .360 | 155. | 16.4 | 695. |
| 14 | .360 | 155. | 16.3 | 686. |
| 15 | .360 | 155. | 16.2 | 684. |
| 16 | .360 | 155. | 16.3 | 679. |
| 17 | .330 | 142. | 16.4 | 683. |
| 18 | .320 | 137. | 16.4 | 651. |
| 19 | .320 | 137. | 16.5 | 670. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .340 | 146. | 16.1 | 684. |
| 22 | .340 | 146. | 16.3 | 676. |
| 23 | .340 | 146. | 16.3 | 665. |
| 24 | .310 | 133. | 16.2 | 605. |

DAY = 87

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .290 | 125. | 16.2 | 574. |
| 2 | .280 | 120. | 16.3 | 561. |
| 3 | .270 | 116. | 16.3 | 553. |
| 4 | .270 | 116. | 16.2 | 535. |
| 5 | .250 | 107. | 16.1 | 507. |
| 6 | .240 | 103. | 16.4 | 500. |
| 7 | .230 | 99. | 16.4 | 483. |
| 8 | .240 | 103. | 16.8 | 529. |
| 9 | .290 | 125. | 16.9 | 611. |
| 10 | .310 | 133. | 16.8 | 644. |
| 11 | .300 | 129. | 16.9 | 643. |
| 12 | .300 | 129. | 16.9 | 640. |
| 13 | .300 | 129. | 16.8 | 625. |
| 14 | .300 | 129. | 16.9 | 629. |
| 15 | .300 | 129. | 16.9 | 619. |
| 16 | .300 | 129. | 17.0 | 622. |
| 17 | .300 | 129. | 16.9 | 623. |
| 18 | .300 | 129. | 16.8 | 630. |
| 19 | .300 | 129. | 16.9 | 640. |
| 20 | .300 | 129. | 16.8 | 638. |
| 21 | .300 | 129. | 16.7 | 645. |
| 22 | .300 | 129. | 16.7 | 639. |
| 23 | .310 | 133. | 16.4 | 597. |
| 24 | .290 | 125. | 16.2 | 513. |

DAY = 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 16.4 | 505. |
| 2 | .310 | 133. | 16.1 | 517. |
| 3 | .290 | 125. | 15.8 | 466. |
| 4 | .260 | 112. | 15.7 | 410. |
| 5 | .260 | 112. | 15.7 | 413. |
| 6 | .270 | 116. | 15.6 | 418. |
| 7 | .270 | 116. | 15.5 | 421. |
| 8 | .280 | 120. | 15.8 | 469. |
| 9 | .280 | 120. | 16.1 | 542. |
| 10 | .300 | 129. | 16.0 | 565. |
| 11 | .310 | 133. | 16.1 | 592. |
| 12 | .320 | 137. | 16.0 | 593. |
| 13 | .320 | 137. | 15.9 | 581. |
| 14 | .320 | 137. | 16.0 | 598. |
| 15 | .310 | 133. | 15.8 | 570. |
| 16 | .310 | 133. | 15.9 | 581. |
| 17 | .310 | 133. | 16.0 | 587. |
| 18 | .330 | 142. | 16.0 | 623. |
| 19 | .330 | 142. | 15.9 | 615. |
| 20 | .340 | 146. | 16.0 | 644. |
| 21 | .360 | 155. | 15.9 | 648. |
| 22 | .360 | 155. | 15.8 | 650. |
| 23 | .330 | 142. | 15.8 | 596. |
| 24 | .300 | 129. | 15.7 | 532. |

DAY = 89

| | NOX | NOX | CO2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.8 | 524. |
| 2 | .270 | 116. | 15.8 | 516. |
| 3 | .250 | 107. | 15.7 | 494. |
| 4 | .240 | 103. | 15.6 | 470. |
| 5 | .250 | 107. | 15.9 | 510. |
| 6 | .270 | 116. | 16.0 | 546. |
| 7 | .280 | 120. | 16.2 | 600. |
| 8 | .310 | 133. | 16.2 | 643. |
| 9 | .330 | 142. | 16.4 | 689. |
| 10 | .330 | 142. | 16.4 | 699. |
| 11 | .330 | 142. | 16.4 | 698. |
| 12 | .340 | 146. | 16.4 | 703. |
| 13 | .340 | 146. | 16.3 | 691. |
| 14 | .350 | 150. | 16.3 | 685. |
| 15 | .340 | 146. | 16.3 | 685. |
| 16 | .330 | 142. | 16.3 | 676. |
| 17 | .330 | 142. | 16.3 | 653. |
| 18 | .330 | 142. | 16.4 | 657. |
| 19 | .340 | 146. | 16.4 | 662. |
| 20 | .340 | 146. | 16.4 | 658. |
| 21 | .340 | 146. | 16.4 | 652. |
| 22 | .340 | 146. | 16.4 | 650. |
| 23 | .310 | 133. | 16.2 | 596. |
| 24 | .270 | 116. | 16.0 | 507. |

DAY = 90



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 16.2 | 508. |
| 2 | .240 | 103. | 16.1 | 523. |
| 3 | .240 | 103. | 16.1 | 521. |
| 4 | .240 | 103. | 16.0 | 505. |
| 5 | .230 | 99. | 15.8 | 493. |
| 6 | .250 | 107. | 15.9 | 526. |
| 7 | .250 | 107. | 15.9 | 535. |
| 8 | .270 | 116. | 16.1 | 573. |
| 9 | .310 | 133. | 16.3 | 653. |
| 10 | .320 | 137. | 16.2 | 673. |
| 11 | .320 | 137. | 16.0 | 650. |
| 12 | .320 | 137. | 16.2 | 661. |
| 13 | .310 | 133. | 16.1 | 644. |
| 14 | .320 | 137. | 16.2 | 649. |
| 15 | .320 | 137. | 16.1 | 647. |
| 16 | .320 | 137. | 16.2 | 647. |
| 17 | .320 | 137. | 16.1 | 643. |
| 18 | .320 | 137. | 16.2 | 646. |
| 19 | .320 | 137. | 16.1 | 635. |
| 20 | .320 | 137. | 16.2 | 652. |
| 21 | .320 | 137. | 16.0 | 644. |
| 22 | .310 | 133. | 15.9 | 621. |
| 23 | .290 | 125. | 15.8 | 575. |
| 24 | .270 | 116. | 15.7 | 525. |

DAY = 91

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 15.7 | 479. |
| 2 | .240 | 103. | 15.8 | 489. |
| 3 | .240 | 103. | 15.8 | 488. |
| 4 | .240 | 103. | 15.7 | 474. |
| 5 | .240 | 103. | 15.8 | 486. |
| 6 | .260 | 112. | 15.9 | 544. |
| 7 | .260 | 112. | 15.8 | 535. |
| 8 | .290 | 125. | 16.1 | 621. |
| 9 | .320 | 137. | 15.9 | 661. |
| 10 | .310 | 133. | 15.2 | 587. |
| 11 | .280 | 120. | 15.2 | 574. |
| 12 | .320 | 137. | 13.0 | 567. |
| 13 | .330 | 142. | 12.2 | 555. |
| 14 | .300 | 129. | 14.4 | 578. |
| 15 | .320 | 137. | 15.3 | 630. |
| 16 | .320 | 137. | 15.4 | 649. |
| 17 | .320 | 137. | 15.2 | 642. |
| 18 | .310 | 133. | 15.4 | 627. |
| 19 | .320 | 137. | 15.7 | 650. |
| 20 | .340 | 146. | 15.7 | 684. |
| 21 | .340 | 146. | 15.7 | 683. |
| 22 | .340 | 146. | 15.6 | 665. |
| 23 | .300 | 129. | 15.6 | 592. |
| 24 | .260 | 112. | 15.3 | 509. |

DAY = 92



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 15.6 | 487. |
| 2 | .270 | 116. | 15.7 | 513. |
| 3 | .260 | 112. | 15.6 | 517. |
| 4 | .240 | 103. | 15.7 | 499. |
| 5 | .260 | 112. | 15.6 | 511. |
| 6 | .270 | 116. | 15.7 | 552. |
| 7 | .300 | 129. | 15.8 | 592. |
| 8 | .320 | 137. | 15.8 | 639. |
| 9 | .340 | 146. | 15.7 | 665. |
| 10 | .340 | 146. | 15.9 | 674. |
| 11 | .330 | 142. | 15.8 | 667. |
| 12 | .330 | 142. | 15.9 | 663. |
| 13 | .320 | 137. | 16.0 | 666. |
| 14 | .330 | 142. | 15.9 | 671. |
| 15 | .330 | 142. | 15.9 | 666. |
| 16 | .330 | 142. | 15.9 | 664. |
| 17 | .320 | 137. | 16.1 | 635. |
| 18 | .290 | 125. | 16.5 | 604. |
| 19 | .300 | 129. | 16.7 | 614. |
| 20 | .320 | 137. | 16.6 | 663. |
| 21 | .310 | 133. | 16.9 | 644. |
| 22 | .280 | 120. | 16.8 | 582. |
| 23 | .260 | 112. | 16.4 | 509. |
| 24 | .250 | 107. | 16.4 | 483. |

DAY = 93

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 16.5 | 515. |
| 2 | .230 | 99. | 16.2 | 459. |
| 3 | .230 | 99. | 16.2 | 448. |
| 4 | .230 | 99. | 16.3 | 456. |
| 5 | .230 | 99. | 16.2 | 455. |
| 6 | .230 | 99. | 16.2 | 470. |
| 7 | .240 | 103. | 16.3 | 512. |
| 8 | .280 | 120. | 16.9 | 622. |
| 9 | .300 | 129. | 16.9 | 669. |
| 10 | .300 | 129. | 16.8 | 680. |
| 11 | .310 | 133. | 16.7 | 672. |
| 12 | .290 | 125. | 16.9 | 682. |
| 13 | .300 | 129. | 16.8 | 665. |
| 14 | .290 | 125. | 17.0 | 678. |
| 15 | .290 | 125. | 17.0 | 670. |
| 16 | .300 | 129. | 16.9 | 671. |
| 17 | .300 | 129. | 16.7 | 672. |
| 18 | .310 | 133. | 16.3 | 658. |
| 19 | .310 | 133. | 16.1 | 642. |
| 20 | .320 | 137. | 16.1 | 652. |
| 21 | .320 | 137. | 16.1 | 665. |
| 22 | .320 | 137. | 16.1 | 675. |
| 23 | .300 | 129. | 15.8 | 617. |
| 24 | .240 | 103. | 15.6 | 471. |

DAY # 94



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 16.0 | 474. |
| 2 | .230 | 99. | 15.8 | 462. |
| 3 | .210 | 90. | 15.6 | 448. |
| 4 | .180 | 77. | 15.6 | 426. |
| 5 | .190 | 82. | 16.0 | 455. |
| 6 | .210 | 90. | 16.0 | 479. |
| 7 | .230 | 99. | 16.0 | 496. |
| 8 | .240 | 103. | 16.1 | 520. |
| 9 | .270 | 116. | 16.2 | 602. |
| 10 | .310 | 133. | 16.2 | 657. |
| 11 | .320 | 137. | 16.0 | 686. |
| 12 | .330 | 142. | 15.9 | 690. |
| 13 | .320 | 137. | 16.0 | 688. |
| 14 | .320 | 137. | 15.9 | 670. |
| 15 | .320 | 137. | 15.9 | 672. |
| 16 | .310 | 133. | 16.0 | 663. |
| 17 | .310 | 133. | 16.0 | 669. |
| 18 | .330 | 142. | 16.2 | 690. |
| 19 | .320 | 137. | 16.0 | 682. |
| 20 | .330 | 142. | 16.1 | 693. |
| 21 | .320 | 137. | 16.0 | 672. |
| 22 | .320 | 137. | 16.0 | 666. |
| 23 | .290 | 125. | 16.0 | 619. |
| 24 | .280 | 120. | 16.0 | 617. |

DAY # 95

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 16.0 | 635. |
| 2 | .330 | 142. | 16.0 | 654. |
| 3 | .310 | 133. | 15.9 | 639. |
| 4 | .310 | 133. | 15.8 | 627. |
| 5 | .310 | 133. | 15.8 | 620. |
| 6 | .290 | 125. | 16.0 | 609. |
| 7 | .290 | 125. | 15.9 | 597. |
| 8 | .290 | 125. | 15.7 | 594. |
| 9 | .300 | 129. | 15.8 | 610. |
| 10 | .310 | 133. | 15.9 | 645. |
| 11 | .300 | 129. | 16.0 | 637. |
| 12 | .310 | 133. | 16.1 | 659. |
| 13 | .320 | 137. | 15.8 | 645. |
| 14 | .280 | 120. | 15.8 | 590. |
| 15 | .260 | 112. | 15.9 | 575. |
| 16 | .260 | 112. | 15.8 | 560. |
| 17 | .270 | 116. | 15.9 | 577. |
| 18 | .300 | 129. | 16.0 | 616. |
| 19 | .320 | 137. | 15.9 | 620. |
| 20 | .340 | 146. | 15.8 | 640. |
| 21 | .330 | 142. | 16.0 | 640. |
| 22 | .320 | 137. | 16.1 | 639. |
| 23 | .310 | 133. | 16.2 | 619. |
| 24 | .270 | 116. | 15.9 | 559. |

DAY = 96



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 16.2 | 576. |
| 2 | .270 | 116. | 16.1 | 575. |
| 3 | .290 | 125. | 16.1 | 604. |
| 4 | .300 | 129. | 16.0 | 612. |
| 5 | .290 | 125. | 16.2 | 615. |
| 6 | .300 | 129. | 16.1 | 624. |
| 7 | .290 | 125. | 16.1 | 622. |
| 8 | .300 | 129. | 16.2 | 645. |
| 9 | .310 | 133. | 16.0 | 647. |
| 10 | .330 | 142. | 16.0 | 662. |
| 11 | .330 | 142. | 16.2 | 681. |
| 12 | .340 | 146. | 16.2 | 702. |
| 13 | .330 | 142. | 16.2 | 693. |
| 14 | .330 | 142. | 16.1 | 675. |
| 15 | .310 | 133. | 16.1 | 645. |
| 16 | .320 | 137. | 16.2 | 659. |
| 17 | .310 | 133. | 15.9 | 615. |
| 18 | .320 | 137. | 16.4 | 658. |
| 19 | .320 | 137. | 16.4 | 667. |
| 20 | *1.000 | *430. | *1.0 | *1. |
| 21 | .330 | 142. | 16.4 | 669. |
| 22 | .310 | 133. | 16.1 | 600. |
| 23 | .270 | 116. | 16.2 | 540. |
| 24 | .240 | 103. | 15.9 | 484. |

DAY = 97

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 16.3 | 506. |
| 2 | .220 | 95. | 16.3 | 516. |
| 3 | .240 | 103. | 16.4 | 549. |
| 4 | .260 | 112. | 16.3 | 552. |
| 5 | .260 | 112. | 16.4 | 563. |
| 6 | .300 | 129. | 16.1 | 590. |
| 7 | .300 | 129. | 16.4 | 642. |
| 8 | .300 | 129. | 16.4 | 642. |
| 9 | .290 | 125. | 16.2 | 601. |
| 10 | .310 | 133. | 16.4 | 661. |
| 11 | .310 | 133. | 16.4 | 677. |
| 12 | .310 | 133. | 16.5 | 687. |
| 13 | .310 | 133. | 16.4 | 666. |
| 14 | .330 | 142. | 16.4 | 675. |
| 15 | .330 | 142. | 16.4 | 670. |
| 16 | .300 | 129. | 16.5 | 641. |
| 17 | .310 | 133. | 16.7 | 664. |
| 18 | .320 | 137. | 16.5 | 675. |
| 19 | .320 | 137. | 16.6 | 672. |
| 20 | .320 | 137. | 16.7 | 675. |
| 21 | .320 | 137. | 16.7 | 669. |
| 22 | .330 | 142. | 16.5 | 647. |
| 23 | .290 | 125. | 16.1 | 571. |
| 24 | .260 | 112. | 16.2 | 519. |

DAY = 98



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.9 | 495. |
| 2 | .270 | 116. | 16.0 | 515. |
| 3 | .270 | 116. | 15.8 | 508. |
| 4 | .270 | 116. | 15.6 | 485. |
| 5 | .260 | 112. | 15.5 | 474. |
| 6 | .260 | 112. | 15.8 | 500. |
| 7 | .260 | 112. | 16.2 | 587. |
| 8 | .280 | 120. | 16.4 | 669. |
| 9 | .290 | 125. | 16.3 | 658. |
| 10 | .300 | 129. | 16.2 | 667. |
| 11 | .310 | 133. | 16.1 | 687. |
| 12 | .310 | 133. | 16.2 | 659. |
| 13 | .300 | 129. | 16.2 | 644. |
| 14 | .300 | 129. | 16.1 | 664. |
| 15 | .310 | 133. | 16.0 | 651. |
| 16 | .310 | 133. | 16.1 | 654. |
| 17 | .310 | 133. | 16.1 | 658. |
| 18 | .310 | 133. | 16.2 | 643. |
| 19 | .320 | 137. | 16.1 | 656. |
| 20 | .330 | 142. | 16.1 | 674. |
| 21 | .330 | 142. | 16.3 | 651. |
| 22 | .310 | 133. | 16.0 | 575. |
| 23 | .290 | 125. | 16.1 | 539. |
| 24 | .270 | 116. | 16.0 | 508. |

DAY = 99

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 15.9 | 476. |
| 2 | .220 | 95. | 15.6 | 440. |
| 3 | .190 | 82. | 15.7 | 420. |
| 4 | .200 | 86. | 15.8 | 426. |
| 5 | .200 | 86. | 15.7 | 430. |
| 6 | .250 | 107. | 16.2 | 555. |
| 7 | .280 | 120. | 16.3 | 627. |
| 8 | .310 | 133. | 16.0 | 636. |
| 9 | .300 | 129. | 16.3 | 667. |
| 10 | .300 | 129. | 16.2 | 671. |
| 11 | .320 | 137. | 16.1 | 674. |
| 12 | .300 | 129. | 16.2 | 669. |
| 13 | .310 | 133. | 16.3 | 664. |
| 14 | .310 | 133. | 16.2 | 655. |
| 15 | .310 | 133. | 16.1 | 660. |
| 16 | .300 | 129. | 16.2 | 642. |
| 17 | .300 | 129. | 15.9 | 622. |
| 18 | .270 | 116. | 15.9 | 569. |
| 19 | .280 | 120. | 16.4 | 592. |
| 20 | .300 | 129. | 16.6 | 663. |
| 21 | .300 | 129. | 16.5 | 666. |
| 22 | .300 | 129. | 16.4 | 653. |
| 23 | .280 | 120. | 16.1 | 564. |
| 24 | .280 | 120. | 16.1 | 535. |

DAY = 100



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.8 | 500. |
| 2 | .240 | 103. | 15.4 | 439. |
| 3 | .230 | 99. | 15.4 | 412. |
| 4 | .240 | 103. | 15.5 | 439. |
| 5 | .240 | 103. | 15.5 | 445. |
| 6 | .250 | 107. | 15.8 | 498. |
| 7 | .250 | 107. | 16.1 | 549. |
| 8 | .280 | 120. | 16.2 | 613. |
| 9 | .300 | 129. | 16.5 | 681. |
| 10 | .290 | 125. | 16.5 | 680. |
| 11 | .290 | 125. | 16.3 | 662. |
| 12 | .300 | 129. | 16.3 | 668. |
| 13 | .300 | 129. | 16.4 | 680. |
| 14 | .300 | 129. | 16.5 | 686. |
| 15 | .290 | 125. | 16.3 | 640. |
| 16 | .280 | 120. | 16.3 | 626. |
| 17 | .290 | 125. | 16.4 | 645. |
| 18 | .290 | 125. | 16.5 | 624. |
| 19 | .290 | 125. | 16.7 | 643. |
| 20 | .300 | 129. | 16.9 | 642. |
| 21 | .300 | 129. | 16.8 | 623. |
| 22 | .280 | 120. | 16.6 | 538. |
| 23 | .240 | 103. | 15.9 | 376. |
| 24 | .120 | 52. | 12.4 | 116. |

DAY = 105

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .190 | 82. | 15.3 | 299. |
| 2 | .210 | 90. | 15.3 | 281. |
| 3 | .210 | 90. | 15.3 | 281. |
| 4 | .200 | 86. | 15.3 | 275. |
| 5 | .180 | 77. | 15.6 | 280. |
| 6 | .170 | 73. | 15.7 | 283. |
| 7 | .190 | 82. | 16.3 | 344. |
| 8 | .220 | 95. | 16.8 | 450. |
| 9 | .240 | 103. | 16.5 | 495. |
| 10 | .250 | 107. | 16.2 | 487. |
| 11 | .250 | 107. | 16.2 | 485. |
| 12 | .230 | 99. | 16.5 | 495. |
| 13 | .250 | 107. | 16.7 | 548. |
| 14 | .260 | 112. | 16.5 | 545. |
| 15 | .240 | 103. | 16.5 | 504. |
| 16 | .230 | 99. | 16.4 | 492. |
| 17 | .230 | 99. | 16.6 | 506. |
| 18 | .230 | 99. | 16.5 | 516. |
| 19 | .260 | 112. | 16.8 | 566. |
| 20 | .280 | 120. | 16.8 | 584. |
| 21 | .280 | 120. | 16.8 | 589. |
| 22 | .270 | 116. | 16.6 | 560. |
| 23 | .250 | 107. | 16.4 | 512. |
| 24 | .240 | 103. | 16.2 | 482. |

DAY = 106



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 16.0 | 415. |
| 2 | .230 | 99. | 16.6 | 473. |
| 3 | .250 | 107. | 16.6 | 511. |
| 4 | .240 | 103. | 16.4 | 487. |
| 5 | .240 | 103. | 16.4 | 498. |
| 6 | .230 | 99. | 16.4 | 500. |
| 7 | .240 | 103. | 16.4 | 515. |
| 8 | .260 | 112. | 16.8 | 571. |
| 9 | .260 | 112. | 17.0 | 612. |
| 10 | .280 | 120. | 17.3 | 670. |
| 11 | =1.000 | =430. | =1.0 | =1. |
| 12 | .310 | 133. | 16.8 | 662. |
| 13 | .320 | 137. | 17.2 | 679. |
| 14 | .320 | 137. | 17.1 | 662. |
| 15 | .310 | 133. | 17.3 | 667. |
| 16 | .330 | 142. | 17.1 | 657. |
| 17 | .340 | 146. | 17.2 | 676. |
| 18 | .330 | 142. | 17.2 | 665. |
| 19 | .310 | 133. | 17.1 | 635. |
| 20 | .330 | 142. | 17.4 | 659. |
| 21 | .330 | 142. | 17.4 | 664. |
| 22 | .310 | 133. | 17.2 | 625. |
| 23 | .290 | 125. | 17.0 | 585. |
| 24 | .290 | 125. | 17.2 | 582. |

DAY = 108

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .250 | 107. | 16.9 | 514. |
| 2 | .230 | 99. | 16.8 | 461. |
| 3 | .230 | 99. | 16.9 | 474. |
| 4 | .220 | 95. | 16.8 | 447. |
| 5 | .220 | 95. | 16.8 | 455. |
| 6 | .210 | 90. | 16.7 | 430. |
| 7 | .220 | 95. | 16.9 | 470. |
| 8 | .260 | 112. | 17.2 | 575. |
| 9 | .310 | 133. | 17.4 | 655. |
| 10 | .320 | 137. | 17.3 | 656. |
| 11 | .320 | 137. | 17.2 | 661. |
| 12 | .330 | 142. | 17.0 | 656. |
| 13 | .330 | 142. | 17.0 | 657. |
| 14 | .330 | 142. | 17.0 | 649. |
| 15 | .330 | 142. | 17.2 | 662. |
| 16 | .310 | 133. | 16.9 | 623. |
| 17 | .320 | 137. | 17.3 | 670. |
| 18 | .320 | 137. | 17.4 | 678. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .310 | 133. | 17.4 | 666. |
| 21 | .340 | 146. | 17.1 | 677. |
| 22 | .330 | 142. | 17.1 | 661. |
| 23 | .330 | 142. | 17.1 | 652. |
| 24 | .300 | 129. | 16.8 | 577. |

DAY = 110

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .320 | 137. | 16.8 | 647. |
| 2 | .320 | 137. | 16.8 | 637. |
| 3 | .320 | 137. | 16.7 | 629. |
| 4 | .290 | 125. | 16.4 | 568. |
| 5 | .290 | 125. | 16.5 | 560. |
| 6 | .320 | 137. | 16.8 | 649. |
| 7 | .310 | 133. | 16.9 | 643. |
| 8 | .300 | 129. | 17.2 | 671. |
| 9 | .310 | 133. | 17.2 | 680. |
| 10 | .310 | 133. | 17.2 | 678. |
| 11 | .320 | 137. | 17.1 | 684. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .320 | 137. | 17.1 | 678. |
| 14 | .320 | 137. | 17.0 | 676. |
| 15 | .320 | 137. | 17.0 | 682. |
| 16 | .320 | 137. | 17.0 | 670. |
| 17 | .310 | 133. | 17.0 | 659. |
| 18 | .310 | 133. | 17.0 | 657. |
| 19 | .310 | 133. | 17.1 | 658. |
| 20 | .310 | 133. | 17.1 | 655. |
| 21 | .310 | 133. | 17.1 | 652. |
| 22 | .320 | 137. | 17.0 | 654. |
| 23 | .320 | 137. | 16.9 | 642. |
| 24 | .310 | 133. | 17.0 | 643. |

DAY = 111

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 17.0 | 634. |
| 2 | .310 | 133. | 17.0 | 635. |
| 3 | .290 | 125. | 16.9 | 607. |
| 4 | .300 | 129. | 17.0 | 623. |
| 5 | .310 | 133. | 17.0 | 637. |
| 6 | .310 | 133. | 16.9 | 629. |
| 7 | .320 | 137. | 17.0 | 648. |
| 8 | .330 | 142. | 17.1 | 689. |
| 9 | .330 | 142. | 16.9 | 692. |
| 10 | .320 | 137. | 16.8 | 665. |
| 11 | .340 | 146. | 16.8 | 687. |
| 12 | .330 | 142. | 16.8 | 674. |
| 13 | .320 | 137. | 16.8 | 650. |
| 14 | .330 | 142. | 16.8 | 672. |
| 15 | .310 | 133. | 17.1 | 668. |
| 16 | .310 | 133. | 17.0 | 663. |
| 17 | .320 | 137. | 16.9 | 666. |
| 18 | .330 | 142. | 16.7 | 667. |
| 19 | .320 | 137. | 16.9 | 661. |
| 20 | .320 | 137. | 17.1 | 680. |
| 21 | .320 | 137. | 17.0 | 680. |
| 22 | .320 | 137. | 16.9 | 643. |
| 23 | .320 | 137. | 17.0 | 649. |
| 24 | .320 | 137. | 16.9 | 644. |

DAY = 112



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 16.9 | 638. |
| 2 | .320 | 137. | 17.1 | 656. |
| 3 | .320 | 137. | 17.0 | 653. |
| 4 | .320 | 137. | 17.0 | 643. |
| 5 | .320 | 137. | 17.0 | 656. |
| 6 | .330 | 142. | 17.0 | 675. |
| 7 | .340 | 146. | 16.9 | 678. |
| 8 | .350 | 150. | 16.9 | 689. |
| 9 | .340 | 146. | 17.0 | 689. |
| 10 | .340 | 146. | 17.0 | 690. |
| 11 | .330 | 142. | 17.0 | 687. |
| 12 | .330 | 142. | 17.0 | 686. |
| 13 | .330 | 142. | 16.9 | 684. |
| 14 | .330 | 142. | 16.8 | 687. |
| 15 | .330 | 142. | 16.9 | 686. |
| 16 | .330 | 142. | 17.0 | 686. |
| 17 | .340 | 146. | 16.9 | 680. |
| 18 | .320 | 137. | 16.8 | 640. |
| 19 | .320 | 137. | 16.9 | 628. |
| 20 | .330 | 142. | 17.0 | 658. |
| 21 | .330 | 142. | 17.0 | 658. |
| 22 | .330 | 142. | 17.0 | 642. |
| 23 | .320 | 137. | 17.1 | 653. |
| 24 | .280 | 120. | 16.6 | 563. |

DAY = 113

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 16.2 | 473. |
| 2 | .200 | 86. | 15.9 | 362. |
| 3 | .180 | 77. | 16.4 | 361. |
| 4 | .190 | 82. | 16.1 | 342. |
| 5 | .180 | 77. | 16.1 | 342. |
| 6 | .200 | 86. | 16.4 | 406. |
| 7 | .200 | 86. | 16.6 | 444. |
| 8 | .270 | 116. | 16.7 | 559. |
| 9 | .310 | 133. | 16.8 | 662. |
| 10 | .310 | 133. | 16.5 | 667. |
| 11 | .300 | 129. | 16.7 | 654. |
| 12 | .300 | 129. | 16.8 | 672. |
| 13 | .280 | 120. | 16.7 | 619. |
| 14 | .280 | 120. | 16.9 | 637. |
| 15 | .280 | 120. | 17.0 | 634. |
| 16 | .290 | 125. | 17.0 | 630. |
| 17 | .290 | 125. | 17.4 | 670. |
| 18 | .290 | 125. | 17.1 | 645. |
| 19 | .280 | 120. | 16.6 | 616. |
| 20 | .300 | 129. | 16.9 | 667. |
| 21 | .300 | 129. | 17.7 | 665. |
| 22 | .280 | 120. | 17.7 | 616. |
| 23 | .300 | 129. | 17.8 | 666. |
| 24 | .290 | 125. | 17.5 | 616. |

DAY = 114



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.6 | 565. |
| 2 | =1.000 | =430. | =1.0 | =1. |
| 3 | .210 | 90. | 17.0 | 456. |
| 4 | .210 | 90. | 17.3 | 470. |
| 5 | .220 | 95. | 17.4 | 497. |
| 6 | .240 | 103. | 17.3 | 513. |
| 7 | .250 | 107. | 17.2 | 536. |
| 8 | .260 | 112. | 17.5 | 593. |
| 9 | .280 | 120. | 17.6 | 638. |
| 10 | .280 | 120. | 17.6 | 654. |
| 11 | .290 | 125. | 17.6 | 674. |
| 12 | .300 | 129. | 17.6 | 688. |
| 13 | .310 | 133. | 17.6 | 690. |
| 14 | .300 | 129. | 17.5 | 670. |
| 15 | .300 | 129. | 17.8 | 681. |
| 16 | .300 | 129. | 17.8 | 685. |
| 17 | .300 | 129. | 17.8 | 669. |
| 18 | .300 | 129. | 17.9 | 678. |
| 19 | .300 | 129. | 17.6 | 656. |
| 20 | .310 | 133. | 17.5 | 652. |
| 21 | .320 | 137. | 17.8 | 682. |
| 22 | .310 | 133. | 18.1 | 676. |
| 23 | .300 | 129. | 18.1 | 659. |
| 24 | .290 | 125. | 18.2 | 642. |

DAY = 115

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 18.1 | 630. |
| 2 | .280 | 120. | 17.7 | 593. |
| 3 | .280 | 120. | 17.9 | 580. |
| 4 | .270 | 116. | 18.0 | 579. |
| 5 | .260 | 112. | 17.9 | 554. |
| 6 | .270 | 116. | 18.1 | 600. |
| 7 | .290 | 125. | 17.1 | 632. |
| 8 | .320 | 137. | 16.5 | 669. |
| 9 | .340 | 146. | 16.1 | 688. |
| 10 | .340 | 146. | 16.0 | 694. |
| 11 | .340 | 146. | 16.0 | 692. |
| 12 | .340 | 146. | 15.9 | 684. |
| 13 | .340 | 146. | 15.8 | 689. |
| 14 | .350 | 150. | 15.7 | 690. |
| 15 | .360 | 155. | 15.6 | 685. |
| 16 | .360 | 155. | 15.6 | 682. |
| 17 | .350 | 150. | 15.6 | 680. |
| 18 | .350 | 150. | 15.6 | 679. |
| 19 | .350 | 150. | 15.5 | 679. |
| 20 | .350 | 150. | 15.5 | 680. |
| 21 | .360 | 155. | 15.4 | 679. |
| 22 | .360 | 155. | 15.4 | 678. |
| 23 | .370 | 159. | 15.6 | 677. |
| 24 | .340 | 146. | 15.7 | 638. |

DAY = 116



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 15.4 | 571. |
| 2 | .310 | 133. | 15.5 | 567. |
| 3 | .300 | 129. | 15.4 | 537. |
| 4 | .290 | 125. | 15.3 | 532. |
| 5 | .300 | 129. | 15.2 | 536. |
| 6 | .330 | 142. | 15.4 | 612. |
| 7 | .330 | 142. | 15.5 | 640. |
| 8 | .350 | 150. | 15.5 | 680. |
| 9 | .360 | 155. | 15.3 | 674. |
| 10 | .350 | 150. | 15.2 | 664. |
| 11 | .350 | 150. | 15.3 | 687. |
| 12 | .350 | 150. | 15.3 | 677. |
| 13 | .340 | 146. | 15.2 | 656. |
| 14 | .330 | 142. | 15.1 | 636. |
| 15 | .330 | 142. | 15.4 | 640. |
| 16 | .340 | 146. | 15.5 | 685. |
| 17 | .330 | 142. | 15.5 | 651. |
| 18 | .330 | 142. | 15.4 | 649. |
| 19 | .330 | 142. | 15.3 | 634. |
| 20 | .340 | 146. | 15.3 | 654. |
| 21 | .350 | 150. | 15.1 | 654. |
| 22 | .360 | 155. | 15.0 | 645. |
| 23 | .340 | 146. | 14.9 | 619. |
| 24 | .320 | 137. | 14.8 | 573. |

DAY = 117

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 15.0 | 619. |
| 2 | .320 | 137. | 14.8 | 557. |
| 3 | .300 | 129. | 14.9 | 548. |
| 4 | .290 | 125. | 14.7 | 519. |
| 5 | .290 | 125. | 14.8 | 530. |
| 6 | .300 | 129. | 14.8 | 540. |
| 7 | .330 | 142. | 15.0 | 624. |
| 8 | .330 | 142. | 15.2 | 640. |
| 9 | .330 | 142. | 15.5 | 662. |
| 10 | .340 | 146. | 15.6 | 679. |
| 11 | .330 | 142. | 15.6 | 674. |
| 12 | .340 | 146. | 15.6 | 674. |
| 13 | .340 | 146. | 15.8 | 684. |
| 14 | .320 | 137. | 16.5 | 674. |
| 15 | .290 | 125. | 18.0 | 676. |
| 16 | .280 | 120. | 17.9 | 626. |
| 17 | .280 | 120. | 18.0 | 630. |
| 18 | .300 | 129. | 17.9 | 652. |
| 19 | .300 | 129. | 18.0 | 656. |
| 20 | .280 | 120. | 17.7 | 592. |
| 21 | .310 | 133. | 18.0 | 663. |
| 22 | .310 | 133. | 17.9 | 651. |
| 23 | .290 | 125. | 17.9 | 615. |
| 24 | .280 | 120. | 17.9 | 603. |

DAY = 118

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 17.9 | 590. |
| 2 | .270 | 116. | 17.8 | 543. |
| 3 | .250 | 107. | 17.7 | 545. |
| 4 | .230 | 99. | 17.6 | 506. |
| 5 | .230 | 99. | 17.7 | 522. |
| 6 | .280 | 120. | 16.2 | 522. |
| 7 | .320 | 137. | 15.8 | 602. |
| 8 | .330 | 142. | 16.0 | 658. |
| 9 | .340 | 146. | 15.7 | 657. |
| 10 | .320 | 137. | 15.8 | 650. |
| 11 | .300 | 129. | 17.0 | 642. |
| 12 | .300 | 129. | 17.9 | 660. |
| 13 | .310 | 133. | 17.7 | 667. |
| 14 | .310 | 133. | 17.8 | 681. |
| 15 | .320 | 137. | 17.6 | 674. |
| 16 | .310 | 133. | 17.6 | 656. |
| 17 | .300 | 129. | 17.4 | 607. |
| 18 | .300 | 129. | 17.6 | 610. |
| 19 | .280 | 120. | 18.0 | 623. |
| 20 | .290 | 125. | 18.0 | 633. |
| 21 | .300 | 129. | 18.1 | 647. |
| 22 | .300 | 129. | 18.0 | 639. |
| 23 | .290 | 125. | 17.7 | 596. |
| 24 | .230 | 99. | 17.3 | 503. |

DAY = 119

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 17.4 | 461. |
| 2 | .190 | 82. | 17.3 | 440. |
| 3 | .180 | 77. | 17.1 | 409. |
| 4 | .170 | 73. | 17.0 | 381. |
| 5 | .180 | 77. | 17.0 | 384. |
| 6 | .180 | 77. | 17.3 | 435. |
| 7 | .230 | 99. | 18.0 | 558. |
| 8 | .280 | 120. | 18.1 | 637. |
| 9 | .310 | 133. | 17.9 | 666. |
| 10 | .320 | 137. | 17.8 | 677. |
| 11 | .320 | 137. | 17.7 | 677. |
| 12 | .320 | 137. | 17.7 | 686. |
| 13 | .320 | 137. | 17.6 | 670. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .320 | 137. | 17.7 | 679. |
| 16 | .300 | 129. | 17.5 | 633. |
| 17 | .290 | 125. | 17.7 | 628. |
| 18 | .290 | 125. | 17.6 | 622. |
| 19 | .300 | 129. | 17.8 | 629. |
| 20 | .310 | 133. | 17.9 | 669. |
| 21 | .320 | 137. | 17.8 | 672. |
| 22 | .320 | 137. | 17.7 | 658. |
| 23 | .250 | 107. | 16.6 | 484. |
| 24 | .190 | 82. | 15.6 | 304. |

DAY = 120



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .210 | 90. | 15.7 | 306. |
| 2 | .210 | 90. | 15.9 | 321. |
| 3 | .210 | 90. | 16.2 | 349. |
| 4 | .210 | 90. | 16.1 | 348. |
| 5 | .210 | 90. | 16.1 | 350. |
| 6 | .200 | 86. | 15.9 | 333. |
| 7 | .200 | 86. | 16.0 | 335. |
| 8 | .180 | 77. | 16.6 | 347. |
| 9 | .180 | 77. | 16.7 | 350. |
| 10 | .180 | 77. | 16.6 | 351. |
| 11 | .180 | 77. | 16.6 | 349. |
| 12 | .180 | 77. | 16.6 | 353. |
| 13 | .180 | 77. | 16.6 | 353. |
| 14 | .180 | 77. | 16.7 | 351. |
| 15 | .170 | 73. | 16.7 | 352. |
| 16 | .170 | 73. | 16.8 | 353. |
| 17 | .170 | 73. | 16.8 | 354. |
| 18 | .200 | 86. | 17.7 | 494. |
| 19 | .220 | 95. | 17.8 | 559. |
| 20 | .220 | 95. | 17.8 | 553. |
| 21 | .240 | 103. | 18.0 | 583. |
| 22 | .260 | 112. | 17.8 | 599. |
| 23 | .250 | 107. | 17.6 | 561. |
| 24 | .220 | 95. | 17.0 | 466. |

DAY = 121

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 17.2 | 468. |
| 2 | .210 | 90. | 17.1 | 436. |
| 3 | .210 | 90. | 17.0 | 430. |
| 4 | .200 | 86. | 16.9 | 398. |
| 5 | .200 | 86. | 17.0 | 398. |
| 6 | .190 | 82. | 17.2 | 413. |
| 7 | .200 | 86. | 17.1 | 406. |
| 8 | .240 | 103. | 17.6 | 510. |
| 9 | .260 | 112. | 17.5 | 552. |
| 10 | .300 | 129. | 17.6 | 611. |
| 11 | .310 | 133. | 17.4 | 632. |
| 12 | .310 | 133. | 17.4 | 621. |
| 13 | .300 | 129. | 17.6 | 648. |
| 14 | .290 | 125. | 17.5 | 619. |
| 15 | .280 | 120. | 17.7 | 613. |
| 16 | .290 | 125. | 17.7 | 625. |
| 17 | .310 | 133. | 17.6 | 639. |
| 18 | .290 | 125. | 17.6 | 616. |
| 19 | .290 | 125. | 17.8 | 614. |
| 20 | .290 | 125. | 17.7 | 614. |
| 21 | .330 | 142. | 17.8 | 652. |
| 22 | .320 | 137. | 17.7 | 634. |
| 23 | .280 | 120. | 17.7 | 586. |
| 24 | .270 | 116. | 17.9 | 598. |

DAY = 122

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.2 | 521. |
| 2 | .230 | 99. | 17.4 | 484. |
| 3 | .210 | 90. | 17.4 | 460. |
| 4 | .210 | 90. | 17.3 | 439. |
| 5 | .210 | 90. | 17.3 | 439. |
| 6 | .240 | 103. | 17.6 | 493. |
| 7 | .250 | 107. | 18.0 | 577. |
| 8 | .280 | 120. | 17.9 | 627. |
| 9 | .310 | 133. | 17.8 | 676. |
| 10 | .310 | 133. | 17.6 | 666. |
| 11 | .310 | 133. | 17.8 | 687. |
| 12 | .310 | 133. | 17.8 | 688. |
| 13 | .310 | 133. | 17.7 | 692. |
| 14 | .310 | 133. | 17.6 | 676. |
| 15 | .300 | 129. | 17.8 | 678. |
| 16 | .300 | 129. | 17.6 | 649. |
| 17 | .300 | 129. | 17.6 | 651. |
| 18 | .300 | 129. | 17.7 | 648. |
| 19 | .310 | 133. | 17.8 | 666. |
| 20 | .310 | 133. | 17.8 | 673. |
| 21 | .310 | 133. | 17.8 | 687. |
| 22 | .300 | 129. | 17.6 | 662. |
| 23 | .300 | 129. | 17.7 | 660. |
| 24 | .270 | 116. | 17.4 | 591. |

DAY = 123

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.6 | 578. |
| 2 | .270 | 116. | 17.1 | 538. |
| 3 | .240 | 103. | 16.9 | 487. |
| 4 | .240 | 103. | 16.8 | 455. |
| 5 | .240 | 103. | 17.0 | 479. |
| 6 | .250 | 107. | 17.1 | 514. |
| 7 | .280 | 120. | 17.6 | 617. |
| 8 | .300 | 129. | 17.6 | 653. |
| 9 | .300 | 129. | 17.6 | 672. |
| 10 | .310 | 133. | 17.5 | 675. |
| 11 | .320 | 137. | 17.5 | 686. |
| 12 | .310 | 133. | 17.6 | 685. |
| 13 | .310 | 133. | 17.7 | 681. |
| 14 | .310 | 133. | 17.7 | 679. |
| 15 | .310 | 133. | 17.8 | 688. |
| 16 | .310 | 133. | 17.7 | 673. |
| 17 | .320 | 137. | 17.7 | 682. |
| 18 | .310 | 133. | 17.6 | 655. |
| 19 | .290 | 125. | 17.7 | 611. |
| 20 | .280 | 120. | 17.5 | 581. |
| 21 | .310 | 133. | 18.0 | 673. |
| 22 | .300 | 129. | 17.8 | 661. |
| 23 | .290 | 125. | 17.7 | 637. |
| 24 | .260 | 112. | 17.1 | 513. |

DAY = 124



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 16.7 | 409. |
| 2 | .210 | 90. | 16.8 | 392. |
| 3 | .200 | 86. | 17.1 | 402. |
| 4 | .200 | 86. | 17.0 | 401. |
| 5 | .200 | 86. | 17.0 | 401. |
| 6 | .230 | 99. | 17.5 | 483. |
| 7 | .260 | 112. | 17.6 | 563. |
| 8 | .290 | 125. | 17.5 | 626. |
| 9 | .310 | 133. | 17.5 | 657. |
| 10 | .310 | 133. | 17.4 | 667. |
| 11 | .320 | 137. | 17.4 | 673. |
| 12 | .320 | 137. | 17.3 | 670. |
| 13 | .320 | 137. | 17.3 | 664. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .310 | 133. | 17.4 | 647. |
| 16 | .300 | 129. | 17.6 | 648. |
| 17 | .300 | 129. | 17.6 | 653. |
| 18 | .310 | 133. | 17.5 | 656. |
| 19 | .310 | 133. | 17.5 | 653. |
| 20 | .300 | 129. | 17.5 | 636. |
| 21 | .310 | 133. | 17.7 | 665. |
| 22 | .320 | 137. | 17.7 | 679. |
| 23 | .300 | 129. | 17.6 | 623. |
| 24 | .240 | 103. | 17.1 | 494. |

DAY = 126

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 17.4 | 627. |
| 2 | .280 | 120. | 17.4 | 617. |
| 3 | .270 | 116. | 17.4 | 605. |
| 4 | .270 | 116. | 17.5 | 608. |
| 5 | .280 | 120. | 17.6 | 619. |
| 6 | .290 | 125. | 17.5 | 640. |
| 7 | .300 | 129. | 17.4 | 649. |
| 8 | .310 | 133. | 17.5 | 684. |
| 9 | .300 | 129. | 17.5 | 675. |
| 10 | .300 | 129. | 17.5 | 660. |
| 11 | .300 | 129. | 17.6 | 671. |
| 12 | .310 | 133. | 17.6 | 683. |
| 13 | .290 | 125. | 17.4 | 649. |
| 14 | .290 | 125. | 17.5 | 650. |
| 15 | .270 | 116. | 17.7 | 640. |
| 16 | .270 | 116. | 17.6 | 625. |
| 17 | .280 | 120. | 17.9 | 667. |
| 18 | .300 | 129. | 17.7 | 687. |
| 19 | .310 | 133. | 17.6 | 687. |
| 20 | .310 | 133. | 17.5 | 659. |
| 21 | .300 | 129. | 17.6 | 659. |
| 22 | .310 | 133. | 17.6 | 675. |
| 23 | .280 | 120. | 17.2 | 592. |
| 24 | .230 | 99. | 16.9 | 479. |

DAY = 127



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .210 | 90. | 16.6 | 388. |
| 2 | .210 | 90. | 16.8 | 400. |
| 3 | .210 | 90. | 16.8 | 394. |
| 4 | .210 | 90. | 16.8 | 399. |
| 5 | .210 | 90. | 16.9 | 394. |
| 6 | .220 | 95. | 16.8 | 394. |
| 7 | .250 | 107. | 17.5 | 539. |
| 8 | .290 | 125. | 17.8 | 652. |
| 9 | .290 | 125. | 17.8 | 674. |
| 10 | .280 | 120. | 17.7 | 653. |
| 11 | .280 | 120. | 17.7 | 648. |
| 12 | .270 | 116. | 17.7 | 637. |
| 13 | .270 | 116. | 17.6 | 623. |
| 14 | .260 | 112. | 17.6 | 605. |
| 15 | .250 | 107. | 17.4 | 573. |
| 16 | .250 | 107. | 17.5 | 570. |
| 17 | .280 | 120. | 17.5 | 605. |
| 18 | .260 | 112. | 17.5 | 596. |
| 19 | .290 | 125. | 17.6 | 661. |
| 20 | .300 | 129. | 17.6 | 664. |
| 21 | .310 | 133. | 17.5 | 683. |
| 22 | .320 | 137. | 17.3 | 670. |
| 23 | .300 | 129. | 17.2 | 628. |
| 24 | .260 | 112. | 17.0 | 563. |

DAY = 128

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 17.1 | 543. |
| 2 | .230 | 99. | 17.1 | 535. |
| 3 | .230 | 99. | 17.3 | 543. |
| 4 | .230 | 99. | 17.2 | 543. |
| 5 | .260 | 112. | 15.7 | 544. |
| 6 | .290 | 125. | 14.3 | 548. |
| 7 | .300 | 129. | 14.2 | 554. |
| 8 | .310 | 133. | 14.4 | 583. |
| 9 | .330 | 142. | 14.5 | 618. |
| 10 | .330 | 142. | 14.2 | 643. |
| 11 | .350 | 150. | 14.3 | 665. |
| 12 | .360 | 155. | 14.2 | 677. |
| 13 | .380 | 163. | 14.2 | 681. |
| 14 | .360 | 155. | 14.0 | 633. |
| 15 | .350 | 150. | 13.6 | 617. |
| 16 | .320 | 137. | 13.7 | 622. |
| 17 | .330 | 142. | 14.3 | 652. |
| 18 | .340 | 146. | 14.3 | 649. |
| 19 | .350 | 150. | 14.4 | 653. |
| 20 | .360 | 155. | 14.5 | 663. |
| 21 | .370 | 159. | 14.6 | 680. |
| 22 | .370 | 159. | 14.6 | 678. |
| 23 | .370 | 159. | 14.7 | 675. |
| 24 | .350 | 150. | 14.9 | 634. |

DAY # 130



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 16.2 | 599. |
| 2 | .290 | 125. | 17.2 | 601. |
| 3 | .290 | 125. | 17.3 | 631. |
| 4 | .300 | 129. | 17.2 | 636. |
| 5 | .310 | 133. | 17.3 | 661. |
| 6 | .320 | 137. | 17.3 | 682. |
| 7 | .300 | 129. | 17.3 | 649. |
| 8 | .320 | 137. | 17.5 | 686. |
| 9 | .320 | 137. | 17.5 | 704. |
| 10 | .330 | 142. | 17.3 | 719. |
| 11 | .340 | 146. | 17.4 | 715. |
| 12 | .310 | 133. | 17.1 | 715. |
| 13 | .320 | 137. | 17.0 | 678. |
| 14 | .320 | 137. | 17.0 | 662. |
| 15 | .310 | 133. | 17.0 | 655. |
| 16 | .300 | 129. | 17.1 | 634. |
| 17 | .310 | 133. | 17.1 | 642. |
| 18 | .300 | 129. | 17.0 | 616. |
| 19 | .300 | 129. | 17.0 | 622. |
| 20 | .300 | 129. | 17.2 | 635. |
| 21 | .310 | 133. | 17.3 | 644. |
| 22 | .320 | 137. | 17.3 | 661. |
| 23 | .310 | 133. | 17.3 | 642. |
| 24 | .310 | 133. | 17.2 | 623. |

DAY # 131

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 17.0 | 574. |
| 2 | .260 | 112. | 16.9 | 540. |
| 3 | .250 | 107. | 17.0 | 538. |
| 4 | .250 | 107. | 16.8 | 516. |
| 5 | .260 | 112. | 16.9 | 543. |
| 6 | .260 | 112. | 17.0 | 543. |
| 7 | .290 | 125. | 17.2 | 565. |
| 8 | .310 | 133. | 17.4 | 621. |
| 9 | .310 | 133. | 17.4 | 690. |
| 10 | .310 | 133. | 17.3 | 687. |
| 11 | .310 | 133. | 17.4 | 688. |
| 12 | .310 | 133. | 17.3 | 678. |
| 13 | .310 | 133. | 17.2 | 664. |
| 14 | .310 | 133. | 17.3 | 689. |
| 15 | .320 | 137. | 17.3 | 675. |
| 16 | .320 | 137. | 17.2 | 678. |
| 17 | .320 | 137. | 17.1 | 678. |
| 18 | .330 | 142. | 17.3 | 678. |
| 19 | .310 | 133. | 17.3 | 648. |
| 20 | .300 | 129. | 17.3 | 646. |
| 21 | .310 | 133. | 17.4 | 666. |
| 22 | .300 | 129. | 17.1 | 674. |
| 23 | .300 | 129. | 17.2 | 635. |
| 24 | .260 | 112. | 16.9 | 567. |

DAY = 132

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.0 | 556. |
| 2 | .260 | 112. | 17.1 | 566. |
| 3 | .250 | 107. | 16.9 | 528. |
| 4 | .240 | 103. | 17.0 | 526. |
| 5 | .250 | 107. | 17.1 | 540. |
| 6 | .270 | 116. | 17.1 | 581. |
| 7 | .300 | 129. | 17.2 | 622. |
| 8 | .330 | 142. | 17.4 | 698. |
| 9 | .330 | 142. | 17.3 | 689. |
| 10 | .320 | 137. | 17.3 | 677. |
| 11 | .330 | 142. | 17.4 | 694. |
| 12 | .330 | 142. | 17.3 | 690. |
| 13 | .330 | 142. | 17.3 | 682. |
| 14 | .340 | 146. | 17.3 | 687. |
| 15 | .330 | 142. | 17.3 | 685. |
| 16 | .320 | 137. | 17.2 | 658. |
| 17 | .320 | 137. | 17.4 | 668. |
| 18 | .320 | 137. | 17.1 | 652. |
| 19 | .320 | 137. | 17.1 | 636. |
| 20 | .320 | 137. | 17.2 | 644. |
| 21 | .330 | 142. | 17.4 | 678. |
| 22 | .330 | 142. | 17.4 | 677. |
| 23 | .320 | 137. | 17.3 | 672. |
| 24 | .270 | 116. | 16.8 | 524. |

DAY = 133

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .230 | 99. | 16.3 | 394. |
| 2 | .210 | 90. | 16.3 | 375. |
| 3 | .200 | 86. | 16.4 | 377. |
| 4 | .200 | 86. | 16.4 | 377. |
| 5 | .200 | 86. | 16.3 | 381. |
| 6 | .220 | 95. | 16.7 | 458. |
| 7 | .240 | 103. | 17.1 | 539. |
| 8 | .280 | 120. | 17.4 | 619. |
| 9 | .290 | 125. | 17.3 | 645. |
| 10 | .290 | 125. | 17.6 | 691. |
| 11 | .300 | 129. | 17.5 | 692. |
| 12 | .300 | 129. | 17.5 | 692. |
| 13 | .300 | 129. | 17.4 | 676. |
| 14 | .300 | 129. | 17.6 | 690. |
| 15 | .300 | 129. | 17.6 | 680. |
| 16 | .290 | 125. | 17.5 | 655. |
| 17 | .280 | 120. | 17.7 | 643. |
| 18 | .270 | 116. | 17.7 | 628. |
| 19 | .270 | 116. | 17.7 | 621. |
| 20 | .270 | 116. | 17.7 | 609. |
| 21 | .280 | 120. | 18.0 | 645. |
| 22 | .280 | 120. | 17.8 | 647. |
| 23 | .280 | 120. | 17.8 | 653. |
| 24 | .270 | 116. | 17.4 | 598. |

DAY = 134



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.4 | 607. |
| 2 | .260 | 112. | 17.3 | 595. |
| 3 | .260 | 112. | 17.4 | 618. |
| 4 | .270 | 116. | 17.4 | 601. |
| 5 | .270 | 116. | 17.4 | 586. |
| 6 | .270 | 116. | 17.4 | 594. |
| 7 | .260 | 112. | 17.5 | 589. |
| 8 | .280 | 120. | 17.6 | 639. |
| 9 | .290 | 125. | 17.5 | 657. |
| 10 | .290 | 125. | 17.5 | 654. |
| 11 | .290 | 125. | 17.5 | 654. |
| 12 | .290 | 125. | 17.5 | 656. |
| 13 | .290 | 125. | 17.6 | 657. |
| 14 | .290 | 125. | 17.6 | 649. |
| 15 | .290 | 125. | 17.7 | 642. |
| 16 | .290 | 125. | 17.5 | 633. |
| 17 | .280 | 120. | 17.6 | 627. |
| 18 | .280 | 120. | 17.7 | 627. |
| 19 | .280 | 120. | 17.7 | 624. |
| 20 | .280 | 120. | 17.7 | 619. |
| 21 | .290 | 125. | 17.9 | 653. |
| 22 | .290 | 125. | 17.9 | 673. |
| 23 | .290 | 125. | 17.8 | 651. |
| 24 | .290 | 125. | 17.8 | 666. |

DAY = 135

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 17.8 | 662. |
| 2 | .280 | 120. | 17.6 | 624. |
| 3 | .260 | 112. | 17.5 | 583. |
| 4 | .250 | 107. | 17.5 | 562. |
| 5 | .240 | 103. | 17.2 | 535. |
| 6 | .230 | 99. | 17.2 | 511. |
| 7 | .240 | 103. | 17.2 | 529. |
| 8 | .260 | 112. | 17.4 | 561. |
| 9 | .300 | 129. | 17.3 | 619. |
| 10 | .310 | 133. | 17.4 | 649. |
| 11 | .320 | 137. | 17.3 | 673. |
| 12 | .320 | 137. | 17.3 | 673. |
| 13 | .320 | 137. | 17.4 | 679. |
| 14 | .310 | 133. | 17.5 | 678. |
| 15 | .300 | 129. | 17.7 | 683. |
| 16 | .310 | 133. | 17.7 | 690. |
| 17 | .300 | 129. | 17.6 | 673. |
| 18 | .300 | 129. | 17.7 | 670. |
| 19 | .310 | 133. | 17.6 | 670. |
| 20 | .320 | 137. | 17.5 | 671. |
| 21 | .320 | 137. | 17.9 | 708. |
| 22 | .310 | 133. | 17.7 | 682. |
| 23 | .300 | 129. | 17.5 | 639. |
| 24 | .290 | 125. | 17.4 | 619. |

DAY = 136

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 17.4 | 619. |
| 2 | .290 | 125. | 17.4 | 618. |
| 3 | .290 | 125. | 17.3 | 600. |
| 4 | .290 | 125. | 17.3 | 599. |
| 5 | .280 | 120. | 17.5 | 599. |
| 6 | .290 | 125. | 17.7 | 636. |
| 7 | .310 | 133. | 17.5 | 665. |
| 8 | .310 | 133. | 17.6 | 687. |
| 9 | .320 | 137. | 17.6 | 691. |
| 10 | .330 | 142. | 17.5 | 695. |
| 11 | .340 | 146. | 17.5 | 695. |
| 12 | .330 | 142. | 17.5 | 695. |
| 13 | .320 | 137. | 17.7 | 694. |
| 14 | .330 | 142. | 17.5 | 694. |
| 15 | .330 | 142. | 17.3 | 687. |
| 16 | .330 | 142. | 17.4 | 692. |
| 17 | .330 | 142. | 17.4 | 694. |
| 18 | .330 | 142. | 17.5 | 689. |
| 19 | .330 | 142. | 17.6 | 695. |
| 20 | .340 | 146. | 17.5 | 701. |
| 21 | .340 | 146. | 17.6 | 706. |
| 22 | .340 | 146. | 17.6 | 711. |
| 23 | .350 | 150. | 17.3 | 684. |
| 24 | .330 | 142. | 17.1 | 611. |

DAY = 137

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 17.3 | 604. |
| 2 | .310 | 133. | 17.2 | 577. |
| 3 | .300 | 129. | 17.2 | 565. |
| 4 | .290 | 125. | 17.2 | 548. |
| 5 | .290 | 125. | 17.6 | 589. |
| 6 | .290 | 125. | 17.4 | 600. |
| 7 | .320 | 137. | 17.6 | 668. |
| 8 | .330 | 142. | 17.5 | 689. |
| 9 | .320 | 137. | 17.4 | 673. |
| 10 | .340 | 146. | 17.2 | 672. |
| 11 | .350 | 150. | 17.2 | 670. |
| 12 | .350 | 150. | 17.2 | 672. |
| 13 | .330 | 142. | 17.3 | 671. |
| 14 | .330 | 142. | 17.2 | 663. |
| 15 | .340 | 146. | 17.2 | 670. |
| 16 | .330 | 142. | 17.4 | 683. |
| 17 | .320 | 137. | 17.6 | 674. |
| 18 | .320 | 137. | 17.6 | 669. |
| 19 | .320 | 137. | 17.6 | 668. |
| 20 | .320 | 137. | 17.5 | 656. |
| 21 | .320 | 137. | 17.5 | 666. |
| 22 | .320 | 137. | 17.5 | 673. |
| 23 | .290 | 125. | 17.7 | 633. |
| 24 | .290 | 125. | 17.4 | 607. |

DAY # 138



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 17.0 | 546. |
| 2 | .280 | 120. | 17.6 | 598. |
| 3 | .270 | 116. | 17.4 | 573. |
| 4 | .270 | 116. | 17.3 | 568. |
| 5 | .280 | 120. | 17.5 | 600. |
| 6 | .290 | 125. | 17.5 | 641. |
| 7 | .300 | 129. | 17.5 | 654. |
| 8 | .300 | 129. | 17.5 | 674. |
| 9 | .300 | 129. | 17.4 | 661. |
| 10 | .300 | 129. | 17.4 | 666. |
| 11 | .310 | 133. | 17.4 | 670. |
| 12 | .310 | 133. | 17.4 | 674. |
| 13 | .310 | 133. | 17.5 | 664. |
| 14 | .310 | 133. | 17.5 | 665. |
| 15 | .300 | 129. | 17.6 | 658. |
| 16 | .300 | 129. | 17.7 | 663. |
| 17 | .300 | 129. | 17.7 | 660. |
| 18 | .290 | 125. | 17.8 | 639. |
| 19 | .290 | 125. | 18.0 | 657. |
| 20 | .300 | 129. | 17.8 | 643. |
| 21 | .310 | 133. | 18.0 | 674. |
| 22 | .320 | 137. | 17.9 | 691. |
| 23 | .310 | 133. | 17.8 | 644. |
| 24 | .290 | 125. | 17.9 | 629. |

DAY # 139

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 17.6 | 578. |
| 2 | .260 | 112. | 17.7 | 554. |
| 3 | .240 | 103. | 17.7 | 521. |
| 4 | .250 | 107. | 17.5 | 512. |
| 5 | .250 | 107. | 17.5 | 508. |
| 6 | .230 | 99. | 17.5 | 514. |
| 7 | .240 | 103. | 17.8 | 577. |
| 8 | .310 | 133. | 17.7 | 669. |
| 9 | .310 | 133. | 17.6 | 678. |
| 10 | .300 | 129. | 17.6 | 678. |
| 11 | .310 | 133. | 17.5 | 684. |
| 12 | .310 | 133. | 17.6 | 685. |
| 13 | .300 | 129. | 17.7 | 681. |
| 14 | .290 | 125. | 17.6 | 683. |
| 15 | .300 | 129. | 17.7 | 681. |
| 16 | .290 | 125. | 17.7 | 674. |
| 17 | .290 | 125. | 17.9 | 681. |
| 18 | .230 | 99. | 17.9 | 672. |
| 19 | .300 | 129. | 17.9 | 677. |
| 20 | .300 | 129. | 17.8 | 665. |
| 21 | .310 | 133. | 17.9 | 682. |
| 22 | .300 | 129. | 17.9 | 676. |
| 23 | .290 | 125. | 17.8 | 654. |
| 24 | .290 | 125. | 17.8 | 624. |

DAY = 140



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.4 | 562. |
| 2 | .220 | 95. | 17.0 | 509. |
| 3 | .180 | 77. | 17.0 | 426. |
| 4 | .170 | 73. | 17.2 | 434. |
| 5 | .170 | 73. | 17.4 | 447. |
| 6 | .190 | 82. | 17.6 | 485. |
| 7 | .260 | 112. | 18.2 | 629. |
| 8 | .250 | 107. | 18.0 | 678. |
| 9 | .170 | 73. | 17.8 | 684. |
| 10 | .250 | 107. | 17.7 | 644. |
| 11 | .310 | 133. | 17.8 | 674. |
| 12 | .310 | 133. | 17.8 | 683. |
| 13 | .300 | 129. | 17.8 | 674. |
| 14 | .300 | 129. | 17.9 | 684. |
| 15 | .290 | 125. | 18.0 | 682. |
| 16 | .290 | 125. | 18.0 | 681. |
| 17 | .280 | 120. | 17.9 | 655. |
| 18 | .280 | 120. | 17.8 | 610. |
| 19 | .280 | 120. | 18.0 | 635. |
| 20 | .300 | 129. | 17.8 | 645. |
| 21 | .300 | 129. | 17.9 | 654. |
| 22 | .300 | 129. | 17.9 | 670. |
| 23 | .300 | 129. | 18.2 | 657. |
| 24 | .230 | 99. | 17.3 | 474. |

DAY = 141

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 16.8 | 357. |
| 2 | .210 | 90. | 17.2 | 387. |
| 3 | .190 | 82. | 17.9 | 460. |
| 4 | .210 | 90. | 18.1 | 507. |
| 5 | .210 | 90. | 17.9 | 493. |
| 6 | .210 | 90. | 18.0 | 509. |
| 7 | .210 | 90. | 18.1 | 531. |
| 8 | .240 | 103. | 18.3 | 608. |
| 9 | .280 | 120. | 18.0 | 646. |
| 10 | .300 | 129. | 18.1 | 686. |
| 11 | .300 | 129. | 18.0 | 679. |
| 12 | .300 | 129. | 17.8 | 658. |
| 13 | .300 | 129. | 17.7 | 649. |
| 14 | .310 | 133. | 17.8 | 657. |
| 15 | .310 | 133. | 17.9 | 672. |
| 16 | .310 | 133. | 17.9 | 671. |
| 17 | .300 | 129. | 18.0 | 674. |
| 18 | .300 | 129. | 18.0 | 667. |
| 19 | .300 | 129. | 18.0 | 661. |
| 20 | .300 | 129. | 17.8 | 624. |
| 21 | .300 | 129. | 17.9 | 630. |
| 22 | .320 | 137. | 18.0 | 661. |
| 23 | .310 | 133. | 18.0 | 656. |
| 24 | .300 | 129. | 17.9 | 629. |

DAY # 142



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 17.8 | 629. |
| 2 | .300 | 129. | 17.9 | 628. |
| 3 | .290 | 125. | 17.8 | 591. |
| 4 | .270 | 116. | 17.8 | 571. |
| 5 | .270 | 116. | 17.8 | 571. |
| 6 | .260 | 112. | 17.5 | 531. |
| 7 | .240 | 103. | 17.6 | 510. |
| 8 | .270 | 116. | 17.8 | 561. |
| 9 | .280 | 120. | 17.8 | 607. |
| 10 | .310 | 133. | 17.9 | 655. |
| 11 | .320 | 137. | 17.9 | 672. |
| 12 | .360 | 155. | 15.1 | 672. |
| 13 | .410 | 176. | 13.5 | 671. |
| 14 | .400 | 172. | 13.3 | 643. |
| 15 | .410 | 176. | 13.5 | 653. |
| 16 | .430 | 185. | 13.6 | 665. |
| 17 | .440 | 189. | 13.6 | 673. |
| 18 | .420 | 180. | 13.8 | 660. |
| 19 | .400 | 172. | 13.9 | 650. |
| 20 | .410 | 176. | 13.9 | 637. |
| 21 | .410 | 176. | 14.1 | 664. |
| 22 | .420 | 180. | 14.1 | 679. |
| 23 | .410 | 176. | 14.1 | 663. |
| 24 | .360 | 155. | 13.8 | 588. |

DAY # 143

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 13.9 | 530. |
| 2 | .290 | 125. | 13.1 | 448. |
| 3 | .280 | 120. | 13.1 | 413. |
| 4 | .270 | 116. | 13.1 | 407. |
| 5 | .260 | 112. | 13.1 | 402. |
| 6 | .270 | 116. | 13.0 | 401. |
| 7 | .270 | 116. | 12.9 | 392. |
| 8 | .270 | 116. | 13.5 | 478. |
| 9 | .340 | 146. | 13.8 | 592. |
| 10 | .370 | 159. | 13.9 | 653. |
| 11 | .380 | 163. | 13.9 | 661. |
| 12 | .380 | 163. | 14.0 | 669. |
| 13 | .380 | 163. | 13.9 | 662. |
| 14 | .370 | 159. | 13.9 | 646. |
| 15 | .370 | 159. | 14.0 | 642. |
| 16 | .360 | 155. | 14.0 | 633. |
| 17 | .350 | 150. | 13.9 | 609. |
| 18 | .360 | 155. | 14.1 | 640. |
| 19 | .360 | 155. | 14.2 | 644. |
| 20 | .370 | 159. | 14.1 | 650. |
| 21 | .370 | 159. | 14.3 | 668. |
| 22 | .370 | 159. | 14.4 | 674. |
| 23 | .370 | 159. | 14.3 | 647. |
| 24 | .370 | 159. | 14.3 | 650. |

DAY = 148

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 14.2 | 624. |
| 2 | .340 | 146. | 14.0 | 589. |
| 3 | .330 | 142. | 14.1 | 580. |
| 4 | .320 | 137. | 14.0 | 561. |
| 5 | .330 | 142. | 14.2 | 583. |
| 6 | .350 | 150. | 14.2 | 623. |
| 7 | .360 | 155. | 14.3 | 650. |
| 8 | .380 | 163. | 14.3 | 682. |
| 9 | .400 | 172. | 14.0 | 681. |
| 10 | .380 | 163. | 14.0 | 676. |
| 11 | .390 | 168. | 14.1 | 674. |
| 12 | .390 | 168. | 14.1 | 677. |
| 13 | .390 | 168. | 14.1 | 672. |
| 14 | .400 | 172. | 14.0 | 673. |
| 15 | .400 | 172. | 13.9 | 668. |
| 16 | .410 | 176. | 14.0 | 670. |
| 17 | .390 | 168. | 13.9 | 640. |
| 18 | .380 | 163. | 14.0 | 655. |
| 19 | .380 | 163. | 14.0 | 638. |
| 20 | .380 | 163. | 14.1 | 644. |
| 21 | .380 | 163. | 14.1 | 644. |
| 22 | .380 | 163. | 14.1 | 644. |
| 23 | .380 | 163. | 14.1 | 643. |
| 24 | .390 | 168. | 14.0 | 638. |

DAY = 149

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 14.3 | 584. |
| 2 | .310 | 133. | 14.6 | 612. |
| 3 | .320 | 137. | 14.6 | 629. |
| 4 | .320 | 137. | 14.6 | 610. |
| 5 | .330 | 142. | 14.5 | 617. |
| 6 | .340 | 146. | 14.0 | 614. |
| 7 | .360 | 155. | 14.4 | 667. |
| 8 | .360 | 155. | 14.3 | 673. |
| 9 | .370 | 159. | 14.3 | 676. |
| 10 | .370 | 159. | 14.3 | 676. |
| 11 | .370 | 159. | 14.7 | 709. |
| 12 | .390 | 168. | 14.7 | 712. |
| 13 | .390 | 168. | 14.6 | 709. |
| 14 | .390 | 168. | 14.7 | 706. |
| 15 | .390 | 168. | 14.6 | 702. |
| 16 | .380 | 163. | 14.7 | 698. |
| 17 | .370 | 159. | 14.7 | 682. |
| 18 | .380 | 163. | 14.6 | 666. |
| 19 | .380 | 163. | 14.8 | 667. |
| 20 | .390 | 168. | 14.8 | 667. |
| 21 | .390 | 168. | 14.6 | 668. |
| 22 | .400 | 172. | 14.7 | 674. |
| 23 | .410 | 176. | 14.7 | 684. |
| 24 | .320 | 137. | 13.9 | 548. |

DAY = 150



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 13.3 | 432. |
| 2 | .260 | 112. | 13.2 | 395. |
| 3 | .260 | 112. | 13.2 | 393. |
| 4 | .260 | 112. | 13.2 | 398. |
| 5 | .250 | 107. | 13.7 | 474. |
| 6 | .260 | 112. | 14.0 | 494. |
| 7 | .290 | 125. | 14.2 | 540. |
| 8 | .340 | 146. | 14.0 | 620. |
| 9 | .390 | 168. | 14.2 | 678. |
| 10 | .400 | 172. | 14.2 | 685. |
| 11 | .400 | 172. | 14.1 | 678. |
| 12 | .380 | 163. | 14.2 | 656. |
| 13 | .370 | 159. | 14.2 | 671. |
| 14 | .370 | 159. | 14.2 | 660. |
| 15 | .370 | 159. | 14.2 | 659. |
| 16 | .380 | 163. | 14.0 | 664. |
| 17 | .370 | 159. | 14.0 | 653. |
| 18 | .370 | 159. | 14.1 | 649. |
| 19 | .360 | 155. | 14.2 | 635. |
| 20 | .350 | 150. | 14.4 | 640. |
| 21 | .330 | 142. | 14.3 | 613. |
| 22 | .340 | 146. | 14.5 | 642. |
| 23 | .340 | 146. | 14.4 | 625. |
| 24 | .330 | 142. | 14.2 | 586. |

DAY = 151

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 14.1 | 578. |
| 2 | .290 | 125. | 14.0 | 564. |
| 3 | .290 | 125. | 14.0 | 546. |
| 4 | .270 | 116. | 14.0 | 538. |
| 5 | .270 | 116. | 14.0 | 525. |
| 6 | .250 | 107. | 13.9 | 499. |
| 7 | .240 | 103. | 13.9 | 483. |
| 8 | .260 | 112. | 13.8 | 512. |
| 9 | .200 | 86. | 13.9 | 616. |
| 10 | .270 | 116. | 13.6 | 633. |
| 11 | .300 | 129. | 13.4 | 616. |
| 12 | .300 | 129. | 13.7 | 665. |
| 13 | .290 | 125. | 13.9 | 666. |
| 14 | .260 | 112. | 14.1 | 668. |
| 15 | .290 | 125. | 14.3 | 658. |
| 16 | .360 | 155. | 14.4 | 652. |
| 17 | .270 | 116. | 14.5 | 672. |
| 18 | .180 | 77. | 14.4 | 669. |
| 19 | .170 | 73. | 14.5 | 636. |
| 20 | .180 | 77. | 14.5 | 654. |
| 21 | .160 | 69. | 14.7 | 662. |
| 22 | .170 | 73. | 14.5 | 659. |
| 23 | .190 | 82. | 14.4 | 602. |
| 24 | .150 | 64. | 14.5 | 614. |

APPENDIX H

IOWA POWER & LIGHT

COUNCIL BLUFFS STATION

UNIT 3

Input Data - Revised Analysis

**PULVERIZED COAL-FIRED UTILITY BOILER NOx EMISSION MONITORING**

IOWA POWER AND LIGHT - COUNCIL BLUFFS UNIT 3

***NOTE - CO2 USED FOR DILUTION CORRECTION, NOT O2***

BABCOCK AND WILCOX BOILER WITH DUAL REGISTER BURNERS 720 GROSS MWE

WYOMING SUBBITUMINOUS COAL NOX MON. REL. ACC. = 9.53PC

DAY 47 = 16 FEBRUARY 1981 ***REVISED ANALYSIS***

PERFORMANCE NOX = 0.34 LB/10**6BTU (146 NG/J)

**INPUT DATA**

DAY = 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 11.5 | 435. |
| 2 | .320 | 137. | 11.4 | 404. |
| 3 | .310 | 133. | 11.4 | 383. |
| 4 | .320 | 137. | 11.2 | 359. |
| 5 | .310 | 133. | 11.3 | 372. |
| 6 | .330 | 142. | 11.8 | 462. |
| 7 | .390 | 168. | 12.1 | 561. |
| 8 | .450 | 193. | 12.1 | 621. |
| 9 | .470 | 202. | 12.2 | 671. |
| 10 | .440 | 189. | 12.4 | 678. |
| 11 | .430 | 185. | 12.6 | 678. |
| 12 | .430 | 185. | 12.6 | 685. |
| 13 | .440 | 189. | 12.4 | 667. |
| 14 | .440 | 189. | 12.4 | 653. |
| 15 | .430 | 185. | 12.5 | 641. |
| 16 | .440 | 189. | 12.6 | 643. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .410 | 176. | 13.7 | 664. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .400 | 172. | 14.0 | 650. |
| 21 | .410 | 176. | 14.1 | 668. |
| 22 | -1.000 | -430. | -1.0 | -1. |
| 23 | .340 | 146. | 13.9 | 537. |
| 24 | .280 | 120. | 13.5 | 416. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 15.9 | 432. |
| 2 | .250 | 107. | 15.8 | 435. |
| 3 | .240 | 103. | 15.7 | 413. |
| 4 | .230 | 99. | 15.9 | 418. |
| 5 | .220 | 95. | 15.9 | 424. |
| 6 | .230 | 99. | 15.9 | 469. |
| 7 | .280 | 120. | 16.4 | 583. |
| 8 | .330 | 142. | 16.5 | 679. |
| 9 | .340 | 146. | 16.5 | 692. |
| 10 | .340 | 146. | 16.3 | 688. |
| 11 | .330 | 142. | 16.3 | 679. |
| 12 | .340 | 146. | 16.4 | 686. |
| 13 | .340 | 146. | 16.3 | 684. |
| 14 | .340 | 146. | 16.5 | 681. |
| 15 | .340 | 146. | 16.4 | 682. |
| 16 | .340 | 146. | 16.5 | 685. |
| 17 | .330 | 142. | 16.5 | 663. |
| 18 | .330 | 142. | 16.5 | 664. |
| 19 | .330 | 142. | 16.5 | 636. |
| 20 | .330 | 142. | 16.6 | 651. |

| | | | | |
|---|---|---|---|---|
| 21 | .330 | 142. | 15.5 | 629. |
| 22 | .340 | 146. | 15.6 | 672. |
| 23 | .320 | 137. | 15.3 | 611. |
| 24 | .260 | 112. | 15.0 | 493. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 15.0 | 338. |
| 2 | .200 | 86. | 14.8 | 322. |
| 3 | .210 | 90. | 14.8 | 322. |
| 4 | .200 | 86. | 14.8 | 313. |
| 5 | .210 | 90. | 14.6 | 304. |
| 6 | .220 | 95. | 14.5 | 308. |
| 7 | .220 | 95. | 15.0 | 352. |
| 8 | .250 | 107. | 15.3 | 487. |
| 9 | .310 | 133. | 15.8 | 655. |
| 10 | .340 | 146. | 15.9 | 693. |
| 11 | .340 | 146. | 15.8 | 693. |
| 12 | .330 | 142. | 15.7 | 675. |
| 13 | .320 | 137. | 15.7 | 661. |
| 14 | .310 | 133. | 15.6 | 623. |
| 15 | .290 | 125. | 15.6 | 594. |
| 16 | .290 | 125. | 15.6 | 573. |
| 17 | .300 | 129. | 15.7 | 594. |
| 18 | .320 | 137. | 15.7 | 637. |
| 19 | .310 | 133. | 15.6 | 627. |
| 20 | .340 | 146. | 15.7 | 667. |
| 21 | .330 | 142. | 15.2 | 590. |
| 22 | .320 | 137. | 15.3 | 580. |
| 23 | .310 | 133. | 15.4 | 578. |
| 24 | .270 | 116. | 15.1 | 497. |

DAY = 54

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.3 | 514. |
| 2 | .270 | 116. | 15.2 | 532. |
| 3 | .270 | 116. | 15.1 | 519. |
| 4 | .270 | 116. | 15.2 | 526. |
| 5 | .260 | 112. | 15.1 | 525. |
| 6 | .270 | 116. | 15.1 | 522. |
| 7 | .300 | 129. | 15.2 | 597. |
| 8 | .350 | 150. | 15.4 | 679. |
| 9 | .370 | 159. | 15.3 | 705. |
| 10 | .380 | 163. | 15.2 | 692. |
| 11 | .390 | 168. | 15.2 | 699. |
| 12 | .390 | 168. | 15.2 | 700. |
| 13 | .380 | 163. | 15.3 | 689. |
| 14 | .380 | 163. | 15.4 | 694. |
| 15 | .380 | 163. | 15.4 | 692. |
| 16 | .380 | 163. | 15.4 | 685. |
| 17 | .370 | 159. | 15.5 | 679. |
| 18 | .380 | 163. | 15.5 | 680. |
| 19 | .390 | 168. | 15.5 | 683. |

| | | | | |
|---|---|---|---|---|
| 20 | .390 | 168. | 15.5 | 678. |
| 21 | .390 | 168. | 15.6 | 686. |
| 22 | .400 | 172. | 15.6 | 690. |
| 23 | .380 | 163. | 15.5 | 665. |
| 24 | .310 | 133. | 15.3 | 542. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 15.4 | 553. |
| 2 | .290 | 125. | 15.3 | 529. |
| 3 | .280 | 120. | 15.3 | 515. |
| 4 | .280 | 120. | 15.3 | 511. |
| 5 | .270 | 116. | 15.3 | 508. |
| 6 | .290 | 125. | 15.6 | 558. |
| 7 | .310 | 133. | 15.6 | 603. |
| 8 | .350 | 150. | 15.5 | 641. |
| 9 | .340 | 146. | 15.6 | 651. |
| 10 | .350 | 150. | 15.7 | 670. |
| 11 | .360 | 155. | 15.6 | 683. |
| 12 | .370 | 159. | 15.6 | 678. |
| 13 | .360 | 155. | 15.6 | 671. |
| 14 | .370 | 159. | 15.7 | 688. |
| 15 | .370 | 159. | 15.6 | 678. |
| 16 | .370 | 159. | 15.7 | 685. |
| 17 | .380 | 163. | 15.7 | 693. |
| 18 | .390 | 168. | 15.5 | 679. |
| 19 | .380 | 163. | 15.5 | 678. |
| 20 | .370 | 159. | 15.6 | 686. |
| 21 | .350 | 150. | 15.7 | 683. |
| 22 | .340 | 146. | 15.6 | 659. |
| 23 | .310 | 133. | 15.4 | 597. |
| 24 | .280 | 120. | 15.2 | 531. |

DAY = 61

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.1 | 451. |
| 2 | .250 | 107. | 15.2 | 445. |
| 3 | .240 | 103. | 15.3 | 455. |
| 4 | .240 | 103. | 15.2 | 474. |
| 5 | .250 | 107. | 15.1 | 488. |
| 6 | .270 | 116. | 15.1 | 526. |
| 7 | .300 | 129. | 15.3 | 617. |
| 8 | .330 | 142. | 15.3 | 658. |
| 9 | .360 | 155. | 15.4 | 694. |
| 10 | .370 | 159. | 15.3 | 693. |
| 11 | .380 | 163. | 15.2 | 693. |
| 12 | .380 | 163. | 15.2 | 687. |
| 13 | .380 | 163. | 15.3 | 680. |
| 14 | .370 | 159. | 15.3 | 691. |
| 15 | .370 | 159. | 15.2 | 670. |
| 16 | .360 | 155. | 15.4 | 680. |
| 17 | .350 | 150. | 15.3 | 671. |
| 18 | .350 | 150. | 15.4 | 688. |

| | | | | |
|---|---|---|---|---|
| 19 | .350 | 150. | 15.0 | 688. |
| 20 | .360 | 155. | 15.5 | 695. |
| 21 | .360 | 155. | 15.0 | 686. |
| 22 | .370 | 159. | 15.0 | 680. |
| 23 | .360 | 155. | 15.3 | 654. |
| 24 | .340 | 146. | 15.0 | 600. |

DAY = 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.1 | 524. |
| 2 | .280 | 120. | 15.1 | 517. |
| 3 | .290 | 125. | 15.1 | 515. |
| 4 | .290 | 125. | 15.1 | 514. |
| 5 | .290 | 125. | 15.1 | 525. |
| 6 | .280 | 120. | 15.3 | 547. |
| 7 | .320 | 137. | 15.5 | 639. |
| 8 | .350 | 150. | 15.4 | 683. |
| 9 | .360 | 155. | 15.3 | 689. |
| 10 | .370 | 159. | 15.3 | 689. |
| 11 | .360 | 155. | 15.2 | 672. |
| 12 | .370 | 159. | 15.3 | 683. |
| 13 | .370 | 159. | 15.3 | 689. |
| 14 | .350 | 150. | 15.5 | 690. |
| 15 | .340 | 146. | 15.5 | 672. |
| 16 | .340 | 146. | 15.5 | 681. |
| 17 | .340 | 146. | 15.4 | 685. |
| 18 | .350 | 150. | 15.3 | 679. |
| 19 | .360 | 155. | 15.4 | 691. |
| 20 | .350 | 150. | 15.3 | 669. |
| 21 | .360 | 155. | 15.4 | 692. |
| 22 | .360 | 155. | 15.3 | 682. |
| 23 | .320 | 137. | 15.1 | 598. |
| 24 | .280 | 120. | 14.8 | 508. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .190 | 82. | 14.6 | 377. |
| 2 | .170 | 73. | 14.9 | 361. |
| 3 | .170 | 73. | 14.9 | 380. |
| 4 | .170 | 73. | 15.1 | 399. |
| 5 | .220 | 95. | 15.0 | 452. |
| 6 | .290 | 125. | 15.0 | 533. |
| 7 | .310 | 133. | 15.2 | 591. |
| 8 | .340 | 146. | 15.4 | 674. |
| 9 | .360 | 155. | 15.3 | 699. |
| 10 | .360 | 155. | 15.3 | 699. |
| 11 | .360 | 155. | 15.2 | 698. |
| 12 | .370 | 159. | 15.2 | 698. |
| 13 | .370 | 159. | 15.2 | 687. |
| 14 | .360 | 155. | 15.3 | 686. |
| 15 | .350 | 150. | 15.3 | 686. |
| 16 | .350 | 150. | 15.3 | 684. |
| 17 | .350 | 150. | 15.3 | 659. |

| | | | | |
|---|---|---|---|---|
| 18 | .350 | 150. | 15.3 | 687. |
| 19 | .360 | 155. | 15.5 | 698. |
| 20 | .350 | 150. | 15.5 | 699. |
| 21 | .350 | 150. | 15.5 | 698. |
| 22 | .340 | 146. | 15.3 | 665. |
| 23 | .310 | 133. | 14.7 | 564. |
| 24 | .260 | 112. | 14.4 | 466. |

DAY = 65

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 14.6 | 445. |
| 2 | .240 | 103. | 14.8 | 471. |
| 3 | .230 | 99. | 14.7 | 464. |
| 4 | .240 | 103. | 14.7 | 458. |
| 5 | .240 | 103. | 14.8 | 476. |
| 6 | .260 | 112. | 15.1 | 551. |
| 7 | .330 | 142. | 15.1 | 622. |
| 8 | .360 | 155. | 15.2 | 677. |
| 9 | .360 | 155. | 15.2 | 689. |
| 10 | .360 | 155. | 15.3 | 688. |
| 11 | .360 | 155. | 15.3 | 688. |
| 12 | .350 | 150. | 15.4 | 689. |
| 13 | .340 | 146. | 15.5 | 689. |
| 14 | .340 | 146. | 15.5 | 688. |
| 15 | .350 | 150. | 15.5 | 688. |
| 16 | .350 | 150. | 15.5 | 688. |
| 17 | .360 | 155. | 15.5 | 688. |
| 18 | .360 | 155. | 15.5 | 689. |
| 19 | .370 | 159. | 15.4 | 688. |
| 20 | .370 | 159. | 15.5 | 689. |
| 21 | .370 | 159. | 15.4 | 689. |
| 22 | .360 | 155. | 15.3 | 664. |
| 23 | .330 | 142. | 15.0 | 583. |
| 24 | .300 | 129. | 14.9 | 520. |

DAY = 66

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 14.8 | 467. |
| 2 | .240 | 103. | 14.9 | 460. |
| 3 | .230 | 99. | 14.8 | 459. |
| 4 | .230 | 99. | 14.9 | 444. |
| 5 | .240 | 103. | 15.1 | 451. |
| 6 | .260 | 112. | 15.2 | 506. |
| 7 | .300 | 129. | 15.0 | 528. |
| 8 | .310 | 133. | 15.0 | 553. |
| 9 | .350 | 146. | 15.3 | 680. |
| 10 | .360 | 155. | 15.4 | 688. |
| 11 | .380 | 163. | 15.3 | 688. |
| 12 | .380 | 163. | 15.4 | 688. |
| 13 | .370 | 159. | 15.4 | 667. |
| 14 | .370 | 159. | 15.4 | 656. |
| 15 | .350 | 150. | 15.4 | 638. |
| 16 | .330 | 142. | 15.4 | 610. |

| | | | | |
|---|---|---|---|---|
| 17 | .330 | 142. | 15.5 | 618. |
| 18 | .350 | 150. | 15.6 | 671. |
| 19 | .360 | 155. | 15.5 | 683. |
| 20 | .380 | 163. | 15.5 | 682. |
| 21 | .380 | 163. | 15.5 | 682. |
| 22 | .360 | 155. | 15.4 | 659. |
| 23 | .350 | 150. | 15.3 | 625. |
| 24 | .330 | 142. | 15.0 | 574. |

DAY = 67

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 15.1 | 590. |
| 2 | .320 | 137. | 14.9 | 552. |
| 3 | .320 | 137. | 14.9 | 549. |
| 4 | .310 | 133. | 14.8 | 538. |
| 5 | .310 | 133. | 14.9 | 559. |
| 6 | .310 | 133. | 15.0 | 567. |
| 7 | .320 | 137. | 14.9 | 571. |
| 8 | .320 | 137. | 15.0 | 590. |
| 9 | .330 | 142. | 15.1 | 634. |
| 10 | .350 | 150. | 15.1 | 648. |
| 11 | .350 | 150. | 14.8 | 588. |
| 12 | .340 | 146. | 15.0 | 582. |
| 13 | .330 | 142. | 15.0 | 572. |
| 14 | .320 | 137. | 14.9 | 547. |
| 15 | .320 | 137. | 14.9 | 535. |
| 16 | .310 | 133. | 14.9 | 502. |
| 17 | .300 | 129. | 15.1 | 515. |
| 18 | .300 | 129. | 15.3 | 557. |
| 19 | .310 | 133. | 15.4 | 614. |
| 20 | .340 | 146. | 15.4 | 646. |
| 21 | .360 | 155. | 15.3 | 643. |
| 22 | .360 | 155. | 15.2 | 615. |
| 23 | .360 | 155. | 15.0 | 592. |
| 24 | .340 | 146. | 14.6 | 508. |

DAY = 68

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 14.8 | 467. |
| 2 | .270 | 116. | 14.9 | 459. |
| 3 | .250 | 107. | 14.9 | 434. |
| 4 | .250 | 107. | 15.0 | 452. |
| 5 | .260 | 112. | 15.1 | 468. |
| 6 | .310 | 133. | 15.1 | 542. |
| 7 | .350 | 150. | 15.2 | 628. |
| 8 | .380 | 163. | 15.3 | 676. |
| 9 | .380 | 163. | 15.2 | 679. |
| 10 | .380 | 163. | 15.2 | 685. |
| 11 | .390 | 168. | 15.2 | 688. |
| 12 | .390 | 168. | 15.2 | 686. |
| 13 | .400 | 172. | 15.2 | 688. |
| 14 | .390 | 168. | 15.3 | 690. |
| 15 | .400 | 172. | 15.4 | 693. |

| | | | | |
|---|---|---|---|---|
| 16 | .400 | 172. | 15.4 | 695. |
| 17 | .390 | 168. | 15.4 | 693. |
| 18 | .380 | 163. | 15.3 | 671. |
| 19 | .380 | 163. | 15.4 | 684. |
| 20 | .380 | 163. | 15.3 | 682. |
| 21 | .390 | 168. | 15.4 | 684. |
| 22 | .390 | 168. | 15.3 | 665. |
| 23 | .360 | 155. | 15.0 | 610. |
| 24 | .300 | 129. | 14.6 | 510. |

DAY = 71

| HOUR | NOx LB/10**6 BTU | NOx NG/J | Co2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 14.9 | 458. |
| 2 | .250 | 107. | 15.1 | 488. |
| 3 | .250 | 107. | 15.0 | 485. |
| 4 | .250 | 107. | 15.0 | 488. |
| 5 | .250 | 107. | 15.1 | 499. |
| 6 | .270 | 116. | 15.1 | 528. |
| 7 | .290 | 125. | 15.4 | 582. |
| 8 | .320 | 137. | 15.5 | 645. |
| 9 | .340 | 146. | 15.4 | 663. |
| 10 | .330 | 142. | 15.5 | 643. |
| 11 | .340 | 146. | 15.8 | 684. |
| 12 | .350 | 150. | 15.8 | 692. |
| 13 | .350 | 150. | 15.8 | 689. |
| 14 | .350 | 150. | 15.9 | 686. |
| 15 | .340 | 146. | 15.8 | 661. |
| 16 | .340 | 146. | 15.8 | 650. |
| 17 | .350 | 150. | 15.9 | 676. |
| 18 | .360 | 155. | 15.8 | 675. |
| 19 | .370 | 159. | 15.9 | 671. |
| 20 | .360 | 155. | 16.0 | 668. |
| 21 | .360 | 155. | 16.0 | 665. |
| 22 | .320 | 137. | 15.8 | 598. |
| 23 | .270 | 116. | 15.2 | 494. |
| 24 | .240 | 103. | 15.3 | 458. |

DAY = 72

| HOUR | NOx LB/10**6 BTU | NOx NG/J | Co2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 15.3 | 421. |
| 2 | .230 | 99. | 15.5 | 454. |
| 3 | .210 | 90. | 15.3 | 414. |
| 4 | .200 | 86. | 15.2 | 399. |
| 5 | .210 | 90. | 15.3 | 416. |
| 6 | .230 | 99. | 15.6 | 484. |
| 7 | .260 | 112. | 15.6 | 553. |
| 8 | .320 | 137. | 15.9 | 655. |
| 9 | .340 | 146. | 15.6 | 661. |
| 10 | .340 | 146. | 15.5 | 650. |
| 11 | .350 | 150. | 15.7 | 675. |
| 12 | .350 | 150. | 15.6 | 673. |
| 13 | .350 | 150. | 15.5 | 653. |
| 14 | .350 | 150. | 15.6 | 658. |

| | | | | |
|---|---|---|---|---|
| 15 | .340 | 146. | 15.6 | 636. |
| 16 | .360 | 155. | 15.8 | 666. |
| 17 | .370 | 159. | 15.6 | 676. |
| 18 | .360 | 155. | 15.6 | 660. |
| 19 | .370 | 159. | 15.8 | 670. |
| 20 | .370 | 159. | 15.7 | 674. |
| 21 | .370 | 159. | 15.7 | 655. |
| 22 | .360 | 155. | 15.6 | 626. |
| 23 | .320 | 137. | 15.2 | 569. |
| 24 | .260 | 112. | 14.9 | 488. |

DAY = 73

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 14.8 | 474. |
| 2 | .250 | 107. | 14.8 | 473. |
| 3 | .260 | 112. | 14.9 | 478. |
| 4 | .240 | 103. | 14.8 | 438. |
| 5 | .240 | 103. | 15.1 | 458. |
| 6 | .250 | 107. | 15.1 | 492. |
| 7 | .250 | 107. | 15.1 | 484. |
| 8 | .280 | 120. | 15.4 | 566. |
| 9 | .340 | 146. | 15.5 | 625. |
| 10 | .370 | 159. | 15.6 | 669. |
| 11 | .370 | 159. | 15.7 | 671. |
| 12 | .370 | 159. | 15.8 | 667. |
| 13 | .360 | 155. | 15.5 | 653. |
| 14 | .360 | 155. | 15.6 | 647. |
| 15 | .340 | 146. | 15.5 | 619. |
| 16 | .320 | 137. | 15.3 | 579. |
| 17 | .310 | 133. | 15.6 | 597. |
| 18 | .340 | 146. | 15.6 | 630. |
| 19 | .370 | 159. | 15.8 | 675. |
| 20 | .380 | 163. | 15.7 | 676. |
| 21 | .380 | 163. | 15.7 | 668. |
| 22 | .380 | 163. | 15.6 | 652. |
| 23 | .330 | 142. | 15.5 | 583. |
| 24 | .270 | 116. | 15.1 | 500. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 14.5 | 383. |
| 2 | .230 | 99. | 15.1 | 397. |
| 3 | .200 | 86. | 15.0 | 398. |
| 4 | .200 | 86. | 14.9 | 373. |
| 5 | .190 | 82. | 14.8 | 348. |
| 6 | .190 | 82. | 14.8 | 352. |
| 7 | .180 | 77. | 15.3 | 426. |
| 8 | .190 | 82. | 15.3 | 420. |
| 9 | .210 | 90. | 15.4 | 470. |
| 10 | .230 | 99. | 15.6 | 556. |
| 11 | .260 | 112. | 15.5 | 591. |
| 12 | .280 | 120. | 15.5 | 602. |
| 13 | .290 | 125. | 15.5 | 622. |

| | | | | |
|---|---|---|---|---|
| 14 | .300 | 129. | 15.4 | 609. |
| 15 | .300 | 129. | 15.4 | 597. |
| 16 | .300 | 129. | 15.5 | 596. |
| 17 | .300 | 129. | 15.5 | 581. |
| 18 | .310 | 133. | 15.6 | 604. |
| 19 | .310 | 133. | 15.9 | 617. |
| 20 | .330 | 142. | 15.7 | 671. |
| 21 | .350 | 150. | 15.6 | 669. |
| 22 | .360 | 155. | 15.5 | 641. |
| 23 | .350 | 150. | 15.3 | 551. |
| 24 | .320 | 137. | 15.2 | 495. |

DAY = 75

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.2 | 456. |
| 2 | .280 | 120. | 15.3 | 490. |
| 3 | .280 | 120. | 15.2 | 487. |
| 4 | .290 | 125. | 15.3 | 489. |
| 5 | .290 | 125. | 15.2 | 506. |
| 6 | .330 | 142. | 15.5 | 600. |
| 7 | .370 | 159. | 15.3 | 651. |
| 8 | .390 | 168. | 15.4 | 677. |
| 9 | .390 | 168. | 15.5 | 685. |
| 10 | .390 | 168. | 15.5 | 695. |
| 11 | .390 | 168. | 15.5 | 697. |
| 12 | .390 | 168. | 15.4 | 691. |
| 13 | .390 | 168. | 15.4 | 688. |
| 14 | .390 | 168. | 15.4 | 688. |
| 15 | .390 | 168. | 15.3 | 669. |
| 16 | .400 | 172. | 15.4 | 681. |
| 17 | .380 | 163. | 15.4 | 657. |
| 18 | .370 | 159. | 15.5 | 657. |
| 19 | .380 | 163. | 15.6 | 673. |
| 20 | .390 | 168. | 15.6 | 677. |
| 21 | .370 | 159. | 15.7 | 668. |
| 22 | .360 | 155. | 15.6 | 647. |
| 23 | .330 | 142. | 15.4 | 587. |
| 24 | .300 | 129. | 15.3 | 526. |

DAY = 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 15.3 | 501. |
| 2 | .270 | 116. | 15.3 | 501. |
| 3 | .250 | 107. | 15.3 | 478. |
| 4 | .250 | 107. | 15.3 | 469. |
| 5 | .250 | 107. | 15.4 | 482. |
| 6 | .300 | 129. | 15.6 | 577. |
| 7 | .350 | 150. | 15.7 | 643. |
| 8 | .370 | 159. | 15.7 | 683. |
| 9 | .350 | 150. | 15.7 | 680. |
| 10 | .360 | 155. | 15.8 | 694. |
| 11 | .370 | 159. | 16.0 | 703. |
| 12 | .370 | 159. | 16.0 | 704. |

| | | | | |
|---|---|---|---|---|
| 13 | .380 | 163. | 16.0 | 702. |
| 14 | .370 | 159. | 16.0 | 698. |
| 15 | .370 | 159. | 16.1 | 699. |
| 16 | .370 | 159. | 16.2 | 700. |
| 17 | .370 | 159. | 16.2 | 697. |
| 18 | .370 | 159. | 16.1 | 676. |
| 19 | .380 | 163. | 16.2 | 698. |
| 20 | .380 | 163. | 16.2 | 701. |
| 21 | .370 | 159. | 16.1 | 692. |
| 22 | .370 | 159. | 15.9 | 670. |
| 23 | .350 | 150. | 15.8 | 643. |
| 24 | .320 | 137. | 15.7 | 596. |

DAY = 77

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 15.6 | 558. |
| 2 | .260 | 112. | 15.5 | 502. |
| 3 | .250 | 107. | 15.7 | 510. |
| 4 | .240 | 103. | 15.3 | 467. |
| 5 | .250 | 107. | 15.5 | 487. |
| 6 | .270 | 116. | 15.6 | 531. |
| 7 | .350 | 150. | 15.6 | 647. |
| 8 | .370 | 159. | 15.8 | 686. |
| 9 | .370 | 159. | 15.7 | 700. |
| 10 | .380 | 163. | 15.8 | 695. |
| 11 | .380 | 163. | 15.7 | 697. |
| 12 | .390 | 168. | 15.4 | 700. |
| 13 | .400 | 172. | 15.5 | 700. |
| 14 | .400 | 172. | 15.5 | 700. |
| 15 | .400 | 172. | 15.5 | 699. |
| 16 | .400 | 172. | 15.5 | 700. |
| 17 | .400 | 172. | 15.6 | 699. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .410 | 176. | 15.6 | 706. |
| 21 | .410 | 176. | 15.6 | 709. |
| 22 | .400 | 172. | 15.4 | 690. |
| 23 | .370 | 159. | 15.2 | 639. |
| 24 | .320 | 137. | 15.1 | 559. |

DAY = 78

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 15.3 | 573. |
| 2 | .320 | 137. | 15.1 | 559. |
| 3 | .310 | 133. | 15.1 | 543. |
| 4 | .300 | 129. | 15.1 | 540. |
| 5 | .310 | 133. | 15.2 | 554. |
| 6 | .330 | 142. | 15.4 | 605. |
| 7 | .370 | 159. | 15.5 | 681. |
| 8 | .390 | 168. | 15.4 | 689. |
| 9 | .400 | 172. | 15.4 | 693. |
| 10 | .400 | 172. | 15.4 | 703. |
| 11 | .380 | 163. | 15.4 | 702. |

| | | | | |
|---|---|---|---|---|
| 12 | .380 | 163. | 15.5 | 702. |
| 13 | .380 | 163. | 14.8 | 703. |
| 14 | .370 | 159. | 15.5 | 702. |
| 15 | .340 | 146. | 15.8 | 689. |
| 16 | .340 | 146. | 15.6 | 684. |
| 17 | .350 | 150. | 15.6 | 687. |
| 18 | .350 | 150. | 15.7 | 682. |
| 19 | .360 | 155. | 15.6 | 681. |
| 20 | .370 | 159. | 15.7 | 699. |
| 21 | .370 | 159. | 15.7 | 691. |
| 22 | .370 | 159. | 15.6 | 688. |
| 23 | .340 | 146. | 15.4 | 625. |
| 24 | .250 | 107. | 14.9 | 477. |

DAY = 79

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 15.2 | 439. |
| 2 | .210 | 90. | 15.2 | 433. |
| 3 | .200 | 86. | 15.2 | 422. |
| 4 | .200 | 86. | 15.2 | 431. |
| 5 | .210 | 90. | 15.3 | 445. |
| 6 | .250 | 107. | 15.5 | 531. |
| 7 | .320 | 137. | 15.6 | 636. |
| 8 | .350 | 150. | 15.5 | 677. |
| 9 | .360 | 155. | 15.5 | 693. |
| 10 | .360 | 155. | 15.3 | 677. |
| 11 | .360 | 155. | 15.3 | 686. |
| 12 | .350 | 150. | 15.4 | 683. |
| 13 | .330 | 142. | 15.4 | 658. |
| 14 | .340 | 146. | 15.5 | 674. |
| 15 | .340 | 146. | 15.4 | 679. |
| 16 | .340 | 146. | 15.4 | 669. |
| 17 | .340 | 146. | 15.3 | 664. |
| 18 | .350 | 150. | 15.4 | 674. |
| 19 | .360 | 155. | 15.4 | 683. |
| 20 | .350 | 150. | 15.4 | 671. |
| 21 | .340 | 146. | 15.5 | 669. |
| 22 | .350 | 150. | 15.4 | 666. |
| 23 | .330 | 142. | 15.5 | 644. |
| 24 | .300 | 129. | 15.1 | 563. |

DAY = 80

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 14.8 | 445. |
| 2 | .220 | 95. | 15.0 | 414. |
| 3 | .210 | 90. | 15.2 | 413. |
| 4 | .200 | 86. | 15.2 | 417. |
| 5 | .220 | 95. | 15.4 | 479. |
| 6 | .290 | 125. | 15.5 | 581. |
| 7 | .310 | 133. | 15.6 | 618. |
| 8 | .320 | 137. | 15.7 | 644. |
| 9 | .340 | 146. | 15.7 | 697. |
| 10 | .350 | 150. | 15.6 | 700. |

| | | | | |
|---|---|---|---|---|
| 11 | .350 | 150. | 15.7 | 700. |
| 12 | .360 | 155. | 15.5 | 698. |
| 13 | .350 | 150. | 15.4 | 682. |
| 14 | .360 | 155. | 15.4 | 683. |
| 15 | .350 | 150. | 15.4 | 678. |
| 16 | .350 | 150. | 15.4 | 688. |
| 17 | .350 | 150. | 15.5 | 695. |
| 18 | .360 | 155. | 15.5 | 699. |
| 19 | .360 | 155. | 15.4 | 692. |
| 20 | .370 | 159. | 15.3 | 681. |
| 21 | .370 | 159. | 15.4 | 681. |
| 22 | .360 | 155. | 15.4 | 681. |
| 23 | .360 | 155. | 15.2 | 663. |
| 24 | .350 | 150. | 15.3 | 666. |

DAY = 81

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 15.3 | 625. |
| 2 | .330 | 142. | 15.4 | 613. |
| 3 | .290 | 125. | 15.1 | 554. |
| 4 | .280 | 120. | 15.2 | 533. |
| 5 | .270 | 116. | 15.2 | 534. |
| 6 | .270 | 116. | 15.3 | 547. |
| 7 | .270 | 116. | 15.2 | 523. |
| 8 | .270 | 116. | 15.4 | 548. |
| 9 | .300 | 129. | 15.4 | 596. |
| 10 | .300 | 129. | 15.3 | 589. |
| 11 | .320 | 137. | 15.4 | 605. |
| 12 | .300 | 129. | 15.4 | 599. |
| 13 | .280 | 120. | 15.3 | 584. |
| 14 | .270 | 116. | 15.2 | 563. |
| 15 | .260 | 112. | 15.2 | 538. |
| 16 | .260 | 112. | 15.1 | 526. |
| 17 | .260 | 112. | 15.2 | 531. |
| 18 | .300 | 129. | 15.6 | 585. |
| 19 | .350 | 150. | 15.8 | 666. |
| 20 | .370 | 159. | 15.7 | 698. |
| 21 | .360 | 155. | 15.8 | 684. |
| 22 | .350 | 150. | 15.7 | 659. |
| 23 | .310 | 133. | 15.4 | 586. |
| 24 | .280 | 120. | 15.3 | 503. |

DAY = 83

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.0 | 418. |
| 2 | .240 | 103. | 15.1 | 395. |
| 3 | .230 | 99. | 15.2 | 389. |
| 4 | .230 | 99. | 15.0 | 360. |
| 5 | .230 | 99. | 15.3 | 400. |
| 6 | .270 | 116. | 15.5 | 497. |
| 7 | .340 | 146. | 15.5 | 588. |
| 8 | .380 | 163. | 15.6 | 660. |
| 9 | .380 | 163. | 15.4 | 672. |

| | | | | |
|---|---|---|---|---|
| 10 | .380 | 163. | 15.8 | 681. |
| 11 | .360 | 155. | 15.4 | 647. |
| 12 | .360 | 155. | 15.5 | 651. |
| 13 | .360 | 155. | 15.5 | 630. |
| 14 | .370 | 159. | 15.6 | 654. |
| 15 | .370 | 159. | 15.6 | 641. |
| 16 | .360 | 155. | 15.6 | 644. |
| 17 | .320 | 137. | 15.9 | 645. |
| 18 | .320 | 137. | 15.9 | 647. |
| 19 | .330 | 142. | 16.0 | 656. |
| 20 | .340 | 146. | 16.1 | 678. |
| 21 | .340 | 146. | 15.8 | 661. |
| 22 | .350 | 150. | 15.5 | 628. |
| 23 | .330 | 142. | 15.8 | 612. |
| 24 | .290 | 125. | 16.0 | 559. |

DAY = 85

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 15.8 | 457. |
| 2 | .230 | 99. | 16.0 | 435. |
| 3 | .230 | 99. | 16.2 | 452. |
| 4 | .230 | 99. | 16.0 | 447. |
| 5 | .230 | 99. | 15.9 | 434. |
| 6 | .250 | 107. | 16.2 | 491. |
| 7 | .300 | 129. | 16.6 | 604. |
| 8 | .340 | 146. | 16.5 | 662. |
| 9 | .360 | 155. | 16.3 | 678. |
| 10 | .350 | 150. | 16.3 | 678. |
| 11 | .350 | 150. | 16.4 | 684. |
| 12 | .360 | 155. | 16.3 | 693. |
| 13 | .370 | 159. | 16.3 | 689. |
| 14 | .360 | 155. | 16.5 | 693. |
| 15 | .360 | 155. | 16.7 | 697. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | .380 | 163. | 16.8 | 688. |
| 20 | .380 | 163. | 16.7 | 680. |
| 21 | .380 | 163. | 16.6 | 676. |
| 22 | .380 | 163. | 16.2 | 654. |
| 23 | .350 | 150. | 16.2 | 629. |
| 24 | .310 | 133. | 15.6 | 520. |

DAY = 86

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 15.9 | 488. |
| 2 | .250 | 107. | 15.8 | 414. |
| 3 | .240 | 103. | 15.8 | 394. |
| 4 | .230 | 99. | 15.8 | 370. |
| 5 | .220 | 95. | 15.9 | 379. |
| 6 | .230 | 99. | 16.1 | 436. |
| 7 | .290 | 125. | 16.5 | 588. |
| 8 | .340 | 146. | 16.5 | 669. |

| | | | | |
|---|---|---|---|---|
| 9 | .360 | 155. | 16.3 | 688. |
| 10 | .350 | 150. | 16.2 | 681. |
| 11 | .360 | 155. | 16.3 | 692. |
| 12 | .360 | 155. | 16.3 | 693. |
| 13 | .360 | 155. | 16.4 | 695. |
| 14 | .360 | 155. | 16.3 | 686. |
| 15 | .360 | 155. | 16.2 | 684. |
| 16 | .360 | 155. | 16.3 | 679. |
| 17 | .330 | 142. | 16.4 | 683. |
| 18 | .320 | 137. | 16.4 | 651. |
| 19 | .320 | 137. | 16.5 | 670. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .340 | 146. | 16.1 | 684. |
| 22 | .340 | 146. | 16.3 | 676. |
| 23 | .340 | 146. | 16.3 | 665. |
| 24 | .310 | 133. | 16.2 | 605. |

DAY = 87

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 16.2 | 574. |
| 2 | .280 | 120. | 16.3 | 561. |
| 3 | .270 | 116. | 16.3 | 553. |
| 4 | .270 | 116. | 16.2 | 535. |
| 5 | .250 | 107. | 16.1 | 507. |
| 6 | .240 | 103. | 16.4 | 500. |
| 7 | .230 | 99. | 16.4 | 483. |
| 8 | .240 | 103. | 16.8 | 529. |
| 9 | .290 | 125. | 16.9 | 611. |
| 10 | .310 | 133. | 16.8 | 644. |
| 11 | .300 | 129. | 16.9 | 643. |
| 12 | .300 | 129. | 16.8 | 640. |
| 13 | .300 | 129. | 16.8 | 625. |
| 14 | .300 | 129. | 16.9 | 629. |
| 15 | .300 | 129. | 16.9 | 619. |
| 16 | .300 | 129. | 17.0 | 622. |
| 17 | .300 | 129. | 16.9 | 623. |
| 18 | .300 | 129. | 16.8 | 630. |
| 19 | .300 | 129. | 16.9 | 649. |
| 20 | .300 | 129. | 16.8 | 638. |
| 21 | .300 | 129. | 16.7 | 645. |
| 22 | .300 | 129. | 16.7 | 639. |
| 23 | .310 | 133. | 16.4 | 597. |
| 24 | .290 | 125. | 16.2 | 513. |

DAY = 91

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 15.7 | 479. |
| 2 | .240 | 103. | 15.8 | 489. |
| 3 | .240 | 103. | 15.8 | 488. |
| 4 | .240 | 103. | 15.7 | 474. |
| 5 | .240 | 103. | 15.8 | 486. |
| 6 | .260 | 112. | 15.9 | 508. |
| 7 | .260 | 112. | 15.8 | 535. |

| | | | | |
|---|---|---|---|---|
| 8 | .290 | 125. | 16.1 | 621. |
| 9 | .320 | 137. | 15.9 | 661. |
| 10 | .310 | 133. | 15.2 | 587. |
| 11 | .280 | 120. | 15.2 | 574. |
| 12 | .320 | 137. | 13.0 | 567. |
| 13 | .330 | 142. | 12.2 | 555. |
| 14 | .300 | 129. | 14.4 | 578. |
| 15 | .320 | 137. | 15.3 | 630. |
| 16 | .320 | 137. | 15.4 | 649. |
| 17 | .320 | 137. | 15.2 | 642. |
| 18 | .310 | 133. | 15.4 | 627. |
| 19 | .320 | 137. | 15.7 | 650. |
| 20 | .340 | 146. | 15.7 | 684. |
| 21 | .340 | 146. | 15.7 | 683. |
| 22 | .340 | 146. | 15.6 | 665. |
| 23 | .300 | 129. | 15.6 | 592. |
| 24 | .260 | 112. | 15.3 | 509. |

DAY = 92

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 15.6 | 487. |
| 2 | .270 | 116. | 15.7 | 513. |
| 3 | .260 | 112. | 15.6 | 517. |
| 4 | .240 | 103. | 15.7 | 499. |
| 5 | .260 | 112. | 15.6 | 511. |
| 6 | .270 | 116. | 15.7 | 552. |
| 7 | .300 | 129. | 15.8 | 592. |
| 8 | .320 | 137. | 15.8 | 639. |
| 9 | .340 | 146. | 15.7 | 665. |
| 10 | .340 | 146. | 15.9 | 674. |
| 11 | .330 | 142. | 15.8 | 687. |
| 12 | .330 | 142. | 15.9 | 663. |
| 13 | .320 | 137. | 16.0 | 666. |
| 14 | .330 | 142. | 15.9 | 671. |
| 15 | .330 | 142. | 15.9 | 666. |
| 16 | .330 | 142. | 15.9 | 664. |
| 17 | .320 | 137. | 16.1 | 639. |
| 18 | .290 | 125. | 16.5 | 604. |
| 19 | .300 | 129. | 16.7 | 614. |
| 20 | .320 | 137. | 16.6 | 663. |
| 21 | .310 | 133. | 16.9 | 644. |
| 22 | .280 | 120. | 16.8 | 582. |
| 23 | .260 | 112. | 16.8 | 509. |
| 24 | .250 | 107. | 16.4 | 483. |

DAY = 93

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 16.5 | 515. |
| 2 | .230 | 99. | 16.2 | 459. |
| 3 | .230 | 99. | 16.2 | 448. |
| 4 | .230 | 99. | 16.3 | 456. |
| 5 | .230 | 99. | 16.2 | 455. |
| 6 | .230 | 99. | 16.2 | 470. |

| | | | | |
|---|---|---|---|---|
| 7 | .240 | 103. | 16.3 | 512. |
| 8 | .280 | 120. | 16.9 | 622. |
| 9 | .300 | 129. | 16.9 | 669. |
| 10 | .300 | 129. | 16.8 | 680. |
| 11 | .310 | 133. | 16.7 | 672. |
| 12 | .290 | 125. | 16.9 | 682. |
| 13 | .300 | 129. | 16.8 | 665. |
| 14 | .290 | 125. | 17.0 | 678. |
| 15 | .290 | 125. | 17.0 | 670. |
| 16 | .300 | 129. | 16.9 | 671. |
| 17 | .300 | 129. | 16.7 | 672. |
| 18 | .310 | 133. | 16.3 | 658. |
| 19 | .310 | 133. | 16.1 | 642. |
| 20 | .320 | 137. | 16.1 | 652. |
| 21 | .320 | 137. | 16.1 | 665. |
| 22 | .320 | 137. | 16.1 | 675. |
| 23 | .300 | 129. | 15.8 | 617. |
| 24 | .240 | 103. | 15.6 | 471. |

DAY = 95

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 16.0 | 635. |
| 2 | .330 | 142. | 16.0 | 654. |
| 3 | .310 | 133. | 15.9 | 639. |
| 4 | .310 | 133. | 15.8 | 627. |
| 5 | .310 | 133. | 15.8 | 620. |
| 6 | .290 | 125. | 16.0 | 609. |
| 7 | .290 | 125. | 15.9 | 597. |
| 8 | .290 | 125. | 15.7 | 594. |
| 9 | .300 | 129. | 15.8 | 610. |
| 10 | .310 | 133. | 15.9 | 645. |
| 11 | .300 | 129. | 16.0 | 637. |
| 12 | .310 | 133. | 16.1 | 659. |
| 13 | .320 | 137. | 15.8 | 645. |
| 14 | .280 | 120. | 15.8 | 590. |
| 15 | .260 | 112. | 15.9 | 575. |
| 16 | .260 | 112. | 15.8 | 560. |
| 17 | .270 | 116. | 15.9 | 577. |
| 18 | .300 | 129. | 16.0 | 616. |
| 19 | .320 | 137. | 15.9 | 620. |
| 20 | .340 | 146. | 15.8 | 640. |
| 21 | .330 | 142. | 16.0 | 640. |
| 22 | .320 | 137. | 16.1 | 639. |
| 23 | .310 | 133. | 16.2 | 619. |
| 24 | .270 | 116. | 15.9 | 559. |

DAY = 96

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 16.2 | 576. |
| 2 | .270 | 116. | 16.1 | 575. |
| 3 | .290 | 125. | 16.1 | 604. |
| 4 | .300 | 129. | 16.0 | 612. |
| 5 | .290 | 125. | 16.2 | 615. |

| | | | | |
|---|---|---|---|---|
| 6 | .300 | 129. | 16.1 | 628. |
| 7 | .290 | 125. | 16.1 | 622. |
| 8 | .300 | 129. | 16.2 | 645. |
| 9 | .310 | 133. | 16.0 | 647. |
| 10 | .330 | 142. | 16.0 | 662. |
| 11 | .330 | 142. | 16.2 | 681. |
| 12 | .340 | 146. | 16.2 | 702. |
| 13 | .330 | 142. | 16.2 | 693. |
| 14 | .330 | 142. | 16.1 | 675. |
| 15 | .310 | 133. | 16.1 | 645. |
| 16 | .320 | 137. | 16.2 | 659. |
| 17 | .310 | 133. | 15.9 | 615. |
| 18 | .320 | 137. | 16.4 | 658. |
| 19 | .320 | 137. | 16.4 | 667. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .330 | 142. | 16.4 | 669. |
| 22 | .310 | 133. | 16.1 | 600. |
| 23 | .270 | 116. | 16.2 | 540. |
| 24 | .240 | 103. | 15.9 | 484. |

DAY = 97

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 16.3 | 506. |
| 2 | .220 | 95. | 16.3 | 516. |
| 3 | .240 | 103. | 16.4 | 529. |
| 4 | .260 | 112. | 16.3 | 552. |
| 5 | .260 | 112. | 16.4 | 563. |
| 6 | .300 | 129. | 16.1 | 590. |
| 7 | .300 | 129. | 16.4 | 642. |
| 8 | .300 | 129. | 16.4 | 642. |
| 9 | .290 | 125. | 16.2 | 601. |
| 10 | .310 | 133. | 16.4 | 661. |
| 11 | .310 | 133. | 16.4 | 677. |
| 12 | .310 | 133. | 16.5 | 687. |
| 13 | .310 | 133. | 16.4 | 666. |
| 14 | .330 | 142. | 16.4 | 675. |
| 15 | .330 | 142. | 16.4 | 670. |
| 16 | .300 | 129. | 16.5 | 641. |
| 17 | .310 | 133. | 16.7 | 664. |
| 18 | .320 | 137. | 16.5 | 675. |
| 19 | .320 | 137. | 16.6 | 672. |
| 20 | .320 | 137. | 16.7 | 675. |
| 21 | .320 | 137. | 16.7 | 669. |
| 22 | .330 | 142. | 16.5 | 647. |
| 23 | .290 | 125. | 16.1 | 571. |
| 24 | .260 | 112. | 16.2 | 519. |

DAY = 99

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 15.9 | 476. |
| 2 | .220 | 95. | 15.6 | 480. |
| 3 | .190 | 82. | 15.7 | 420. |
| 4 | .200 | 86. | 15.8 | 426. |

| | | | | |
|---|---|---|---|---|
| 5 | .200 | 86. | 15.7 | 430. |
| 6 | .250 | 107. | 16.2 | 555. |
| 7 | .280 | 120. | 16.3 | 627. |
| 8 | .310 | 133. | 16.0 | 636. |
| 9 | .300 | 129. | 16.3 | 667. |
| 10 | .300 | 129. | 16.2 | 671. |
| 11 | .320 | 137. | 16.1 | 676. |
| 12 | .300 | 129. | 16.2 | 669. |
| 13 | .310 | 133. | 16.3 | 664. |
| 14 | .310 | 133. | 16.2 | 655. |
| 15 | .310 | 133. | 16.1 | 660. |
| 16 | .300 | 129. | 16.2 | 642. |
| 17 | .300 | 129. | 15.9 | 622. |
| 18 | .270 | 116. | 15.9 | 569. |
| 19 | .280 | 120. | 16.4 | 592. |
| 20 | .300 | 129. | 16.6 | 663. |
| 21 | .300 | 129. | 16.5 | 666. |
| 22 | .300 | 129. | 16.4 | 653. |
| 23 | .280 | 120. | 16.1 | 564. |
| 24 | .280 | 120. | 16.1 | 535. |

DAY = 100

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 15.8 | 500. |
| 2 | .240 | 103. | 15.4 | 439. |
| 3 | .230 | 99. | 15.4 | 412. |
| 4 | .240 | 103. | 15.5 | 439. |
| 5 | .240 | 103. | 15.5 | 445. |
| 6 | .250 | 107. | 15.8 | 498. |
| 7 | .250 | 107. | 16.1 | 549. |
| 8 | .280 | 120. | 16.2 | 613. |
| 9 | .300 | 129. | 16.5 | 681. |
| 10 | .290 | 125. | 16.5 | 680. |
| 11 | .290 | 125. | 16.3 | 662. |
| 12 | .300 | 129. | 16.3 | 668. |
| 13 | .300 | 129. | 16.4 | 680. |
| 14 | .300 | 129. | 16.5 | 686. |
| 15 | .290 | 125. | 16.3 | 640. |
| 16 | .280 | 120. | 16.3 | 626. |
| 17 | .290 | 125. | 16.4 | 645. |
| 18 | .290 | 125. | 16.5 | 624. |
| 19 | .290 | 125. | 16.7 | 643. |
| 20 | .300 | 129. | 16.9 | 642. |
| 21 | .300 | 129. | 16.8 | 623. |
| 22 | .280 | 120. | 16.6 | 538. |
| 23 | .240 | 103. | 15.9 | 376. |
| 24 | .120 | 52. | 12.4 | 116. |

DAY = 105

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .190 | 82. | 15.3 | 299. |
| 2 | .210 | 90. | 15.3 | 281. |
| 3 | .210 | 90. | 15.3 | 281. |

| | | | | |
|---|---|---|---|---|
| 4 | .200 | 86. | 15.3 | 279. |
| 5 | .180 | 77. | 15.6 | 280. |
| 6 | .170 | 73. | 15.7 | 283. |
| 7 | .190 | 82. | 16.3 | 344. |
| 8 | .220 | 95. | 16.8 | 450. |
| 9 | .240 | 103. | 16.5 | 495. |
| 10 | .250 | 107. | 16.2 | 487. |
| 11 | .250 | 107. | 16.2 | 485. |
| 12 | .230 | 99. | 16.5 | 495. |
| 13 | .250 | 107. | 16.7 | 508. |
| 14 | .260 | 112. | 16.5 | 545. |
| 15 | .240 | 103. | 16.5 | 504. |
| 16 | .230 | 99. | 16.8 | 492. |
| 17 | .230 | 99. | 16.6 | 506. |
| 18 | .230 | 99. | 16.5 | 516. |
| 19 | .260 | 112. | 16.8 | 566. |
| 20 | .280 | 120. | 16.8 | 584. |
| 21 | .280 | 120. | 16.8 | 589. |
| 22 | .270 | 116. | 16.6 | 560. |
| 23 | .250 | 107. | 16.9 | 512. |
| 24 | .240 | 103. | 16.2 | 482. |

DAY = 106

| HOUR | NOX LB/10**6 BTU | NOX NG/J | Co2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 16.0 | 415. |
| 2 | .230 | 99. | 16.6 | 473. |
| 3 | .250 | 107. | 16.6 | 511. |
| 4 | .240 | 103. | 16.9 | 487. |
| 5 | .240 | 103. | 16.9 | 498. |
| 6 | .230 | 99. | 16.8 | 500. |
| 7 | .240 | 103. | 16.8 | 515. |
| 8 | .260 | 112. | 16.8 | 571. |
| 9 | .260 | 112. | 17.0 | 612. |
| 10 | .280 | 120. | 17.3 | 670. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .310 | 133. | 16.8 | 662. |
| 13 | .320 | 137. | 17.2 | 679. |
| 14 | .320 | 137. | 17.1 | 662. |
| 15 | .310 | 133. | 17.3 | 667. |
| 16 | .330 | 142. | 17.1 | 657. |
| 17 | .340 | 146. | 17.2 | 676. |
| 18 | .330 | 142. | 17.2 | 665. |
| 19 | .310 | 133. | 17.1 | 635. |
| 20 | .330 | 142. | 17.4 | 659. |
| 21 | .330 | 142. | 17.4 | 664. |
| 22 | .310 | 133. | 17.2 | 625. |
| 23 | .290 | 125. | 17.0 | 585. |
| 24 | .290 | 125. | 17.2 | 582. |

DAY = 108

| HOUR | NOX LB/10**6 BTU | NOX NG/J | Co2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 16.9 | 513. |
| 2 | .230 | 99. | 16.8 | 461. |

| | | | | |
|---|---|---|---|---|
| 3 | .230 | 99. | 16.9 | 474. |
| 4 | .220 | 95. | 16.8 | 447. |
| 5 | .220 | 95. | 16.8 | 455. |
| 6 | .210 | 90. | 16.7 | 430. |
| 7 | .220 | 95. | 16.9 | 470. |
| 8 | .260 | 112. | 17.2 | 575. |
| 9 | .310 | 133. | 17.4 | 655. |
| 10 | .320 | 137. | 17.3 | 656. |
| 11 | .320 | 137. | 17.2 | 661. |
| 12 | .330 | 142. | 17.0 | 656. |
| 13 | .330 | 142. | 17.0 | 657. |
| 14 | .330 | 142. | 17.0 | 649. |
| 15 | .330 | 142. | 17.2 | 662. |
| 16 | .310 | 133. | 16.9 | 623. |
| 17 | .320 | 137. | 17.3 | 670. |
| 18 | .320 | 137. | 17.4 | 674. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .310 | 133. | 17.4 | 666. |
| 21 | .340 | 146. | 17.1 | 677. |
| 22 | .330 | 142. | 17.1 | 661. |
| 23 | .330 | 142. | 17.1 | 652. |
| 24 | .300 | 129. | 16.8 | 577. |

DAY = 110

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 16.8 | 647. |
| 2 | .320 | 137. | 16.8 | 637. |
| 3 | .320 | 137. | 16.7 | 629. |
| 4 | .290 | 125. | 16.4 | 568. |
| 5 | .290 | 125. | 16.5 | 560. |
| 6 | .320 | 137. | 16.8 | 648. |
| 7 | .310 | 133. | 16.9 | 643. |
| 8 | .300 | 129. | 17.2 | 671. |
| 9 | .310 | 133. | 17.2 | 680. |
| 10 | .310 | 133. | 17.2 | 678. |
| 11 | .320 | 137. | 17.1 | 684. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .320 | 137. | 17.1 | 678. |
| 14 | .320 | 137. | 17.0 | 676. |
| 15 | .320 | 137. | 17.0 | 682. |
| 16 | .320 | 137. | 17.0 | 670. |
| 17 | .310 | 133. | 17.0 | 659. |
| 18 | .310 | 133. | 17.0 | 657. |
| 19 | .310 | 133. | 17.1 | 658. |
| 20 | .310 | 133. | 17.1 | 655. |
| 21 | .310 | 133. | 17.1 | 652. |
| 22 | .320 | 137. | 17.0 | 654. |
| 23 | .320 | 137. | 16.9 | 642. |
| 24 | .310 | 133. | 17.0 | 643. |

DAY = 111

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 17.0 | 650. |

| | | | | |
|---|---|---|---|---|
| 2 | .310 | 133. | 17.0 | 635. |
| 3 | .290 | 125. | 16.9 | 607. |
| 4 | .300 | 129. | 17.0 | 623. |
| 5 | .310 | 133. | 17.0 | 637. |
| 6 | .310 | 133. | 16.9 | 629. |
| 7 | .320 | 137. | 17.0 | 648. |
| 8 | .330 | 142. | 17.1 | 689. |
| 9 | .330 | 142. | 16.9 | 692. |
| 10 | .320 | 137. | 16.8 | 665. |
| 11 | .300 | 129. | 16.8 | 647. |
| 12 | .330 | 142. | 16.8 | 674. |
| 13 | .320 | 137. | 16.8 | 650. |
| 14 | .330 | 142. | 16.8 | 672. |
| 15 | .310 | 133. | 17.1 | 668. |
| 16 | .310 | 133. | 17.0 | 663. |
| 17 | .320 | 137. | 16.9 | 666. |
| 18 | .330 | 142. | 16.7 | 667. |
| 19 | .320 | 137. | 16.9 | 661. |
| 20 | .320 | 137. | 17.1 | 680. |
| 21 | .320 | 137. | 17.0 | 680. |
| 22 | .320 | 137. | 16.9 | 643. |
| 23 | .320 | 137. | 17.0 | 649. |
| 24 | .320 | 137. | 16.9 | 644. |

DAY = 112

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 16.9 | 638. |
| 2 | .320 | 137. | 17.1 | 656. |
| 3 | .320 | 137. | 17.0 | 653. |
| 4 | .320 | 137. | 17.0 | 643. |
| 5 | .320 | 137. | 17.0 | 656. |
| 6 | .330 | 142. | 17.0 | 675. |
| 7 | .340 | 146. | 16.9 | 678. |
| 8 | .350 | 150. | 16.9 | 689. |
| 9 | .340 | 146. | 17.0 | 689. |
| 10 | .340 | 146. | 17.0 | 690. |
| 11 | .330 | 142. | 17.0 | 687. |
| 12 | .330 | 142. | 17.0 | 686. |
| 13 | .330 | 142. | 16.9 | 684. |
| 14 | .330 | 142. | 16.8 | 687. |
| 15 | .330 | 142. | 16.9 | 686. |
| 16 | .330 | 142. | 17.0 | 686. |
| 17 | .300 | 129. | 16.9 | 680. |
| 18 | .320 | 137. | 16.8 | 640. |
| 19 | .320 | 137. | 16.9 | 628. |
| 20 | .330 | 142. | 17.0 | 658. |
| 21 | .330 | 142. | 17.0 | 658. |
| 22 | .330 | 142. | 17.0 | 642. |
| 23 | .320 | 137. | 17.1 | 653. |
| 24 | .280 | 120. | 16.6 | 563. |

DAY = 113

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .260 | 112. | 16.2 | 473. |
| 2 | .200 | 86. | 15.9 | 362. |
| 3 | .180 | 77. | 16.4 | 361. |
| 4 | .190 | 82. | 16.1 | 342. |
| 5 | .180 | 77. | 16.1 | 342. |
| 6 | .200 | 86. | 16.4 | 406. |
| 7 | .200 | 86. | 16.6 | 488. |
| 8 | .270 | 116. | 16.7 | 559. |
| 9 | .310 | 133. | 16.8 | 662. |
| 10 | .310 | 133. | 16.5 | 667. |
| 11 | .300 | 129. | 16.7 | 658. |
| 12 | .300 | 129. | 16.8 | 672. |
| 13 | .280 | 120. | 16.7 | 619. |
| 14 | .280 | 120. | 16.9 | 637. |
| 15 | .280 | 120. | 17.0 | 634. |
| 16 | .290 | 125. | 17.0 | 630. |
| 17 | .290 | 125. | 17.4 | 670. |
| 18 | .290 | 125. | 17.1 | 645. |
| 19 | .280 | 120. | 16.6 | 616. |
| 20 | .300 | 129. | 16.9 | 667. |
| 21 | .300 | 129. | 17.7 | 665. |
| 22 | .280 | 120. | 17.7 | 616. |
| 23 | .300 | 129. | 17.8 | 666. |
| 24 | .290 | 125. | 17.5 | 616. |

DAY = 114

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 112. | 17.6 | 585. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .210 | 90. | 17.0 | 456. |
| 4 | .210 | 90. | 17.3 | 470. |
| 5 | .220 | 95. | 17.4 | 497. |
| 6 | .240 | 103. | 17.3 | 513. |
| 7 | .250 | 107. | 17.2 | 536. |
| 8 | .260 | 112. | 17.5 | 593. |
| 9 | .280 | 120. | 17.6 | 638. |
| 10 | .280 | 120. | 17.6 | 654. |
| 11 | .290 | 125. | 17.6 | 674. |
| 12 | .300 | 129. | 17.6 | 688. |
| 13 | .310 | 133. | 17.6 | 690. |
| 14 | .300 | 129. | 17.5 | 670. |
| 15 | .300 | 129. | 17.8 | 681. |
| 16 | .300 | 129. | 17.8 | 685. |
| 17 | .300 | 129. | 17.8 | 669. |
| 18 | .300 | 129. | 17.9 | 678. |
| 19 | .300 | 129. | 17.6 | 656. |
| 20 | .310 | 133. | 17.5 | 652. |
| 21 | .320 | 137. | 17.8 | 682. |
| 22 | .310 | 133. | 18.1 | 676. |
| 23 | .300 | 129. | 18.1 | 659. |
| 24 | .290 | 125. | 18.2 | 642. |

DAY = 115

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .290 | 125. | 18.1 | 630. |
| 2 | .280 | 120. | 17.7 | 593. |
| 3 | .280 | 120. | 17.9 | 580. |
| 4 | .270 | 116. | 18.0 | 579. |
| 5 | .260 | 112. | 17.9 | 554. |
| 6 | .270 | 118. | 18.1 | 600. |
| 7 | .290 | 125. | 17.1 | 632. |
| 8 | .320 | 137. | 16.5 | 669. |
| 9 | .340 | 146. | 16.1 | 688. |
| 10 | .340 | 146. | 16.0 | 694. |
| 11 | .340 | 146. | 16.0 | 692. |
| 12 | .340 | 146. | 15.9 | 688. |
| 13 | .340 | 146. | 15.8 | 689. |
| 14 | .350 | 150. | 15.7 | 690. |
| 15 | .360 | 155. | 15.6 | 685. |
| 16 | .360 | 155. | 15.6 | 682. |
| 17 | .350 | 150. | 15.6 | 680. |
| 18 | .350 | 150. | 15.6 | 679. |
| 19 | .350 | 150. | 15.5 | 679. |
| 20 | .350 | 150. | 15.5 | 680. |
| 21 | .360 | 155. | 15.6 | 679. |
| 22 | .360 | 155. | 15.4 | 678. |
| 23 | .370 | 159. | 15.6 | 677. |
| 24 | .340 | 146. | 15.7 | 638. |

DAY = 116

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 15.4 | 571. |
| 2 | .310 | 133. | 15.5 | 567. |
| 3 | .300 | 129. | 15.6 | 537. |
| 4 | .290 | 125. | 15.3 | 532. |
| 5 | .300 | 129. | 15.2 | 536. |
| 6 | .330 | 142. | 15.4 | 612. |
| 7 | .330 | 142. | 15.5 | 640. |
| 8 | .350 | 150. | 15.5 | 680. |
| 9 | .360 | 155. | 15.3 | 670. |
| 10 | .350 | 150. | 15.2 | 664. |
| 11 | .350 | 150. | 15.3 | 687. |
| 12 | .350 | 150. | 15.3 | 677. |
| 13 | .340 | 146. | 15.2 | 656. |
| 14 | .330 | 142. | 15.1 | 636. |
| 15 | .330 | 142. | 15.0 | 640. |
| 16 | .340 | 146. | 15.5 | 685. |
| 17 | .330 | 142. | 15.5 | 651. |
| 18 | .330 | 142. | 15.6 | 649. |
| 19 | .330 | 142. | 15.3 | 634. |
| 20 | .340 | 146. | 15.3 | 654. |
| 21 | .350 | 150. | 15.1 | 650. |
| 22 | .360 | 155. | 15.0 | 645. |
| 23 | .340 | 146. | 14.9 | 619. |
| 24 | .320 | 137. | 14.8 | 573. |

DAY = 117

| | NOX | NOX | CO2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 15.0 | 619. |
| 2 | .320 | 137. | 14.8 | 557. |
| 3 | .300 | 129. | 14.9 | 548. |
| 4 | .290 | 125. | 14.7 | 519. |
| 5 | .290 | 125. | 14.8 | 530. |
| 6 | .300 | 129. | 14.8 | 540. |
| 7 | .330 | 142. | 15.0 | 624. |
| 8 | .330 | 142. | 15.2 | 640. |
| 9 | .330 | 142. | 15.5 | 662. |
| 10 | .340 | 146. | 15.6 | 679. |
| 11 | .330 | 142. | 15.6 | 674. |
| 12 | .340 | 146. | 15.6 | 674. |
| 13 | .340 | 146. | 15.8 | 684. |
| 14 | .320 | 137. | 16.5 | 674. |
| 15 | .290 | 125. | 18.0 | 676. |
| 16 | .280 | 120. | 17.9 | 626. |
| 17 | .280 | 120. | 18.0 | 630. |
| 18 | .300 | 129. | 17.9 | 652. |
| 19 | .300 | 129. | 18.0 | 656. |
| 20 | .280 | 120. | 17.7 | 592. |
| 21 | .310 | 133. | 18.0 | 663. |
| 22 | .310 | 133. | 17.9 | 651. |
| 23 | .290 | 125. | 17.9 | 615. |
| 24 | .280 | 120. | 17.9 | 603. |

DAY = 118

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 17.9 | 590. |
| 2 | .270 | 116. | 17.8 | 563. |
| 3 | .250 | 107. | 17.7 | 545. |
| 4 | .230 | 99. | 17.6 | 506. |
| 5 | .230 | 99. | 17.7 | 522. |
| 6 | .280 | 120. | 16.2 | 522. |
| 7 | .320 | 137. | 15.8 | 602. |
| 8 | .330 | 142. | 16.0 | 658. |
| 9 | .340 | 146. | 15.7 | 657. |
| 10 | .320 | 137. | 15.8 | 650. |
| 11 | .300 | 129. | 17.0 | 642. |
| 12 | .300 | 129. | 17.9 | 660. |
| 13 | .310 | 133. | 17.7 | 667. |
| 14 | .310 | 133. | 17.8 | 681. |
| 15 | .320 | 137. | 17.6 | 674. |
| 16 | .310 | 133. | 17.6 | 656. |
| 17 | .300 | 129. | 17.4 | 607. |
| 18 | .300 | 129. | 17.6 | 610. |
| 19 | .280 | 120. | 18.0 | 623. |
| 20 | .290 | 125. | 18.0 | 633. |
| 21 | .300 | 129. | 18.1 | 647. |
| 22 | .300 | 129. | 18.0 | 639. |
| 23 | .290 | 125. | 17.7 | 596. |
| 24 | .230 | 99. | 17.3 | 503. |

DAY = 120

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .210 | 90. | 15.7 | 306. |
| 2 | .210 | 90. | 15.9 | 321. |
| 3 | .210 | 90. | 16.2 | 349. |
| 4 | .210 | 90. | 16.1 | 348. |
| 5 | .210 | 90. | 16.1 | 350. |
| 6 | .200 | 86. | 15.9 | 333. |
| 7 | .200 | 86. | 16.0 | 335. |
| 8 | .180 | 77. | 16.6 | 347. |
| 9 | .180 | 77. | 16.7 | 350. |
| 10 | .180 | 77. | 16.8 | 351. |
| 11 | .180 | 77. | 16.6 | 349. |
| 12 | .180 | 77. | 16.6 | 353. |
| 13 | .180 | 77. | 16.6 | 353. |
| 14 | .180 | 77. | 16.7 | 351. |
| 15 | .170 | 73. | 16.7 | 352. |
| 16 | .170 | 73. | 16.8 | 353. |
| 17 | .170 | 73. | 16.8 | 354. |
| 18 | .200 | 86. | 17.7 | 494. |
| 19 | .220 | 95. | 17.8 | 559. |
| 20 | .220 | 95. | 17.8 | 553. |
| 21 | .240 | 103. | 18.0 | 583. |
| 22 | .260 | 112. | 17.8 | 599. |
| 23 | .250 | 107. | 17.6 | 561. |
| 24 | .220 | 95. | 17.0 | 466. |

DAY = 122



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.2 | 521. |
| 2 | .230 | 99. | 17.4 | 484. |
| 3 | .210 | 90. | 17.4 | 460. |
| 4 | .210 | 90. | 17.3 | 439. |
| 5 | .210 | 90. | 17.3 | 439. |
| 6 | .240 | 103. | 17.6 | 493. |
| 7 | .250 | 107. | 18.0 | 577. |
| 8 | .280 | 120. | 17.9 | 627. |
| 9 | .310 | 133. | 17.8 | 676. |
| 10 | .310 | 133. | 17.6 | 686. |
| 11 | .310 | 133. | 17.8 | 687. |
| 12 | .310 | 133. | 17.8 | 688. |
| 13 | .310 | 133. | 17.7 | 692. |
| 14 | .310 | 133. | 17.6 | 676. |
| 15 | .300 | 129. | 17.8 | 678. |
| 16 | .300 | 129. | 17.6 | 649. |
| 17 | .300 | 129. | 17.6 | 651. |
| 18 | .300 | 129. | 17.7 | 648. |
| 19 | .310 | 133. | 17.8 | 686. |
| 20 | .310 | 133. | 17.8 | 673. |
| 21 | .310 | 133. | 17.8 | 687. |
| 22 | .300 | 129. | 17.6 | 662. |
| 23 | .300 | 129. | 17.7 | 660. |
| 24 | .270 | 116. | 17.4 | 591. |

DAY = 123

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.6 | 578. |
| 2 | .270 | 116. | 17.1 | 538. |
| 3 | .240 | 103. | 16.9 | 487. |
| 4 | .240 | 103. | 16.8 | 455. |
| 5 | .240 | 103. | 17.0 | 479. |
| 6 | .250 | 107. | 17.1 | 514. |
| 7 | .280 | 120. | 17.6 | 617. |
| 8 | .300 | 129. | 17.6 | 653. |
| 9 | .300 | 129. | 17.6 | 672. |
| 10 | .310 | 133. | 17.5 | 675. |
| 11 | .320 | 137. | 17.5 | 686. |
| 12 | .310 | 133. | 17.6 | 685. |
| 13 | .310 | 133. | 17.7 | 681. |
| 14 | .310 | 133. | 17.7 | 679. |
| 15 | .310 | 133. | 17.8 | 688. |
| 16 | .310 | 133. | 17.7 | 673. |
| 17 | .320 | 137. | 17.7 | 682. |
| 18 | .310 | 133. | 17.6 | 655. |
| 19 | .290 | 125. | 17.7 | 611. |
| 20 | .280 | 120. | 17.5 | 581. |
| 21 | .310 | 133. | 18.0 | 673. |
| 22 | .300 | 129. | 17.8 | 661. |
| 23 | .290 | 125. | 17.7 | 637. |
| 24 | .260 | 112. | 17.1 | 513. |

DAY = 126



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 17.4 | 627. |
| 2 | .280 | 120. | 17.4 | 617. |
| 3 | .270 | 116. | 17.4 | 605. |
| 4 | .270 | 116. | 17.5 | 608. |
| 5 | .280 | 120. | 17.6 | 619. |
| 6 | .290 | 125. | 17.5 | 640. |
| 7 | .300 | 129. | 17.4 | 649. |
| 8 | .310 | 133. | 17.5 | 684. |
| 9 | .300 | 129. | 17.5 | 675. |
| 10 | .300 | 129. | 17.5 | 660. |
| 11 | .300 | 129. | 17.6 | 671. |
| 12 | .310 | 133. | 17.6 | 683. |
| 13 | .290 | 125. | 17.4 | 649. |
| 14 | .290 | 125. | 17.5 | 650. |
| 15 | .270 | 116. | 17.7 | 640. |
| 16 | .270 | 116. | 17.6 | 625. |
| 17 | .280 | 120. | 17.9 | 667. |
| 18 | .300 | 129. | 17.7 | 687. |
| 19 | .310 | 133. | 17.6 | 687. |
| 20 | .310 | 133. | 17.5 | 659. |
| 21 | .300 | 129. | 17.6 | 659. |
| 22 | .310 | 133. | 17.6 | 675. |
| 23 | .280 | 120. | 17.2 | 592. |
| 24 | .230 | 99. | 16.9 | 479. |

DAY = 127

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .210 | 90. | 16.6 | 388. |
| 2 | .210 | 90. | 16.8 | 400. |
| 3 | .210 | 90. | 16.8 | 394. |
| 4 | .210 | 90. | 16.8 | 399. |
| 5 | .210 | 90. | 16.9 | 394. |
| 6 | .220 | 95. | 16.8 | 394. |
| 7 | .250 | 107. | 17.5 | 539. |
| 8 | .290 | 125. | 17.8 | 652. |
| 9 | .290 | 125. | 17.8 | 674. |
| 10 | .280 | 120. | 17.7 | 653. |
| 11 | .280 | 120. | 17.7 | 648. |
| 12 | .270 | 116. | 17.7 | 637. |
| 13 | .270 | 116. | 17.6 | 623. |
| 14 | .260 | 112. | 17.6 | 605. |
| 15 | .250 | 107. | 17.4 | 573. |
| 16 | .250 | 107. | 17.5 | 570. |
| 17 | .280 | 120. | 17.5 | 605. |
| 18 | .260 | 112. | 17.5 | 596. |
| 19 | .290 | 125. | 17.6 | 661. |
| 20 | .300 | 129. | 17.6 | 664. |
| 21 | .310 | 133. | 17.5 | 683. |
| 22 | .320 | 137. | 17.3 | 670. |
| 23 | .300 | 129. | 17.2 | 628. |
| 24 | .260 | 112. | 17.0 | 563. |

DAY = 128



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 17.1 | 543. |
| 2 | .230 | 99. | 17.1 | 535. |
| 3 | .230 | 99. | 17.3 | 543. |
| 4 | .230 | 99. | 17.2 | 543. |
| 5 | .260 | 112. | 15.7 | 544. |
| 6 | .290 | 125. | 14.3 | 548. |
| 7 | .300 | 129. | 14.2 | 554. |
| 8 | .310 | 133. | 14.4 | 583. |
| 9 | .330 | 142. | 14.5 | 618. |
| 10 | .330 | 142. | 14.2 | 603. |
| 11 | .350 | 150. | 14.3 | 665. |
| 12 | .360 | 155. | 14.2 | 677. |
| 13 | .380 | 163. | 14.2 | 681. |
| 14 | .360 | 155. | 14.0 | 633. |
| 15 | .350 | 150. | 13.6 | 617. |
| 16 | .320 | 137. | 13.7 | 622. |
| 17 | .330 | 142. | 14.3 | 652. |
| 18 | .340 | 146. | 14.3 | 649. |
| 19 | .350 | 150. | 14.4 | 653. |
| 20 | .360 | 155. | 14.5 | 663. |
| 21 | .370 | 159. | 14.6 | 680. |
| 22 | .370 | 159. | 14.6 | 678. |
| 23 | .370 | 159. | 14.7 | 675. |
| 24 | .350 | 150. | 14.9 | 634. |

DAY = 130

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 16.2 | 599. |
| 2 | .290 | 125. | 17.2 | 601. |
| 3 | .290 | 125. | 17.3 | 631. |
| 4 | .300 | 129. | 17.2 | 636. |
| 5 | .310 | 133. | 17.3 | 661. |
| 6 | .320 | 137. | 17.3 | 682. |
| 7 | .300 | 129. | 17.3 | 649. |
| 8 | .320 | 137. | 17.5 | 686. |
| 9 | .320 | 137. | 17.5 | 704. |
| 10 | .330 | 142. | 17.3 | 719. |
| 11 | .340 | 146. | 17.4 | 715. |
| 12 | .310 | 133. | 17.1 | 715. |
| 13 | .320 | 137. | 17.0 | 678. |
| 14 | .320 | 137. | 17.0 | 662. |
| 15 | .310 | 133. | 17.0 | 655. |
| 16 | .300 | 129. | 17.1 | 634. |
| 17 | .310 | 133. | 17.1 | 642. |
| 18 | .300 | 129. | 17.0 | 616. |
| 19 | .300 | 129. | 17.0 | 622. |
| 20 | .300 | 129. | 17.2 | 635. |
| 21 | .310 | 133. | 17.3 | 644. |
| 22 | .320 | 137. | 17.3 | 661. |
| 23 | .310 | 133. | 17.3 | 642. |
| 24 | .310 | 133. | 17.2 | 623. |

DAY = 134



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.4 | 607. |
| 2 | .260 | 112. | 17.3 | 595. |
| 3 | .260 | 112. | 17.4 | 618. |
| 4 | .270 | 116. | 17.4 | 601. |
| 5 | .270 | 116. | 17.4 | 586. |
| 6 | .270 | 116. | 17.4 | 594. |
| 7 | .260 | 112. | 17.5 | 589. |
| 8 | .280 | 120. | 17.6 | 639. |
| 9 | .290 | 125. | 17.5 | 657. |
| 10 | .290 | 125. | 17.5 | 654. |
| 11 | .290 | 125. | 17.5 | 654. |
| 12 | .290 | 125. | 17.5 | 656. |
| 13 | .290 | 125. | 17.6 | 657. |
| 14 | .290 | 125. | 17.6 | 649. |
| 15 | .290 | 125. | 17.7 | 642. |
| 16 | .290 | 125. | 17.5 | 633. |
| 17 | .280 | 120. | 17.6 | 627. |
| 18 | .280 | 120. | 17.7 | 627. |
| 19 | .280 | 120. | 17.7 | 624. |
| 20 | .280 | 120. | 17.7 | 619. |
| 21 | .290 | 125. | 17.9 | 653. |
| 22 | .290 | 125. | 17.9 | 673. |
| 23 | .290 | 125. | 17.8 | 653. |
| 24 | .290 | 125. | 17.8 | 666. |

DAY = 135

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 17.8 | 662. |
| 2 | .280 | 120. | 17.6 | 624. |
| 3 | .260 | 112. | 17.5 | 583. |
| 4 | .250 | 107. | 17.5 | 562. |
| 5 | .240 | 103. | 17.2 | 535. |
| 6 | .230 | 99. | 17.2 | 511. |
| 7 | .240 | 103. | 17.2 | 529. |
| 8 | .260 | 112. | 17.4 | 561. |
| 9 | .300 | 129. | 17.3 | 619. |
| 10 | .310 | 133. | 17.4 | 649. |
| 11 | .320 | 137. | 17.3 | 673. |
| 12 | .320 | 137. | 17.3 | 673. |
| 13 | .320 | 137. | 17.4 | 679. |
| 14 | .310 | 133. | 17.5 | 678. |
| 15 | .300 | 129. | 17.7 | 683. |
| 16 | .310 | 133. | 17.7 | 690. |
| 17 | .300 | 129. | 17.6 | 673. |
| 18 | .300 | 129. | 17.7 | 670. |
| 19 | .310 | 133. | 17.6 | 670. |
| 20 | .320 | 137. | 17.5 | 671. |
| 21 | .320 | 137. | 17.9 | 708. |
| 22 | .310 | 133. | 17.7 | 682. |
| 23 | .300 | 129. | 17.5 | 639. |
| 24 | .290 | 125. | 17.4 | 619. |

DAY = 136



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 17.4 | 619. |
| 2 | .290 | 125. | 17.4 | 618. |
| 3 | .290 | 125. | 17.3 | 600. |
| 4 | .290 | 125. | 17.3 | 599. |
| 5 | .280 | 120. | 17.5 | 599. |
| 6 | .290 | 125. | 17.7 | 636. |
| 7 | .310 | 133. | 17.9 | 665. |
| 8 | .310 | 133. | 17.6 | 687. |
| 9 | .320 | 137. | 17.6 | 691. |
| 10 | .330 | 142. | 17.5 | 695. |
| 11 | .340 | 146. | 17.5 | 695. |
| 12 | .330 | 142. | 17.5 | 695. |
| 13 | .320 | 137. | 17.7 | 698. |
| 14 | .330 | 142. | 17.5 | 694. |
| 15 | .330 | 142. | 17.3 | 687. |
| 16 | .330 | 142. | 17.4 | 692. |
| 17 | .330 | 142. | 17.4 | 694. |
| 18 | .330 | 142. | 17.5 | 689. |
| 19 | .330 | 142. | 17.6 | 695. |
| 20 | .340 | 146. | 17.5 | 701. |
| 21 | .340 | 146. | 17.6 | 706. |
| 22 | .340 | 146. | 17.8 | 711. |
| 23 | .350 | 150. | 17.3 | 684. |
| 24 | .330 | 142. | 17.1 | 611. |

DAY = 138

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 17.0 | 586. |
| 2 | .280 | 120. | 17.6 | 598. |
| 3 | .270 | 116. | 17.4 | 573. |
| 4 | .270 | 116. | 17.3 | 568. |
| 5 | .280 | 120. | 17.5 | 600. |
| 6 | .290 | 125. | 17.5 | 641. |
| 7 | .300 | 129. | 17.5 | 654. |
| 8 | .300 | 129. | 17.5 | 674. |
| 9 | .300 | 129. | 17.4 | 661. |
| 10 | .300 | 129. | 17.4 | 666. |
| 11 | .310 | 133. | 17.4 | 670. |
| 12 | .310 | 133. | 17.4 | 674. |
| 13 | .310 | 133. | 17.5 | 664. |
| 14 | .310 | 133. | 17.5 | 665. |
| 15 | .300 | 129. | 17.6 | 658. |
| 16 | .300 | 129. | 17.7 | 663. |
| 17 | .300 | 129. | 17.7 | 660. |
| 18 | .290 | 125. | 17.8 | 639. |
| 19 | .290 | 125. | 18.0 | 657. |
| 20 | .300 | 129. | 17.8 | 643. |
| 21 | .310 | 133. | 18.0 | 674. |
| 22 | .320 | 137. | 17.9 | 691. |
| 23 | .310 | 133. | 17.8 | 644. |
| 24 | .290 | 125. | 17.9 | 629. |

DAY = 139



| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 17.6 | 578. |
| 2 | .260 | 112. | 17.7 | 554. |
| 3 | .240 | 103. | 17.7 | 521. |
| 4 | .250 | 107. | 17.5 | 512. |
| 5 | .250 | 107. | 17.5 | 508. |
| 6 | .230 | 99. | 17.5 | 514. |
| 7 | .240 | 103. | 17.8 | 577. |
| 8 | .310 | 133. | 17.7 | 669. |
| 9 | .310 | 133. | 17.6 | 678. |
| 10 | .300 | 129. | 17.6 | 678. |
| 11 | .310 | 133. | 17.5 | 684. |
| 12 | .310 | 133. | 17.6 | 685. |
| 13 | .300 | 129. | 17.7 | 681. |
| 14 | .290 | 125. | 17.6 | 683. |
| 15 | .300 | 129. | 17.7 | 681. |
| 16 | .290 | 125. | 17.7 | 674. |
| 17 | .290 | 125. | 17.9 | 681. |
| 18 | .230 | 99. | 17.9 | 672. |
| 19 | .300 | 129. | 17.9 | 677. |
| 20 | .300 | 129. | 17.8 | 665. |
| 21 | .310 | 133. | 17.9 | 682. |
| 22 | .300 | 129. | 17.9 | 676. |
| 23 | .290 | 125. | 17.8 | 654. |
| 24 | .290 | 125. | 17.8 | 624. |

DAY = 140

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 17.0 | 562. |
| 2 | .220 | 95. | 17.0 | 509. |
| 3 | .180 | 77. | 17.0 | 426. |
| 4 | .170 | 73. | 17.2 | 434. |
| 5 | .170 | 73. | 17.0 | 447. |
| 6 | .190 | 82. | 17.6 | 485. |
| 7 | .260 | 112. | 18.2 | 629. |
| 8 | .250 | 107. | 18.0 | 678. |
| 9 | .170 | 73. | 17.8 | 684. |
| 10 | .250 | 107. | 17.7 | 688. |
| 11 | .310 | 133. | 17.8 | 674. |
| 12 | .310 | 133. | 17.8 | 683. |
| 13 | .300 | 129. | 17.8 | 674. |
| 14 | .300 | 129. | 17.9 | 686. |
| 15 | .290 | 125. | 18.0 | 682. |
| 16 | .290 | 125. | 18.0 | 681. |
| 17 | .280 | 120. | 17.9 | 655. |
| 18 | .280 | 120. | 17.8 | 610. |
| 19 | .280 | 120. | 18.0 | 635. |
| 20 | .300 | 129. | 17.8 | 645. |
| 21 | .300 | 129. | 17.9 | 654. |
| 22 | .300 | 129. | 17.9 | 670. |
| 23 | .300 | 129. | 18.2 | 657. |
| 24 | .230 | 99. | 17.3 | 474. |

DAY = 142

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 17.8 | 629. |
| 2 | .300 | 129. | 17.9 | 628. |
| 3 | .290 | 125. | 17.8 | 591. |
| 4 | .270 | 116. | 17.8 | 571. |
| 5 | .270 | 116. | 17.8 | 571. |
| 6 | .260 | 112. | 17.5 | 531. |
| 7 | .240 | 103. | 17.6 | 510. |
| 8 | .270 | 116. | 17.8 | 561. |
| 9 | .280 | 120. | 17.8 | 607. |
| 10 | .310 | 133. | 17.9 | 655. |
| 11 | .320 | 137. | 17.9 | 672. |
| 12 | .360 | 155. | 15.1 | 672. |
| 13 | .410 | 176. | 13.5 | 671. |
| 14 | .400 | 172. | 13.3 | 643. |
| 15 | .410 | 176. | 13.5 | 653. |
| 16 | .430 | 185. | 13.6 | 665. |
| 17 | .440 | 189. | 13.6 | 673. |
| 18 | .420 | 180. | 13.8 | 660. |
| 19 | .400 | 172. | 13.9 | 650. |
| 20 | .410 | 176. | 13.9 | 637. |
| 21 | .410 | 176. | 14.1 | 664. |
| 22 | .420 | 180. | 14.1 | 679. |
| 23 | .410 | 176. | 14.1 | 663. |
| 24 | .360 | 155. | 13.8 | 588. |

DAY = 144

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 14.2 | 628. |
| 2 | .340 | 146. | 14.0 | 589. |
| 3 | .330 | 142. | 14.1 | 580. |
| 4 | .320 | 137. | 14.0 | 561. |
| 5 | .330 | 142. | 14.2 | 583. |
| 6 | .350 | 150. | 14.2 | 623. |
| 7 | .360 | 155. | 14.3 | 650. |
| 8 | .380 | 163. | 14.3 | 682. |
| 9 | .400 | 172. | 14.0 | 681. |
| 10 | .380 | 163. | 14.0 | 676. |
| 11 | .390 | 168. | 14.1 | 674. |
| 12 | .390 | 168. | 14.1 | 677. |
| 13 | .390 | 168. | 14.1 | 672. |
| 14 | .400 | 172. | 14.0 | 673. |
| 15 | .400 | 172. | 13.9 | 668. |
| 16 | .410 | 176. | 14.0 | 670. |
| 17 | .390 | 168. | 13.9 | 640. |
| 18 | .380 | 163. | 14.0 | 655. |
| 19 | .380 | 163. | 14.0 | 638. |
| 20 | .380 | 163. | 14.1 | 644. |
| 21 | .380 | 163. | 14.1 | 644. |
| 22 | .380 | 163. | 14.1 | 644. |
| 23 | .380 | 163. | 14.1 | 643. |
| 24 | .390 | 168. | 14.0 | 638. |

DAY = 149

| HOUR | NOX LB/10**6 BTU | NOX NG/J | CO2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 14.3 | 584. |
| 2 | .310 | 133. | 14.6 | 612. |
| 3 | .320 | 137. | 14.6 | 629. |
| 4 | .320 | 137. | 14.6 | 610. |
| 5 | .330 | 142. | 14.5 | 617. |
| 6 | .340 | 146. | 14.0 | 614. |
| 7 | .360 | 155. | 14.4 | 667. |
| 8 | .360 | 155. | 14.3 | 673. |
| 9 | .370 | 159. | 14.3 | 676. |
| 10 | .370 | 159. | 14.3 | 676. |
| 11 | .370 | 159. | 14.7 | 709. |
| 12 | .390 | 168. | 14.7 | 712. |
| 13 | .390 | 168. | 14.6 | 709. |
| 14 | .390 | 168. | 14.7 | 706. |
| 15 | .390 | 168. | 14.6 | 702. |
| 16 | .380 | 163. | 14.7 | 698. |
| 17 | .370 | 159. | 14.7 | 682. |
| 18 | .380 | 163. | 14.6 | 666. |
| 19 | .380 | 163. | 14.8 | 667. |
| 20 | .390 | 168. | 14.8 | 667. |
| 21 | .390 | 168. | 14.6 | 668. |
| 22 | .400 | 172. | 14.7 | 674. |
| 23 | .410 | 176. | 14.7 | 684. |
| 24 | .320 | 137. | 13.9 | 548. |

APPENDIX I

PENNSYLVANIA ELECTRIC

HOMER CITY GENERATING STATION

UNIT 3

Input Data

**PULVERIZED COAL-FIRED UTILITY BOILER NOx EMISSION MONITORING**

PENNSYLVANIA ELECTRIC HOMER CITY STATION UNIT 3

B+W BOILER OPPOSED FACE-FIRED

680 MWE GROSS DAY 1 = 1 MAY 1979

DUAL REGISTER BURNERS BITUMINOUS COAL

NOX MONITOR RELATIVE ACCURACY = 12.4 PC

PERFORMANCE TEST NOX = 0.68 LB/10**6 BTU. 292 NG/J

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 8.0 | 447. |
| 2 | .530 | 228. | 8.0 | 451. |
| 3 | .530 | 228. | 8.0 | 452. |
| 4 | .530 | 228. | 8.0 | 457. |
| 5 | .530 | 228. | 8.0 | 455. |
| 6 | .530 | 228. | 8.0 | 449. |
| 7 | .530 | 228. | 8.0 | 450. |
| 8 | .590 | 253. | 8.0 | 455. |
| 9 | .590 | 253. | 8.0 | 454. |
| 10 | .590 | 253. | 8.0 | 450. |
| 11 | .590 | 253. | 8.0 | 448. |
| 12 | .590 | 253. | 8.0 | 449. |
| 13 | .590 | 253. | 8.0 | 454. |
| 14 | .590 | 253. | 8.0 | 450. |
| 15 | .590 | 253. | 8.0 | 449. |
| 16 | .590 | 253. | 8.0 | 452. |
| 17 | .590 | 253. | 8.0 | 448. |
| 18 | .530 | 228. | 8.0 | 450. |
| 19 | .530 | 228. | 8.0 | 449. |
| 20 | .530 | 228. | 8.0 | 446. |
| 21 | .530 | 228. | 8.0 | 451. |
| 22 | .530 | 228. | 8.0 | 451. |
| 23 | .530 | 228. | 8.0 | 448. |
| 24 | .530 | 228. | 8.0 | 453. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 8.0 | 450. |
| 2 | .530 | 228. | 8.0 | 449. |
| 3 | .540 | 232. | 8.2 | 448. |
| 4 | .530 | 228. | 8.0 | 449. |
| 5 | .590 | 253. | 8.0 | 455. |
| 6 | .540 | 232. | 8.2 | 460. |
| 7 | .600 | 258. | 8.2 | 452. |
| 8 | .590 | 253. | 8.0 | 452. |
| 9 | .590 | 253. | 8.0 | 452. |
| 10 | .610 | 262. | 8.5 | 453. |
| 11 | .550 | 236. | 8.5 | 452. |
| 12 | .560 | 241. | 8.8 | 452. |
| 13 | .550 | 236. | 8.5 | 449. |
| 14 | .550 | 236. | 8.5 | 453. |
| 15 | .550 | 236. | 8.5 | 452. |
| 16 | .550 | 236. | 8.5 | 450. |
| 17 | .550 | 236. | 8.5 | 448. |
| 18 | .550 | 236. | 8.5 | 446. |
| 19 | .550 | 236. | 8.5 | 446. |
| 20 | .550 | 236. | 8.5 | 447. |

| | | | | |
|---|---|---|---|---|
| 21 | .550 | 236. | 8.5 | 452. |
| 22 | .550 | 236. | 8.5 | 448. |
| 23 | .550 | 236. | 8.5 | 444. |
| 24 | .550 | 236. | 8.5 | 441. |

DAY # 3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 8.5 | 446. |
| 2 | .610 | 262. | 8.5 | 450. |
| 3 | .600 | 258. | 8.2 | 468. |
| 4 | .620 | 266. | 7.5 | 490. |
| 5 | .690 | 296. | 7.7 | 556. |
| 6 | .680 | 292. | 7.5 | 609. |
| 7 | .610 | 262. | 7.2 | 609. |
| 8 | .610 | 262. | 7.2 | 610. |
| 9 | .610 | 262. | 7.2 | 623. |
| 10 | .610 | 262. | 7.2 | 622. |
| 11 | .610 | 262. | 7.2 | 622. |
| 12 | .590 | 253. | 6.7 | 614. |
| 13 | .640 | 275. | 6.7 | 625. |
| 14 | .640 | 275. | 6.7 | 646. |
| 15 | .640 | 275. | 6.7 | 650. |
| 16 | .640 | 275. | 6.7 | 651. |
| 17 | .640 | 275. | 6.7 | 652. |
| 18 | .640 | 275. | 6.7 | 648. |
| 19 | .640 | 275. | 6.7 | 648. |
| 20 | .640 | 275. | 6.7 | 647. |
| 21 | .640 | 275. | 6.7 | 648. |
| 22 | .640 | 275. | 6.7 | 649. |
| 23 | .640 | 275. | 6.7 | 652. |
| 24 | .640 | 275. | 6.7 | 650. |

DAY # 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.0 | 654. |
| 2 | .650 | 279. | 7.0 | 652. |
| 3 | .650 | 279. | 7.0 | 650. |
| 4 | .650 | 279. | 7.0 | 652. |
| 5 | .650 | 279. | 7.0 | 652. |
| 6 | .670 | 288. | 7.2 | 654. |
| 7 | .670 | 288. | 7.2 | 654. |
| 8 | .670 | 288. | 7.2 | 651. |
| 9 | .670 | 288. | 7.2 | 650. |
| 10 | .670 | 288. | 7.2 | 652. |
| 11 | .650 | 279. | 7.0 | 651. |
| 12 | .650 | 279. | 7.0 | 654. |
| 13 | .650 | 279. | 7.0 | 650. |
| 14 | .650 | 279. | 7.0 | 649. |
| 15 | .710 | 305. | 7.0 | 652. |
| 16 | .710 | 305. | 7.0 | 651. |
| 17 | .710 | 305. | 7.0 | 656. |
| 18 | .650 | 279. | 7.0 | 652. |
| 19 | .650 | 279. | 7.0 | 652. |

| | | | | |
|---|---|---|---|---|
| 20 | .650 | 279. | 7.0 | 651. |
| 21 | .650 | 279. | 7.0 | 652. |
| 22 | .650 | 279. | 7.0 | 654. |
| 23 | .650 | 279. | 7.0 | 654. |
| 24 | .650 | 279. | 7.0 | 657. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 7.2 | 651. |
| 2 | .720 | 309. | 7.2 | 589. |
| 3 | .710 | 305. | 7.0 | 649. |
| 4 | .710 | 305. | 7.0 | 655. |
| 5 | .710 | 305. | 7.0 | 657. |
| 6 | .710 | 305. | 7.0 | 656. |
| 7 | .710 | 305. | 7.0 | 657. |
| 8 | .710 | 305. | 7.0 | 656. |
| 9 | .710 | 305. | 7.0 | 656. |
| 10 | .710 | 305. | 7.0 | 654. |
| 11 | .710 | 305. | 7.0 | 653. |
| 12 | .710 | 305. | 7.0 | 651. |
| 13 | .710 | 305. | 7.0 | 653. |
| 14 | .710 | 305. | 7.0 | 657. |
| 15 | .650 | 279. | 7.0 | 655. |
| 16 | .650 | 279. | 7.0 | 652. |
| 17 | .650 | 279. | 7.0 | 652. |
| 18 | .650 | 279. | 7.0 | 655. |
| 19 | .650 | 279. | 7.0 | 654. |
| 20 | .650 | 279. | 7.0 | 654. |
| 21 | .650 | 279. | 7.0 | 655. |
| 22 | .650 | 279. | 7.0 | 655. |
| 23 | .650 | 279. | 7.0 | 657. |
| 24 | .710 | 305. | 7.0 | 642. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .710 | 305. | 7.0 | 657. |
| 2 | .710 | 305. | 7.0 | 659. |
| 3 | .710 | 305. | 7.0 | 659. |
| 4 | .710 | 305. | 7.0 | 660. |
| 5 | .710 | 305. | 7.0 | 660. |
| 6 | .710 | 305. | 7.0 | 660. |
| 7 | .650 | 279. | 7.0 | 658. |
| 8 | .650 | 279. | 7.0 | 653. |
| 9 | .640 | 275. | 6.7 | 654. |
| 10 | .640 | 275. | 6.7 | 655. |
| 11 | .650 | 279. | 7.0 | 656. |
| 12 | .650 | 279. | 7.0 | 653. |
| 13 | .650 | 279. | 7.0 | 652. |
| 14 | .650 | 279. | 7.0 | 651. |
| 15 | .650 | 279. | 7.0 | 653. |
| 16 | .650 | 279. | 7.0 | 654. |
| 17 | .650 | 279. | 7.0 | 655. |
| 18 | .650 | 279. | 7.0 | 655. |

| | | | | |
|---|---|---|---|---|
| 19 | .650 | 279. | 7.0 | 655. |
| 20 | .650 | 279. | 7.0 | 652. |
| 21 | .650 | 279. | 7.0 | 653. |
| 22 | .650 | 279. | 7.0 | 653. |
| 23 | .670 | 288. | 7.2 | 654. |
| 24 | .600 | 258. | 7.0 | 672. |

DAY # 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.0 | 651. |
| 2 | .650 | 279. | 7.0 | 649. |
| 3 | .650 | 279. | 7.0 | 644. |
| 4 | .650 | 279. | 7.0 | 652. |
| 5 | .650 | 279. | 7.0 | 652. |
| 6 | .650 | 279. | 7.0 | 652. |
| 7 | .650 | 279. | 7.0 | 650. |
| 8 | .650 | 279. | 7.0 | 649. |
| 9 | .650 | 279. | 7.0 | 658. |
| 10 | .650 | 279. | 7.0 | 650. |
| 11 | .650 | 279. | 7.0 | 649. |
| 12 | .600 | 258. | 7.0 | 644. |
| 13 | .600 | 258. | 7.0 | 646. |
| 14 | .610 | 262. | 7.2 | 647. |
| 15 | .610 | 262. | 7.2 | 654. |
| 16 | .610 | 262. | 7.2 | 649. |
| 17 | .610 | 262. | 7.2 | 647. |
| 18 | .610 | 262. | 7.2 | 647. |
| 19 | .610 | 262. | 7.2 | 647. |
| 20 | .610 | 262. | 7.2 | 646. |
| 21 | .610 | 262. | 7.2 | 648. |
| 22 | .610 | 262. | 7.2 | 646. |
| 23 | .610 | 262. | 7.2 | 648. |
| 24 | .600 | 258. | 7.0 | 637. |

DAY # 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 7.2 | 646. |
| 2 | .600 | 258. | 7.0 | 644. |
| 3 | .600 | 258. | 7.0 | 648. |
| 4 | .600 | 258. | 7.0 | 647. |
| 5 | .600 | 258. | 7.0 | 650. |
| 6 | .600 | 258. | 7.0 | 649. |
| 7 | .610 | 262. | 7.2 | 647. |
| 8 | .610 | 262. | 7.2 | 646. |
| 9 | .600 | 258. | 7.0 | 644. |
| 10 | .600 | 258. | 7.0 | 645. |
| 11 | .600 | 258. | 7.0 | 646. |
| 12 | .600 | 258. | 7.0 | 643. |
| 13 | .600 | 258. | 7.0 | 647. |
| 14 | .600 | 258. | 7.0 | 646. |
| 15 | .600 | 258. | 7.0 | 645. |
| 16 | .600 | 258. | 7.0 | 641. |
| 17 | .600 | 258. | 7.0 | 648. |

| | | | | |
|---|---|---|---|---|
| 18 | .600 | 258. | 7.0 | 660. |
| 19 | .600 | 258. | 7.0 | 649. |
| 20 | .600 | 258. | 7.0 | 648. |
| 21 | .600 | 258. | 7.0 | 647. |
| 22 | .600 | 258. | 7.0 | 647. |
| 23 | .600 | 258. | 7.0 | 648. |
| 24 | .600 | 258. | 7.0 | 649. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.0 | 648. |
| 2 | .600 | 258. | 7.0 | 643. |
| 3 | .600 | 258. | 7.0 | 649. |
| 4 | .600 | 258. | 7.0 | 649. |
| 5 | .600 | 258. | 7.0 | 652. |
| 6 | .600 | 258. | 7.0 | 651. |
| 7 | .600 | 258. | 7.0 | 651. |
| 8 | .600 | 258. | 7.0 | 651. |
| 9 | .600 | 258. | 7.0 | 647. |
| 10 | .600 | 258. | 7.0 | 645. |
| 11 | .600 | 258. | 7.0 | 647. |
| 12 | .550 | 236. | 7.0 | 639. |
| 13 | .550 | 236. | 7.0 | 646. |
| 14 | .600 | 258. | 7.0 | 645. |
| 15 | .600 | 258. | 7.0 | 643. |
| 16 | .600 | 258. | 7.0 | 643. |
| 17 | .600 | 258. | 7.0 | 645. |
| 18 | .600 | 258. | 7.0 | 646. |
| 19 | .600 | 258. | 7.0 | 647. |
| 20 | .600 | 258. | 7.0 | 646. |
| 21 | .600 | 258. | 7.0 | 648. |
| 22 | .600 | 258. | 7.0 | 645. |
| 23 | .600 | 258. | 7.0 | 645. |
| 24 | .600 | 258. | 7.0 | 650. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.0 | 644. |
| 2 | .600 | 258. | 7.0 | 646. |
| 3 | .600 | 258. | 7.0 | 648. |
| 4 | .600 | 258. | 7.0 | 648. |
| 5 | .600 | 258. | 7.0 | 650. |
| 6 | .600 | 258. | 7.0 | 650. |
| 7 | .600 | 258. | 7.0 | 659. |
| 8 | .600 | 258. | 7.0 | 645. |
| 9 | .590 | 253. | 6.7 | 644. |
| 10 | .640 | 275. | 6.7 | 645. |
| 11 | .590 | 253. | 6.7 | 646. |
| 12 | .600 | 258. | 7.0 | 637. |
| 13 | .600 | 258. | 7.0 | 650. |
| 14 | .600 | 258. | 7.0 | 646. |
| 15 | .600 | 258. | 7.0 | 647. |
| 16 | .600 | 258. | 7.0 | 646. |

| | | | | |
|---|---|---|---|---|
| 17 | .600 | 258. | 7.0 | 651. |
| 18 | .600 | 258. | 7.0 | 649. |
| 19 | .600 | 258. | 7.0 | 649. |
| 20 | .600 | 258. | 7.0 | 648. |
| 21 | .600 | 258. | 7.0 | 647. |
| 22 | .600 | 258. | 7.0 | 645. |
| 23 | .600 | 258. | 7.0 | 649. |
| 24 | .600 | 258. | 7.0 | 645. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 6.7 | 660. |
| 2 | .640 | 275. | 6.7 | 658. |
| 3 | .640 | 275. | 6.7 | 657. |
| 4 | .640 | 275. | 6.7 | 657. |
| 5 | .640 | 275. | 6.7 | 657. |
| 6 | .640 | 275. | 6.7 | 659. |
| 7 | .640 | 275. | 6.7 | 657. |
| 8 | .640 | 275. | 6.7 | 661. |
| 9 | .640 | 275. | 6.7 | 662. |
| 10 | .700 | 301. | 6.7 | 658. |
| 11 | .650 | 279. | 7.0 | 659. |
| 12 | .710 | 305. | 7.0 | 610. |
| 13 | .710 | 305. | 7.0 | 651. |
| 14 | .650 | 279. | 7.0 | 664. |
| 15 | .640 | 275. | 6.7 | 662. |
| 16 | .640 | 275. | 6.7 | 661. |
| 17 | .640 | 275. | 6.7 | 657. |
| 18 | .640 | 275. | 6.7 | 658. |
| 19 | .640 | 275. | 6.7 | 657. |
| 20 | .590 | 253. | 6.7 | 659. |
| 21 | .630 | 271. | 6.5 | 660. |
| 22 | .630 | 271. | 6.5 | 659. |
| 23 | .630 | 271. | 6.5 | 660. |
| 24 | .630 | 271. | 6.5 | 657. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .690 | 296. | 6.5 | 655. |
| 2 | .590 | 253. | 6.7 | 659. |
| 3 | .630 | 271. | 6.5 | 657. |
| 4 | .630 | 271. | 6.5 | 661. |
| 5 | .630 | 271. | 6.5 | 656. |
| 6 | .690 | 296. | 6.5 | 655. |
| 7 | .650 | 279. | 7.0 | 656. |
| 8 | .680 | 292. | 7.5 | 659. |
| 9 | .670 | 288. | 7.2 | 659. |
| 10 | .710 | 305. | 7.0 | 660. |
| 11 | .690 | 296. | 6.5 | 658. |
| 12 | .690 | 296. | 6.5 | 659. |
| 13 | .690 | 296. | 6.5 | 659. |
| 14 | .690 | 296. | 6.5 | 658. |
| 15 | .690 | 296. | 6.5 | 657. |

| | | | | |
|---|---|---|---|---|
| 16 | .690 | 296. | 6.5 | 658. |
| 17 | .690 | 296. | 6.5 | 657. |
| 18 | .630 | 271. | 6.5 | 654. |
| 19 | .630 | 271. | 6.5 | 652. |
| 20 | .630 | 271. | 6.5 | 653. |
| 21 | .630 | 271. | 6.5 | 658. |
| 22 | .640 | 275. | 6.7 | 658. |
| 23 | .640 | 275. | 6.7 | 658. |
| 24 | .640 | 275. | 6.7 | 663. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.0 | 659. |
| 2 | .650 | 279. | 7.0 | 660. |
| 3 | .650 | 279. | 7.0 | 656. |
| 4 | .650 | 279. | 7.0 | 653. |
| 5 | .650 | 279. | 7.0 | 655. |
| 6 | .650 | 279. | 7.0 | 658. |
| 7 | .650 | 279. | 7.0 | 659. |
| 8 | .630 | 271. | 6.5 | 658. |
| 9 | .630 | 271. | 6.5 | 655. |
| 10 | .690 | 296. | 6.5 | 655. |
| 11 | .630 | 271. | 6.5 | 657. |
| 12 | .630 | 271. | 6.5 | 658. |
| 13 | .630 | 271. | 6.5 | 657. |
| 14 | .630 | 271. | 6.5 | 657. |
| 15 | .630 | 271. | 6.5 | 655. |
| 16 | .620 | 266. | 6.3 | 656. |
| 17 | .620 | 266. | 6.3 | 653. |
| 18 | .620 | 266. | 6.3 | 657. |
| 19 | .630 | 271. | 6.5 | 658. |
| 20 | .630 | 271. | 6.5 | 657. |
| 21 | .630 | 271. | 6.5 | 655. |
| 22 | .630 | 271. | 6.5 | 655. |
| 23 | .620 | 266. | 6.3 | 652. |
| 24 | .630 | 271. | 6.5 | 666. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 658. |
| 2 | .630 | 271. | 6.5 | 653. |
| 3 | .630 | 271. | 6.5 | 658. |
| 4 | .620 | 266. | 6.3 | 655. |
| 5 | .620 | 266. | 6.3 | 655. |
| 6 | .630 | 271. | 6.5 | 656. |
| 7 | .630 | 271. | 6.5 | 657. |
| 8 | .640 | 275. | 6.7 | 656. |
| 9 | .630 | 271. | 6.5 | 656. |
| 10 | .640 | 275. | 6.7 | 657. |
| 11 | .640 | 275. | 6.7 | 657. |
| 12 | .640 | 275. | 6.7 | 655. |
| 13 | .640 | 275. | 6.7 | 652. |
| 14 | .630 | 271. | 6.5 | 656. |

| | | | | |
|---|---|---|---|---|
| 15 | .640 | 275. | 6.7 | 659. |
| 16 | .640 | 275. | 6.7 | 655. |
| 17 | .640 | 275. | 6.7 | 654. |
| 18 | .640 | 275. | 6.7 | 653. |
| 19 | .640 | 275. | 6.7 | 655. |
| 20 | .640 | 275. | 6.7 | 657. |
| 21 | .640 | 275. | 6.7 | 658. |
| 22 | .640 | 275. | 6.7 | 657. |
| 23 | .590 | 253. | 6.7 | 658. |
| 24 | .640 | 275. | 6.7 | 656. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 6.7 | 653. |
| 2 | .640 | 275. | 6.7 | 652. |
| 3 | .640 | 275. | 6.7 | 656. |
| 4 | .640 | 275. | 6.7 | 656. |
| 5 | .640 | 275. | 6.7 | 657. |
| 6 | .640 | 275. | 6.7 | 654. |
| 7 | .640 | 275. | 6.7 | 654. |
| 8 | .630 | 271. | 6.5 | 656. |
| 9 | .630 | 271. | 6.5 | 656. |
| 10 | .630 | 271. | 6.5 | 656. |
| 11 | .630 | 271. | 6.5 | 653. |
| 12 | .630 | 271. | 6.5 | 653. |
| 13 | .630 | 271. | 6.5 | 655. |
| 14 | .630 | 271. | 6.5 | 655. |
| 15 | .580 | 249. | 6.5 | 658. |
| 16 | .630 | 271. | 6.5 | 655. |
| 17 | .580 | 249. | 6.5 | 651. |
| 18 | .580 | 249. | 6.5 | 655. |
| 19 | .580 | 249. | 6.5 | 656. |
| 20 | .580 | 249. | 6.5 | 657. |
| 21 | .580 | 249. | 6.5 | 658. |
| 22 | .580 | 249. | 6.5 | 657. |
| 23 | .580 | 249. | 6.5 | 656. |
| 24 | .580 | 249. | 6.5 | 645. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.3 | 651. |
| 2 | .570 | 245. | 6.3 | 654. |
| 3 | .610 | 262. | 6.0 | 654. |
| 4 | .560 | 241. | 6.0 | 652. |
| 5 | .620 | 266. | 6.3 | 651. |
| 6 | .630 | 271. | 6.5 | 650. |
| 7 | .630 | 271. | 6.5 | 653. |
| 8 | .640 | 275. | 6.7 | 653. |
| 9 | .640 | 275. | 6.7 | 654. |
| 10 | .590 | 253. | 6.7 | 654. |
| 11 | .590 | 253. | 6.7 | 654. |
| 12 | .640 | 275. | 6.7 | 655. |
| 13 | .640 | 275. | 6.7 | 654. |

| | | | | |
|---|---|---|---|---|
| 14 | .640 | 275. | 6.7 | 655. |
| 15 | .640 | 275. | 6.7 | 656. |
| 16 | .640 | 275. | 6.7 | 657. |
| 17 | .640 | 275. | 6.7 | 657. |
| 18 | .640 | 275. | 6.7 | 654. |
| 19 | .640 | 275. | 6.7 | 654. |
| 20 | .640 | 275. | 6.7 | 654. |
| 21 | .640 | 275. | 6.7 | 651. |
| 22 | .610 | 262. | 7.2 | 655. |
| 23 | .600 | 258. | 7.0 | 650. |
| 24 | .600 | 258. | 7.0 | 661. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .590 | 253. | 6.7 | 656. |
| 2 | .590 | 253. | 6.7 | 654. |
| 3 | .590 | 253. | 6.7 | 655. |
| 4 | .640 | 275. | 6.7 | 657. |
| 5 | .700 | 301. | 6.7 | 657. |
| 6 | .700 | 301. | 6.7 | 659. |
| 7 | .700 | 301. | 6.7 | 658. |
| 8 | .630 | 271. | 6.5 | 658. |
| 9 | .630 | 271. | 6.5 | 660. |
| 10 | .690 | 296. | 6.5 | 661. |
| 11 | .630 | 271. | 6.5 | 662. |
| 12 | .630 | 271. | 6.5 | 661. |
| 13 | .640 | 275. | 6.7 | 656. |
| 14 | .640 | 275. | 6.7 | 655. |
| 15 | .630 | 271. | 6.5 | 654. |
| 16 | .630 | 271. | 6.5 | 656. |
| 17 | .630 | 271. | 6.5 | 658. |
| 18 | .630 | 271. | 6.5 | 657. |
| 19 | .580 | 249. | 6.5 | 654. |
| 20 | .580 | 249. | 6.5 | 655. |
| 21 | .580 | 249. | 6.5 | 659. |
| 22 | .580 | 249. | 6.5 | 659. |
| 23 | .630 | 271. | 6.5 | 659. |
| 24 | .580 | 249. | 6.5 | 646. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 654. |
| 2 | .630 | 271. | 6.5 | 658. |
| 3 | .580 | 249. | 6.5 | 657. |
| 4 | .570 | 245. | 6.3 | 656. |
| 5 | .620 | 266. | 6.3 | 655. |
| 6 | .620 | 266. | 6.3 | 656. |
| 7 | .620 | 266. | 6.3 | 656. |
| 8 | .580 | 249. | 6.5 | 655. |
| 9 | .630 | 271. | 6.5 | 654. |
| 10 | .630 | 271. | 6.5 | 654. |
| 11 | .590 | 253. | 6.7 | 659. |
| 12 | .650 | 279. | 7.0 | 651. |

| | | | | |
|---|---|---|---|---|
| 13 | .650 | 279. | 7.0 | 658. |
| 14 | .600 | 258. | 7.0 | 658. |
| 15 | .600 | 258. | 7.0 | 656. |
| 16 | .600 | 258. | 7.0 | 656. |
| 17 | .600 | 258. | 7.0 | 652. |
| 18 | .600 | 258. | 7.0 | 654. |
| 19 | .590 | 253. | 6.7 | 657. |
| 20 | .600 | 258. | 7.0 | 654. |
| 21 | .600 | 258. | 7.0 | 654. |
| 22 | .600 | 258. | 7.0 | 652. |
| 23 | .650 | 279. | 7.0 | 658. |
| 24 | .600 | 258. | 7.0 | 662. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.0 | 659. |
| 2 | .600 | 258. | 7.0 | 661. |
| 3 | .600 | 258. | 7.0 | 657. |
| 4 | .600 | 258. | 7.0 | 656. |
| 5 | .590 | 253. | 6.7 | 655. |
| 6 | .600 | 258. | 7.0 | 656. |
| 7 | .600 | 258. | 7.0 | 656. |
| 8 | .650 | 279. | 7.0 | 659. |
| 9 | .640 | 275. | 6.7 | 661. |
| 10 | .630 | 271. | 6.5 | 654. |
| 11 | .640 | 275. | 6.7 | 653. |
| 12 | .640 | 275. | 6.7 | 656. |
| 13 | .640 | 275. | 6.7 | 659. |
| 14 | .640 | 275. | 6.7 | 659. |
| 15 | .640 | 275. | 6.7 | 659. |
| 16 | .640 | 275. | 6.7 | 656. |
| 17 | .640 | 275. | 6.7 | 653. |
| 18 | .640 | 275. | 6.7 | 656. |
| 19 | .640 | 275. | 6.7 | 660. |
| 20 | .640 | 275. | 6.7 | 658. |
| 21 | .640 | 275. | 6.7 | 656. |
| 22 | .640 | 275. | 6.7 | 655. |
| 23 | .640 | 275. | 6.7 | 654. |
| 24 | .640 | 275. | 6.7 | 648. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 6.7 | 658. |
| 2 | .640 | 275. | 6.7 | 659. |
| 3 | .640 | 275. | 6.7 | 656. |
| 4 | .640 | 275. | 6.7 | 658. |
| 5 | .640 | 275. | 6.7 | 656. |
| 6 | .640 | 275. | 6.7 | 659. |
| 7 | .640 | 275. | 6.7 | 657. |
| 8 | .640 | 275. | 6.7 | 657. |
| 9 | .640 | 275. | 6.7 | 657. |
| 10 | .640 | 275. | 6.7 | 659. |
| 11 | .640 | 275. | 6.7 | 659. |

| | | | | |
|---|---|---|---|---|
| 12 | .640 | 275. | 6.7 | 661. |
| 13 | .640 | 275. | 6.7 | 660. |
| 14 | .640 | 275. | 6.7 | 662. |
| 15 | .640 | 275. | 6.7 | 650. |
| 16 | .640 | 275. | 6.7 | 656. |
| 17 | .650 | 279. | 7.0 | 658. |
| 18 | .650 | 279. | 7.0 | 656. |
| 19 | .650 | 279. | 7.0 | 659. |
| 20 | .650 | 279. | 7.0 | 659. |
| 21 | .650 | 279. | 7.0 | 655. |
| 22 | .650 | 279. | 7.0 | 653. |
| 23 | .640 | 275. | 6.7 | 657. |
| 24 | .640 | 275. | 6.7 | 655. |

DAY # 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .600 | 258. | 7.0 | 655. |
| 2 | .640 | 275. | 6.7 | 567. |
| 3 | .650 | 279. | 7.0 | 573. |
| 4 | .670 | 288. | 7.2 | 652. |
| 5 | .650 | 279. | 7.0 | 655. |
| 6 | .650 | 279. | 7.0 | 658. |
| 7 | .670 | 288. | 7.2 | 656. |
| 8 | .640 | 275. | 6.7 | 604. |
| 9 | .640 | 275. | 6.7 | 632. |
| 10 | .640 | 275. | 6.7 | 627. |
| 11 | .640 | 275. | 6.7 | 627. |
| 12 | .640 | 275. | 6.7 | 624. |
| 13 | .640 | 275. | 6.7 | 624. |
| 14 | .640 | 275. | 6.7 | 628. |
| 15 | .650 | 279. | 7.0 | 632. |
| 16 | .650 | 279. | 7.0 | 629. |
| 17 | .640 | 275. | 6.7 | 633. |
| 18 | .650 | 279. | 7.0 | 633. |
| 19 | .650 | 279. | 7.0 | 625. |
| 20 | .650 | 279. | 7.0 | 624. |
| 21 | .650 | 279. | 7.0 | 630. |
| 22 | .650 | 279. | 7.0 | 633. |
| 23 | .650 | 279. | 7.0 | 632. |
| 24 | .640 | 275. | 6.7 | 615. |

DAY # 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .640 | 275. | 6.7 | 631. |
| 2 | .650 | 279. | 7.0 | 613. |
| 3 | .600 | 258. | 7.0 | 554. |
| 4 | .570 | 245. | 7.5 | 507. |
| 5 | .630 | 271. | 7.7 | 443. |
| 6 | .630 | 271. | 7.7 | 437. |
| 7 | .640 | 275. | 8.0 | 435. |
| 8 | .690 | 296. | 7.7 | 437. |
| 9 | .720 | 309. | 7.2 | 502. |
| 10 | .670 | 288. | 7.2 | 643. |

| | | | | |
|---|---|---|---|---|
| 11 | .670 | 288. | 7.2 | 656. |
| 12 | .650 | 279. | 7.0 | 658. |
| 13 | .640 | 275. | 6.7 | 655. |
| 14 | .700 | 301. | 6.7 | 650. |
| 15 | .700 | 301. | 6.7 | 656. |
| 16 | .640 | 275. | 6.7 | 654. |
| 17 | .640 | 275. | 6.7 | 657. |
| 18 | .640 | 275. | 6.7 | 656. |
| 19 | .640 | 275. | 6.7 | 654. |
| 20 | .640 | 275. | 6.7 | 652. |
| 21 | .640 | 275. | 6.7 | 657. |
| 22 | .640 | 275. | 6.7 | 657. |
| 23 | .650 | 279. | 7.0 | 655. |
| 24 | .600 | 258. | 7.0 | 662. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.0 | 657. |
| 2 | .650 | 279. | 7.0 | 659. |
| 3 | .650 | 279. | 7.0 | 656. |
| 4 | .650 | 279. | 7.0 | 655. |
| 5 | .650 | 279. | 7.0 | 654. |
| 6 | .650 | 279. | 7.0 | 657. |
| 7 | .650 | 279. | 7.0 | 656. |
| 8 | .650 | 279. | 7.0 | 656. |
| 9 | .650 | 279. | 7.0 | 655. |
| 10 | .650 | 279. | 7.0 | 656. |
| 11 | .650 | 279. | 7.0 | 654. |
| 12 | .650 | 279. | 7.0 | 656. |
| 13 | .650 | 279. | 7.0 | 655. |
| 14 | .650 | 279. | 7.0 | 656. |
| 15 | .650 | 279. | 7.0 | 654. |
| 16 | .650 | 279. | 7.0 | 654. |
| 17 | .650 | 279. | 7.0 | 652. |
| 18 | .650 | 279. | 7.0 | 654. |
| 19 | .650 | 279. | 7.0 | 656. |
| 20 | .650 | 279. | 7.0 | 657. |
| 21 | .650 | 279. | 7.0 | 652. |
| 22 | .650 | 279. | 7.0 | 652. |
| 23 | .650 | 279. | 7.0 | 653. |
| 24 | .650 | 279. | 7.0 | 670. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.0 | 655. |
| 2 | .650 | 279. | 7.0 | 657. |
| 3 | .650 | 279. | 7.0 | 604. |
| 4 | .710 | 305. | 7.0 | 635. |
| 5 | .710 | 305. | 7.0 | 656. |
| 6 | .710 | 305. | 7.0 | 655. |
| 7 | .710 | 305. | 7.0 | 653. |
| 8 | .710 | 305. | 7.0 | 654. |
| 9 | .650 | 279. | 7.0 | 655. |

| | | | | |
|---|---|---|---|---|
| 10 | .650 | 279. | 7.0 | 655. |
| 11 | .600 | 258. | 7.0 | 652. |
| 12 | .600 | 258. | 7.0 | 659. |
| 13 | .650 | 279. | 7.0 | 653. |
| 14 | .650 | 279. | 7.0 | 655. |
| 15 | .640 | 275. | 6.7 | 656. |
| 16 | .640 | 275. | 6.7 | 656. |
| 17 | .710 | 305. | 7.0 | 657. |
| 18 | .640 | 275. | 6.7 | 656. |
| 19 | .650 | 279. | 7.0 | 655. |
| 20 | .650 | 279. | 7.0 | 654. |
| 21 | .640 | 275. | 6.7 | 654. |
| 22 | .650 | 279. | 7.0 | 655. |
| 23 | .710 | 305. | 7.0 | 656. |
| 24 | .710 | 305. | 7.0 | 647. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 7.0 | 657. |
| 2 | .650 | 279. | 7.0 | 657. |
| 3 | .650 | 279. | 7.0 | 657. |
| 4 | .650 | 279. | 7.0 | 659. |
| 5 | .650 | 279. | 7.0 | 655. |
| 6 | .650 | 279. | 7.0 | 653. |
| 7 | .650 | 279. | 7.0 | 654. |
| 8 | .650 | 279. | 7.0 | 657. |
| 9 | .650 | 279. | 7.0 | 655. |
| 10 | .650 | 279. | 7.0 | 655. |
| 11 | .650 | 279. | 7.0 | 653. |
| 12 | .650 | 279. | 7.0 | 656. |
| 13 | .650 | 279. | 7.0 | 655. |
| 14 | .650 | 279. | 7.0 | 656. |
| 15 | .650 | 279. | 7.0 | 652. |
| 16 | .650 | 279. | 7.0 | 652. |
| 17 | .650 | 279. | 7.0 | 657. |
| 18 | .640 | 275. | 7.0 | 661. |
| 19 | .640 | 275. | 6.7 | 661. |
| 20 | .640 | 275. | 6.7 | 661. |
| 21 | .640 | 275. | 6.7 | 661. |
| 22 | .640 | 275. | 6.7 | 658. |
| 23 | .640 | 275. | 6.7 | 657. |
| 24 | .680 | 292. | 6.7 | 638. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .690 | 296. | 6.5 | 652. |
| 2 | .690 | 296. | 6.5 | 653. |
| 3 | .690 | 296. | 6.5 | 656. |
| 4 | .690 | 296. | 6.5 | 656. |
| 5 | .690 | 296. | 6.5 | 654. |
| 6 | .690 | 296. | 6.5 | 653. |
| 7 | .690 | 296. | 6.5 | 654. |
| 8 | .690 | 296. | 6.5 | 655. |

| | | | | |
|---|---|---|---|---|
| 9 | .690 | 296. | 6.5 | 658. |
| 10 | .690 | 296. | 6.5 | 656. |
| 11 | .690 | 296. | 6.5 | 653. |
| 12 | .690 | 296. | 6.5 | 654. |
| 13 | .690 | 296. | 6.5 | 655. |
| 14 | .690 | 296. | 6.5 | 655. |
| 15 | .680 | 292. | 6.5 | 657. |
| 16 | .690 | 296. | 6.3 | 662. |
| 17 | .690 | 296. | 6.5 | 661. |
| 18 | .690 | 296. | 6.5 | 662. |
| 19 | .630 | 271. | 6.5 | 657. |
| 20 | .690 | 296. | 6.5 | 657. |
| 21 | .690 | 296. | 6.5 | 657. |
| 22 | .690 | 296. | 6.5 | 657. |
| 23 | .630 | 271. | 6.5 | 654. |
| 24 | .690 | 296. | 6.5 | 656. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .690 | 296. | 6.5 | 654. |
| 2 | .690 | 296. | 6.5 | 655. |
| 3 | .690 | 296. | 6.5 | 657. |
| 4 | .690 | 296. | 6.5 | 655. |
| 5 | .690 | 296. | 6.5 | 655. |
| 6 | .690 | 296. | 6.5 | 653. |
| 7 | .690 | 296. | 6.5 | 657. |
| 8 | .690 | 296. | 6.5 | 656. |
| 9 | .690 | 296. | 6.5 | 653. |
| 10 | .690 | 296. | 6.5 | 656. |
| 11 | .690 | 296. | 6.5 | 655. |
| 12 | .690 | 296. | 6.5 | 653. |
| 13 | .680 | 292. | 6.5 | 652. |
| 14 | .690 | 296. | 6.3 | 653. |
| 15 | .690 | 296. | 6.5 | 652. |
| 16 | .690 | 296. | 6.5 | 653. |
| 17 | .690 | 296. | 6.5 | 650. |
| 18 | .690 | 296. | 6.5 | 650. |
| 19 | .680 | 292. | 6.5 | 654. |
| 20 | .630 | 271. | 6.3 | 652. |
| 21 | .630 | 271. | 6.5 | 652. |
| 22 | .630 | 271. | 6.5 | 649. |
| 23 | .630 | 271. | 6.5 | 651. |
| 24 | .630 | 271. | 6.5 | 653. |

DAY = 46

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 653. |
| 2 | .630 | 271. | 6.5 | 651. |
| 3 | .630 | 271. | 6.5 | 651. |
| 4 | .680 | 292. | 6.5 | 652. |
| 5 | .690 | 296. | 6.3 | 654. |
| 6 | .630 | 271. | 6.5 | 654. |
| 7 | .630 | 271. | 6.5 | 651. |

| | | | | |
|---|---|---|---|---|
| 8 | .630 | 271. | 6.5 | 650. |
| 9 | .620 | 266. | 6.5 | 652. |
| 10 | .630 | 271. | 6.3 | 652. |
| 11 | .630 | 271. | 6.5 | 649. |
| 12 | .630 | 271. | 6.5 | 652. |
| 13 | .630 | 271. | 6.5 | 649. |
| 14 | .690 | 296. | 6.5 | 648. |
| 15 | .690 | 296. | 6.5 | 651. |
| 16 | .690 | 296. | 6.5 | 652. |
| 17 | .690 | 296. | 6.5 | 650. |
| 18 | .690 | 296. | 6.5 | 648. |
| 19 | .690 | 296. | 6.5 | 649. |
| 20 | .690 | 296. | 6.5 | 651. |
| 21 | .690 | 296. | 6.5 | 652. |
| 22 | .680 | 292. | 6.5 | 653. |
| 23 | .680 | 292. | 6.3 | 652. |
| 24 | .680 | 292. | 6.3 | 649. |

DAY # 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 649. |
| 2 | .680 | 292. | 6.3 | 651. |
| 3 | .740 | 318. | 6.3 | 651. |
| 4 | .750 | 322. | 6.3 | 653. |
| 5 | .690 | 296. | 6.5 | 653. |
| 6 | .690 | 296. | 6.5 | 651. |
| 7 | .690 | 296. | 6.5 | 650. |
| 8 | .680 | 292. | 6.5 | 653. |
| 9 | .680 | 292. | 6.3 | 655. |
| 10 | .680 | 292. | 6.3 | 655. |
| 11 | .680 | 292. | 6.3 | 656. |
| 12 | .680 | 292. | 6.3 | 651. |
| 13 | .680 | 292. | 6.3 | 653. |
| 14 | .680 | 292. | 6.3 | 651. |
| 15 | .680 | 292. | 6.3 | 654. |
| 16 | .680 | 292. | 6.3 | 653. |
| 17 | .680 | 292. | 6.3 | 653. |
| 18 | .680 | 292. | 6.3 | 650. |
| 19 | .680 | 292. | 6.3 | 653. |
| 20 | .680 | 292. | 6.3 | 657. |
| 21 | .680 | 292. | 6.3 | 655. |
| 22 | .680 | 292. | 6.3 | 652. |
| 23 | .680 | 292. | 6.3 | 651. |
| 24 | .680 | 292. | 6.3 | 651. |

DAY # 48

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 655. |
| 2 | .680 | 292. | 6.3 | 654. |
| 3 | .680 | 292. | 6.3 | 653. |
| 4 | .680 | 292. | 6.5 | 650. |
| 5 | .680 | 292. | 6.3 | 653. |
| 6 | .680 | 292. | 6.3 | 654. |

| | | | | |
|---|---|---|---|---|
| 7 | .690 | 296. | 6.3 | 655. |
| 8 | .680 | 292. | 6.5 | 656. |
| 9 | .680 | 292. | 6.3 | 656. |
| 10 | .680 | 292. | 6.3 | 655. |
| 11 | .680 | 292. | 6.3 | 654. |
| 12 | .670 | 288. | 6.3 | 657. |
| 13 | .670 | 288. | 6.0 | 658. |
| 14 | .670 | 288. | 6.0 | 657. |
| 15 | .670 | 288. | 6.0 | 653. |
| 16 | .670 | 288. | 6.0 | 647. |
| 17 | .670 | 288. | 6.0 | 653. |
| 18 | .610 | 262. | 6.0 | 660. |
| 19 | .610 | 262. | 6.0 | 652. |
| 20 | .620 | 266. | 6.0 | 651. |
| 21 | .610 | 262. | 6.3 | 645. |
| 22 | .620 | 266. | 6.0 | 654. |
| 23 | .710 | 305. | 6.3 | 661. |
| 24 | .690 | 296. | 6.7 | 660. |

DAY # 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.5 | 656. |
| 2 | .620 | 266. | 6.3 | 655. |
| 3 | .680 | 292. | 6.3 | 654. |
| 4 | .680 | 292. | 6.3 | 658. |
| 5 | .670 | 288. | 6.3 | 647. |
| 6 | .670 | 288. | 6.0 | 650. |
| 7 | .670 | 288. | 6.0 | 652. |
| 8 | .680 | 292. | 6.0 | 652. |
| 9 | .680 | 292. | 6.3 | 649. |
| 10 | .740 | 318. | 6.3 | 648. |
| 11 | .670 | 288. | 6.3 | 650. |
| 12 | .670 | 288. | 6.0 | 652. |
| 13 | .670 | 288. | 6.0 | 655. |
| 14 | .670 | 288. | 6.0 | 652. |
| 15 | .670 | 288. | 6.0 | 665. |
| 16 | .680 | 292. | 6.0 | 655. |
| 17 | .670 | 288. | 6.3 | 649. |
| 18 | .670 | 288. | 6.0 | 654. |
| 19 | .670 | 288. | 6.0 | 655. |
| 20 | .680 | 292. | 6.0 | 654. |
| 21 | .680 | 292. | 6.3 | 653. |
| 22 | .680 | 292. | 6.3 | 655. |
| 23 | .680 | 292. | 6.3 | 655. |
| 24 | .680 | 292. | 6.3 | 649. |

DAY # 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 655. |
| 2 | .680 | 292. | 6.3 | 654. |
| 3 | .680 | 292. | 6.3 | 655. |
| 4 | .680 | 292. | 6.3 | 656. |
| 5 | .680 | 292. | 6.3 | 654. |

| | | | | |
|---|---|---|---|---|
| 6 | .680 | 292. | 6.3 | 656. |
| 7 | .680 | 292. | 6.3 | 655. |
| 8 | .680 | 292. | 6.3 | 656. |
| 9 | .680 | 292. | 6.3 | 657. |
| 10 | .680 | 292. | 6.3 | 653. |
| 11 | .680 | 292. | 6.3 | 653. |
| 12 | .680 | 292. | 6.3 | 650. |
| 13 | .680 | 292. | 6.3 | 654. |
| 14 | .680 | 292. | 6.3 | 656. |
| 15 | .680 | 292. | 6.3 | 657. |
| 16 | .680 | 292. | 6.3 | 654. |
| 17 | .680 | 292. | 6.3 | 654. |
| 18 | .740 | 318. | 6.3 | 651. |
| 19 | .680 | 292. | 6.3 | 652. |
| 20 | .680 | 292. | 6.3 | 654. |
| 21 | .680 | 292. | 6.3 | 655. |
| 22 | .680 | 292. | 6.3 | 654. |
| 23 | .750 | 322. | 6.3 | 653. |
| 24 | .740 | 318. | 6.5 | 650. |

DAY = 51

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .750 | 322. | 6.3 | 657. |
| 2 | .750 | 322. | 6.5 | 658. |
| 3 | .750 | 322. | 6.5 | 658. |
| 4 | .750 | 322. | 6.5 | 656. |
| 5 | .760 | 326. | 6.5 | 654. |
| 6 | .690 | 296. | 6.7 | 656. |
| 7 | .670 | 288. | 6.5 | 649. |
| 8 | .670 | 288. | 6.0 | 652. |
| 9 | .670 | 288. | 6.0 | 653. |
| 10 | .670 | 288. | 6.0 | 650. |
| 11 | .660 | 284. | 6.0 | 652. |
| 12 | .660 | 284. | 5.7 | 653. |
| 13 | .710 | 305. | 5.7 | 654. |
| 14 | .660 | 284. | 5.7 | 656. |
| 15 | .660 | 284. | 5.7 | 653. |
| 16 | .660 | 284. | 5.7 | 650. |
| 17 | .660 | 284. | 5.7 | 649. |
| 18 | .660 | 284. | 5.7 | 652. |
| 19 | .660 | 284. | 5.7 | 651. |
| 20 | .660 | 284. | 5.7 | 652. |
| 21 | .660 | 284. | 5.7 | 650. |
| 22 | .660 | 284. | 5.7 | 650. |
| 23 | .660 | 284. | 5.7 | 654. |
| 24 | .670 | 288. | 5.7 | 654. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .670 | 288. | 6.0 | 654. |
| 2 | .670 | 288. | 6.0 | 654. |
| 3 | .670 | 288. | 6.0 | 655. |
| 4 | .670 | 288. | 6.0 | 653. |

| | | | | |
|---|---|---|---|---|
| 5 | .670 | 288. | 6.0 | 654. |
| 6 | .670 | 288. | 6.0 | 655. |
| 7 | .670 | 288. | 6.0 | 655. |
| 8 | .670 | 288. | 6.0 | 655. |
| 9 | .670 | 288. | 6.0 | 656. |
| 10 | .670 | 288. | 6.0 | 654. |
| 11 | .660 | 284. | 6.0 | 651. |
| 12 | .660 | 284. | 5.7 | 661. |
| 13 | .660 | 284. | 5.7 | 649. |
| 14 | .660 | 284. | 5.7 | 651. |
| 15 | .600 | 258. | 5.7 | 654. |
| 16 | .600 | 258. | 5.7 | 653. |
| 17 | .600 | 258. | 5.7 | 649. |
| 18 | .600 | 258. | 5.7 | 650. |
| 19 | .660 | 284. | 5.7 | 653. |
| 20 | .660 | 284. | 5.7 | 651. |
| 21 | .660 | 284. | 5.7 | 650. |
| 22 | .660 | 284. | 5.7 | 651. |
| 23 | .660 | 284. | 5.7 | 650. |
| 24 | .660 | 284. | 5.7 | 658. |

DAY = 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .740 | 318. | 6.5 | 609. |
| 2 | .720 | 309. | 6.3 | 606. |
| 3 | .720 | 309. | 6.0 | 610. |
| 4 | .720 | 309. | 6.0 | 637. |
| 5 | .720 | 309. | 6.0 | 669. |
| 6 | .660 | 284. | 6.0 | 666. |
| 7 | .670 | 288. | 5.7 | 663. |
| 8 | .720 | 309. | 6.0 | 666. |
| 9 | .720 | 309. | 6.0 | 665. |
| 10 | .660 | 284. | 6.0 | 664. |
| 11 | .650 | 279. | 5.7 | 664. |
| 12 | .660 | 284. | 5.5 | 661. |
| 13 | .600 | 258. | 5.7 | 660. |
| 14 | .670 | 288. | 5.7 | 662. |
| 15 | .670 | 288. | 6.0 | 664. |
| 16 | .670 | 288. | 6.0 | 662. |
| 17 | .670 | 288. | 6.0 | 658. |
| 18 | .670 | 288. | 6.0 | 659. |
| 19 | .670 | 288. | 6.0 | 661. |
| 20 | .670 | 288. | 6.0 | 661. |
| 21 | .670 | 288. | 6.0 | 662. |
| 22 | .670 | 288. | 6.0 | 659. |
| 23 | .670 | 288. | 6.0 | 660. |
| 24 | .670 | 288. | 6.0 | 663. |

DAY = 63

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .670 | 288. | 6.0 | 660. |
| 2 | .670 | 288. | 6.0 | 658. |
| 3 | .670 | 288. | 6.0 | 657. |

| | | | | |
|---|---|---|---|---|
| 4 | .670 | 288. | 6.0 | 660. |
| 5 | .670 | 288. | 6.0 | 661. |
| 6 | .600 | 258. | 6.0 | 662. |
| 7 | .600 | 258. | 5.7 | 660. |
| 8 | .660 | 284. | 5.7 | 656. |
| 9 | .660 | 284. | 5.7 | 658. |
| 10 | .670 | 288. | 5.7 | 660. |
| 11 | .670 | 288. | 6.0 | 659. |
| 12 | .670 | 288. | 6.0 | 655. |
| 13 | .670 | 288. | 6.0 | 664. |
| 14 | .670 | 288. | 6.0 | 659. |
| 15 | .670 | 288. | 6.0 | 655. |
| 16 | .610 | 262. | 6.0 | 657. |
| 17 | .610 | 262. | 6.0 | 662. |
| 18 | .610 | 262. | 6.0 | 661. |
| 19 | .680 | 292. | 6.0 | 661. |
| 20 | .680 | 292. | 6.3 | 661. |
| 21 | .670 | 288. | 6.3 | 660. |
| 22 | .680 | 292. | 6.0 | 660. |
| 23 | .670 | 288. | 6.3 | 662. |
| 24 | .680 | 292. | 6.0 | 657. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 658. |
| 2 | .670 | 288. | 6.3 | 658. |
| 3 | .680 | 292. | 6.0 | 660. |
| 4 | .680 | 292. | 6.3 | 658. |
| 5 | .680 | 292. | 6.3 | 659. |
| 6 | .680 | 292. | 6.3 | 665. |
| 7 | .680 | 292. | 6.3 | 663. |
| 8 | .680 | 292. | 6.3 | 663. |
| 9 | .680 | 292. | 6.3 | 659. |
| 10 | .690 | 296. | 6.3 | 664. |
| 11 | .680 | 292. | 6.5 | 659. |
| 12 | .670 | 288. | 6.3 | 658. |
| 13 | .670 | 288. | 6.0 | 658. |
| 14 | .720 | 309. | 6.0 | 655. |
| 15 | .720 | 309. | 6.0 | 661. |
| 16 | .720 | 309. | 6.0 | 660. |
| 17 | .720 | 309. | 6.0 | 660. |
| 18 | .740 | 318. | 6.0 | 665. |
| 19 | .740 | 318. | 6.3 | 659. |
| 20 | .740 | 318. | 6.3 | 660. |
| 21 | .650 | 279. | 6.3 | 660. |
| 22 | .730 | 314. | 5.5 | 661. |
| 23 | .780 | 335. | 7.2 | 647. |
| 24 | .780 | 335. | 7.0 | 596. |

DAY = 65

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .780 | 335. | 7.0 | 625. |
| 2 | .780 | 335. | 7.0 | 627. |

| | | | | |
|---|---|---|---|---|
| 3 | .780 | 335. | 7.0 | 632. |
| 4 | .780 | 335. | 7.0 | 638. |
| 5 | .780 | 335. | 7.0 | 635. |
| 6 | .780 | 335. | 7.0 | 637. |
| 7 | .780 | 335. | 7.0 | 633. |
| 8 | .780 | 335. | 7.0 | 636. |
| 9 | .710 | 305. | 7.0 | 633. |
| 10 | .690 | 296. | 6.7 | 637. |
| 11 | .680 | 292. | 6.5 | 639. |
| 12 | .670 | 288. | 6.3 | 651. |
| 13 | .680 | 292. | 6.0 | 658. |
| 14 | .690 | 296. | 6.3 | 660. |
| 15 | .690 | 296. | 6.5 | 660. |
| 16 | .690 | 296. | 6.5 | 659. |
| 17 | .690 | 296. | 6.5 | 658. |
| 18 | .690 | 296. | 6.5 | 660. |
| 19 | .690 | 296. | 6.5 | 660. |
| 20 | .690 | 296. | 6.5 | 661. |
| 21 | .690 | 296. | 6.5 | 661. |
| 22 | .690 | 296. | 6.5 | 662. |
| 23 | .690 | 296. | 6.5 | 663. |
| 24 | .630 | 271. | 6.5 | 666. |

DAY # 66

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 661. |
| 2 | .630 | 271. | 6.5 | 605. |
| 3 | .630 | 271. | 6.5 | 590. |
| 4 | .630 | 271. | 6.5 | 588. |
| 5 | .690 | 296. | 6.5 | 586. |
| 6 | .690 | 296. | 6.5 | 587. |
| 7 | .710 | 305. | 6.5 | 615. |
| 8 | .650 | 279. | 6.7 | 667. |
| 9 | .710 | 305. | 6.7 | 601. |
| 10 | .720 | 309. | 6.7 | 529. |
| 11 | .710 | 305. | 7.0 | 633. |
| 12 | .710 | 305. | 6.7 | 662. |
| 13 | .710 | 305. | 6.7 | 661. |
| 14 | .710 | 305. | 6.7 | 661. |
| 15 | .710 | 305. | 6.7 | 661. |
| 16 | .710 | 305. | 6.7 | 663. |
| 17 | .710 | 305. | 6.7 | 666. |
| 18 | .710 | 305. | 6.7 | 662. |
| 19 | .690 | 296. | 6.7 | 661. |
| 20 | .690 | 296. | 6.5 | 658. |
| 21 | .600 | 258. | 6.5 | 665. |
| 22 | .580 | 249. | 7.0 | 663. |
| 23 | .580 | 249. | 8.0 | 556. |
| 24 | .580 | 249. | 8.0 | 427. |

DAY # 67

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .660 | 284. | 8.0 | 425. |

| | | | | |
|---|---|---|---|---|
| 2 | .730 | 314. | 7.0 | 433. |
| 3 | .680 | 292. | 7.2 | 561. |
| 4 | .750 | 322. | 7.5 | 610. |
| 5 | .750 | 322. | 7.5 | 601. |
| 6 | .780 | 335. | 7.5 | 601. |
| 7 | .780 | 335. | 7.0 | 634. |
| 8 | .780 | 335. | 7.0 | 664. |
| 9 | .780 | 335. | 7.0 | 662. |
| 10 | .780 | 335. | 7.0 | 659. |
| 11 | .780 | 335. | 7.0 | 660. |
| 12 | .760 | 326. | 7.0 | 661. |
| 13 | .750 | 322. | 6.7 | 659. |
| 14 | .760 | 326. | 6.5 | 661. |
| 15 | .750 | 322. | 7.0 | 660. |
| 16 | .750 | 322. | 7.5 | 663. |
| 17 | .780 | 335. | 7.5 | 665. |
| 18 | .750 | 322. | 7.0 | 662. |
| 19 | .750 | 322. | 6.5 | 658. |
| 20 | .750 | 322. | 6.5 | 661. |
| 21 | .760 | 326. | 6.5 | 662. |
| 22 | .820 | 352. | 6.7 | 663. |
| 23 | .780 | 335. | 6.7 | 662. |
| 24 | .710 | 305. | 7.0 | 654. |

DAY = 68

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .690 | 296. | 6.7 | 619. |
| 2 | .820 | 352. | 6.5 | 580. |
| 3 | .820 | 352. | 6.7 | 661. |
| 4 | .820 | 352. | 6.7 | 661. |
| 5 | .820 | 352. | 6.7 | 660. |
| 6 | .820 | 352. | 6.7 | 659. |
| 7 | .820 | 352. | 6.7 | 661. |
| 8 | .760 | 326. | 6.7 | 663. |
| 9 | .760 | 326. | 6.7 | 661. |
| 10 | .760 | 326. | 6.7 | 661. |
| 11 | .760 | 326. | 6.7 | 659. |
| 12 | .750 | 322. | 6.7 | 657. |
| 13 | .750 | 322. | 6.5 | 659. |
| 14 | .750 | 322. | 6.5 | 661. |
| 15 | .750 | 322. | 6.5 | 658. |
| 16 | .690 | 296. | 6.5 | 659. |
| 17 | .690 | 296. | 6.5 | 662. |
| 18 | .690 | 296. | 6.5 | 656. |
| 19 | .690 | 296. | 6.5 | 654. |
| 20 | .690 | 296. | 6.5 | 657. |
| 21 | .690 | 296. | 6.5 | 659. |
| 22 | .690 | 296. | 6.5 | 660. |
| 23 | .690 | 296. | 6.5 | 661. |
| 24 | .690 | 296. | 6.5 | 662. |

DAY = 69

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .690 | 296. | 6.5 | 657. |
| 2 | .690 | 296. | 6.5 | 655. |
| 3 | .690 | 296. | 6.5 | 659. |
| 4 | .690 | 296. | 6.5 | 659. |
| 5 | .690 | 296. | 6.5 | 658. |
| 6 | .690 | 296. | 6.5 | 656. |
| 7 | .680 | 292. | 6.5 | 658. |
| 8 | .690 | 296. | 6.3 | 658. |
| 9 | .690 | 296. | 6.5 | 659. |
| 10 | .680 | 292. | 6.5 | 655. |
| 11 | .680 | 292. | 6.3 | 656. |
| 12 | .680 | 292. | 6.3 | 655. |
| 13 | .680 | 292. | 6.3 | 657. |
| 14 | .680 | 292. | 6.3 | 656. |
| 15 | .680 | 292. | 6.3 | 654. |
| 16 | .680 | 292. | 6.3 | 659. |
| 17 | .710 | 305. | 6.3 | 656. |
| 18 | .690 | 296. | 6.7 | 660. |
| 19 | .690 | 296. | 6.5 | 657. |
| 20 | .690 | 296. | 6.5 | 655. |
| 21 | .690 | 296. | 6.5 | 652. |
| 22 | .690 | 296. | 6.5 | 656. |
| 23 | .680 | 292. | 6.5 | 661. |
| 24 | .680 | 292. | 6.3 | 659. |

DAY # 70

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .710 | 305. | 6.3 | 655. |
| 2 | .660 | 284. | 6.7 | 657. |
| 3 | .660 | 284. | 7.0 | 657. |
| 4 | .720 | 309. | 7.0 | 653. |
| 5 | .720 | 309. | 7.0 | 653. |
| 6 | .720 | 309. | 7.0 | 657. |
| 7 | .720 | 309. | 7.0 | 657. |
| 8 | .720 | 309. | 7.0 | 659. |
| 9 | .720 | 309. | 7.0 | 656. |
| 10 | .720 | 309. | 7.0 | 656. |
| 11 | .660 | 284. | 7.0 | 657. |
| 12 | .660 | 284. | 7.0 | 658. |
| 13 | .660 | 284. | 7.0 | 656. |
| 14 | .660 | 284. | 7.0 | 658. |
| 15 | .660 | 284. | 7.0 | 655. |
| 16 | .660 | 284. | 7.0 | 655. |
| 17 | .660 | 284. | 7.0 | 653. |
| 18 | .650 | 279. | 7.0 | 655. |
| 19 | .650 | 279. | 6.7 | 657. |
| 20 | .650 | 279. | 6.7 | 655. |
| 21 | .650 | 279. | 6.7 | 653. |
| 22 | .650 | 279. | 6.7 | 652. |
| 23 | .650 | 279. | 6.7 | 655. |
| 24 | .650 | 279. | 6.7 | 659. |

DAY # 71

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .650 | 279. | 6.7 | 653. |
| 2 | .650 | 279. | 6.7 | 653. |
| 3 | .650 | 279. | 6.7 | 655. |
| 4 | .650 | 279. | 6.7 | 657. |
| 5 | .650 | 279. | 6.7 | 660. |
| 6 | .710 | 305. | 6.7 | 657. |
| 7 | .650 | 279. | 6.7 | 655. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | .650 | 279. | 6.7 | 654. |
| 10 | .650 | 279. | 6.7 | 656. |
| 11 | .650 | 279. | 6.7 | 654. |
| 12 | .650 | 279. | 6.7 | 652. |
| 13 | .650 | 279. | 6.7 | 654. |
| 14 | .650 | 279. | 6.7 | 654. |
| 15 | .650 | 279. | 6.7 | 652. |
| 16 | .650 | 279. | 6.7 | 656. |
| 17 | .650 | 279. | 6.7 | 652. |
| 18 | .650 | 279. | 6.7 | 653. |
| 19 | .650 | 279. | 6.7 | 652. |
| 20 | .650 | 279. | 6.7 | 655. |
| 21 | .650 | 279. | 6.7 | 656. |
| 22 | .650 | 279. | 6.7 | 653. |
| 23 | .650 | 279. | 6.7 | 656. |
| 24 | .650 | 279. | 6.7 | 663. |

DAY = 72

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 6.7 | 651. |
| 2 | .650 | 279. | 6.7 | 647. |
| 3 | .590 | 253. | 6.7 | 633. |
| 4 | .650 | 279. | 6.7 | 633. |
| 5 | .650 | 279. | 6.7 | 630. |
| 6 | .650 | 279. | 6.7 | 637. |
| 7 | .650 | 279. | 6.7 | 636. |
| 8 | .650 | 279. | 6.7 | 639. |
| 9 | .650 | 279. | 6.7 | 646. |
| 10 | .650 | 279. | 6.7 | 640. |
| 11 | .590 | 253. | 6.7 | 640. |
| 12 | .650 | 279. | 6.7 | 645. |
| 13 | .650 | 279. | 6.7 | 641. |
| 14 | .650 | 279. | 6.7 | 647. |
| 15 | .650 | 279. | 6.7 | 641. |
| 16 | .650 | 279. | 6.7 | 637. |
| 17 | .590 | 253. | 6.7 | 642. |
| 18 | .610 | 262. | 7.2 | 633. |
| 19 | .550 | 236. | 7.2 | 596. |
| 20 | .590 | 253. | 6.7 | 515. |
| 21 | .650 | 279. | 6.7 | 640. |
| 22 | .650 | 279. | 6.7 | 649. |
| 23 | .650 | 279. | 6.7 | 649. |
| 24 | .650 | 279. | 6.7 | 632. |

DAY = 73

| NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 6.7 | 648. |
| 2 | .650 | 279. | 6.7 | 651. |
| 3 | .650 | 279. | 6.7 | 648. |
| 4 | .650 | 279. | 6.7 | 654. |
| 5 | .650 | 279. | 6.7 | 654. |
| 6 | .650 | 279. | 6.7 | 655. |
| 7 | .650 | 279. | 6.7 | 653. |
| 8 | .650 | 279. | 6.7 | 653. |
| 9 | .630 | 271. | 6.5 | 656. |
| 10 | .630 | 271. | 6.5 | 655. |
| 11 | .630 | 271. | 6.5 | 654. |
| 12 | .630 | 271. | 6.5 | 657. |
| 13 | .650 | 279. | 6.7 | 652. |
| 14 | .630 | 271. | 6.5 | 650. |
| 15 | .620 | 266. | 6.3 | 654. |
| 16 | .620 | 266. | 6.3 | 652. |
| 17 | .630 | 271. | 6.5 | 653. |
| 18 | .630 | 271. | 6.5 | 651. |
| 19 | .630 | 271. | 6.5 | 651. |
| 20 | .630 | 271. | 6.5 | 653. |
| 21 | .620 | 266. | 6.3 | 654. |
| 22 | .620 | 266. | 6.3 | 654. |
| 23 | .630 | 271. | 6.5 | 655. |
| 24 | .630 | 271. | 6.5 | 659. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 652. |
| 2 | .630 | 271. | 6.5 | 650. |
| 3 | .620 | 266. | 6.3 | 653. |
| 4 | .630 | 271. | 6.5 | 656. |
| 5 | .630 | 271. | 6.5 | 655. |
| 6 | .630 | 271. | 6.5 | 653. |
| 7 | .630 | 271. | 6.5 | 651. |
| 8 | .620 | 266. | 6.3 | 654. |
| 9 | .620 | 266. | 6.3 | 654. |
| 10 | .620 | 266. | 6.3 | 657. |
| 11 | .620 | 266. | 6.3 | 655. |
| 12 | .630 | 271. | 6.5 | 651. |
| 13 | .630 | 271. | 6.5 | 651. |
| 14 | .620 | 266. | 6.3 | 648. |
| 15 | .620 | 266. | 6.3 | 653. |
| 16 | .570 | 245. | 6.3 | 649. |
| 17 | .620 | 266. | 6.3 | 654. |
| 18 | .620 | 266. | 6.3 | 649. |
| 19 | .620 | 266. | 6.3 | 651. |
| 20 | .620 | 266. | 6.3 | 653. |
| 21 | .620 | 266. | 6.3 | 655. |
| 22 | .620 | 266. | 6.3 | 656. |
| 23 | .630 | 271. | 6.5 | 655. |
| 24 | .630 | 271. | 6.5 | 664. |

DAY = 75

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 654. |
| 2 | .630 | 271. | 6.5 | 652. |
| 3 | .580 | 249. | 6.5 | 652. |
| 4 | .620 | 266. | 6.3 | 616. |
| 5 | .620 | 266. | 6.3 | 608. |
| 6 | .630 | 271. | 6.5 | 619. |
| 7 | .630 | 271. | 6.5 | 617. |
| 8 | .630 | 271. | 6.5 | 622. |
| 9 | .620 | 266. | 6.3 | 624. |
| 10 | .620 | 266. | 6.3 | 631. |
| 11 | .630 | 271. | 6.5 | 633. |
| 12 | .630 | 271. | 6.5 | 636. |
| 13 | .620 | 266. | 6.3 | 641. |
| 14 | .620 | 266. | 6.3 | 636. |
| 15 | .620 | 266. | 6.3 | 647. |
| 16 | .620 | 266. | 6.3 | 651. |
| 17 | .620 | 266. | 6.3 | 652. |
| 18 | .620 | 266. | 6.3 | 653. |
| 19 | .620 | 266. | 6.3 | 649. |
| 20 | .620 | 266. | 6.3 | 647. |
| 21 | .620 | 266. | 6.3 | 649. |
| 22 | .570 | 245. | 6.3 | 652. |
| 23 | .510 | 219. | 6.3 | 632. |
| 24 | .570 | 245. | 6.3 | 570. |

DAY # 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.3 | 605. |
| 2 | .570 | 245. | 6.3 | 610. |
| 3 | .570 | 245. | 6.3 | 612. |
| 4 | .570 | 245. | 6.3 | 611. |
| 5 | .570 | 245. | 6.3 | 619. |
| 6 | .620 | 266. | 6.3 | 617. |
| 7 | .620 | 266. | 6.3 | 614. |
| 8 | .620 | 266. | 6.3 | 620. |
| 9 | .620 | 266. | 6.3 | 625. |
| 10 | .620 | 266. | 6.3 | 622. |
| 11 | .620 | 266. | 6.3 | 621. |
| 12 | .570 | 245. | 6.3 | 619. |
| 13 | .570 | 245. | 6.3 | 618. |
| 14 | .570 | 245. | 6.3 | 620. |
| 15 | .570 | 245. | 6.3 | 616. |
| 16 | .570 | 245. | 6.3 | 615. |
| 17 | .570 | 245. | 6.3 | 619. |
| 18 | .570 | 245. | 6.3 | 616. |
| 19 | .570 | 245. | 6.3 | 616. |
| 20 | .570 | 245. | 6.3 | 617. |
| 21 | .570 | 245. | 6.3 | 614. |
| 22 | .570 | 245. | 6.3 | 616. |
| 23 | .570 | 245. | 6.3 | 618. |
| 24 | .620 | 266. | 6.3 | 615. |

DAY # 77

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 6.3 | 626. |
| 2 | .620 | 266. | 6.3 | 648. |
| 3 | .620 | 266. | 6.3 | 652. |
| 4 | .620 | 266. | 6.3 | 653. |
| 5 | .620 | 266. | 6.3 | 655. |
| 6 | .620 | 266. | 6.3 | 653. |
| 7 | .620 | 266. | 6.3 | 653. |
| 8 | .620 | 266. | 6.3 | 652. |
| 9 | .620 | 266. | 6.3 | 653. |
| 10 | .620 | 266. | 6.3 | 654. |
| 11 | .620 | 266. | 6.3 | 654. |
| 12 | .570 | 245. | 6.3 | 654. |
| 13 | .570 | 245. | 6.3 | 652. |
| 14 | .570 | 245. | 6.3 | 650. |
| 15 | .570 | 245. | 6.3 | 651. |
| 16 | .570 | 245. | 6.3 | 650. |
| 17 | .570 | 245. | 6.3 | 653. |
| 18 | .570 | 245. | 6.3 | 652. |
| 19 | .580 | 249. | 6.5 | 651. |
| 20 | .580 | 249. | 6.5 | 651. |
| 21 | .580 | 249. | 6.5 | 649. |
| 22 | .580 | 249. | 6.5 | 654. |
| 23 | .580 | 249. | 6.5 | 653. |
| 24 | .580 | 249. | 6.5 | 662. |

DAY = 78



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 657. |
| 2 | .580 | 249. | 6.5 | 654. |
| 3 | .580 | 249. | 6.5 | 655. |
| 4 | .580 | 249. | 6.5 | 655. |
| 5 | .630 | 271. | 6.5 | 654. |
| 6 | .630 | 271. | 6.5 | 657. |
| 7 | .630 | 271. | 6.5 | 659. |
| 8 | .630 | 271. | 6.5 | 657. |
| 9 | .630 | 271. | 6.5 | 654. |
| 10 | .630 | 271. | 6.5 | 653. |
| 11 | .630 | 271. | 6.5 | 653. |
| 12 | .570 | 245. | 6.3 | 653. |
| 13 | .620 | 266. | 6.3 | 653. |
| 14 | .620 | 266. | 6.3 | 654. |
| 15 | .620 | 266. | 6.3 | 655. |
| 16 | .620 | 266. | 6.3 | 655. |
| 17 | .580 | 249. | 6.5 | 652. |
| 18 | .570 | 245. | 6.3 | 654. |
| 19 | .580 | 249. | 6.5 | 653. |
| 20 | .620 | 266. | 6.3 | 651. |
| 21 | .630 | 271. | 6.5 | 654. |
| 22 | .630 | 271. | 6.5 | 654. |
| 23 | .630 | 271. | 6.5 | 654. |
| 24 | .630 | 271. | 6.5 | 650. |

DAY = 79

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 654. |
| 2 | .620 | 266. | 6.3 | 650. |
| 3 | .580 | 249. | 6.5 | 661. |
| 4 | .630 | 271. | 6.5 | 654. |
| 5 | .630 | 271. | 6.5 | 655. |
| 6 | .630 | 271. | 6.5 | 657. |
| 7 | .630 | 271. | 6.5 | 655. |
| 8 | .630 | 271. | 6.5 | 656. |
| 9 | .620 | 266. | 6.3 | 654. |
| 10 | .630 | 271. | 6.5 | 653. |
| 11 | .630 | 271. | 6.5 | 653. |
| 12 | .630 | 271. | 6.5 | 654. |
| 13 | .630 | 271. | 6.5 | 651. |
| 14 | .620 | 266. | 6.3 | 654. |
| 15 | .620 | 266. | 6.3 | 656. |
| 16 | .630 | 271. | 6.5 | 657. |
| 17 | .630 | 271. | 6.5 | 653. |
| 18 | .580 | 249. | 6.5 | 653. |
| 19 | .570 | 245. | 6.3 | 652. |
| 20 | .620 | 266. | 6.3 | 656. |
| 21 | .620 | 266. | 6.3 | 657. |
| 22 | .620 | 266. | 6.3 | 658. |
| 23 | .620 | 266. | 6.3 | 657. |
| 24 | .630 | 271. | 6.5 | 659. |

DAY = 80



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 6.5 | 651. |
| 2 | .630 | 271. | 6.5 | 655. |
| 3 | .620 | 266. | 6.3 | 655. |
| 4 | .620 | 266. | 6.3 | 656. |
| 5 | .630 | 271. | 6.5 | 657. |
| 6 | .630 | 271. | 6.5 | 655. |
| 7 | .630 | 271. | 6.5 | 653. |
| 8 | .630 | 271. | 6.5 | 655. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .630 | 271. | 6.5 | 650. |
| 11 | .630 | 271. | 6.5 | 652. |
| 12 | .630 | 271. | 6.5 | 654. |
| 13 | .630 | 271. | 6.5 | 652. |
| 14 | .630 | 271. | 6.5 | 651. |
| 15 | .630 | 271. | 6.5 | 651. |
| 16 | .630 | 271. | 6.5 | 655. |
| 17 | .630 | 271. | 6.5 | 654. |
| 18 | .630 | 271. | 6.5 | 656. |
| 19 | .630 | 271. | 6.5 | 651. |
| 20 | .620 | 266. | 6.3 | 650. |
| 21 | .620 | 266. | 6.3 | 654. |
| 22 | .630 | 271. | 6.5 | 655. |
| 23 | .630 | 271. | 6.5 | 652. |
| 24 | .620 | 266. | 6.3 | 651. |

DAY = 82

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | -1.000 | -430. | -1.0 | -1. |
| 4 | -1.000 | -430. | -1.0 | -1. |
| 5 | .410 | 176. | 14.5 | 86. |
| 6 | .570 | 245. | 12.0 | 138. |
| 7 | .490 | 210. | 9.0 | 259. |
| 8 | .730 | 314. | 7.2 | 431. |
| 9 | .750 | 322. | 6.5 | 591. |
| 10 | .690 | 296. | 6.5 | 659. |
| 11 | .680 | 292. | 6.3 | 657. |
| 12 | .670 | 288. | 6.0 | 657. |
| 13 | .670 | 288. | 6.0 | 656. |
| 14 | .720 | 309. | 6.0 | 655. |
| 15 | .720 | 309. | 6.0 | 657. |
| 16 | .720 | 309. | 6.0 | 655. |
| 17 | .710 | 305. | 5.7 | 654. |
| 18 | .710 | 305. | 5.7 | 656. |
| 19 | .710 | 305. | 5.7 | 656. |
| 20 | .710 | 305. | 5.7 | 656. |
| 21 | .710 | 305. | 5.7 | 656. |
| 22 | .710 | 305. | 5.7 | 655. |
| 23 | .700 | 301. | 5.5 | 657. |
| 24 | .700 | 301. | 5.5 | 681. |

DAY # 83



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .710 | 305. | 5.7 | 655. |
| 2 | .710 | 305. | 5.7 | 657. |
| 3 | .710 | 305. | 5.7 | 657. |
| 4 | .710 | 305. | 5.7 | 657. |
| 5 | .660 | 284. | 5.7 | 655. |
| 6 | .660 | 284. | 5.7 | 658. |
| 7 | .660 | 284. | 5.7 | 658. |
| 8 | .710 | 305. | 5.7 | 658. |
| 9 | .710 | 305. | 5.7 | 656. |
| 10 | .710 | 305. | 5.7 | 653. |
| 11 | .710 | 305. | 5.7 | 656. |
| 12 | .710 | 305. | 5.7 | 655. |
| 13 | .720 | 309. | 6.0 | 652. |
| 14 | .710 | 305. | 5.7 | 654. |
| 15 | .710 | 305. | 5.7 | 656. |
| 16 | .710 | 305. | 5.7 | 654. |
| 17 | .720 | 309. | 6.0 | 658. |
| 18 | .710 | 305. | 5.7 | 655. |
| 19 | .710 | 305. | 5.7 | 654. |
| 20 | .670 | 288. | 6.0 | 652. |
| 21 | .660 | 284. | 5.7 | 651. |
| 22 | .670 | 288. | 6.0 | 655. |
| 23 | .670 | 288. | 6.0 | 650. |
| 24 | .710 | 305. | 5.7 | 647. |

DAY # 84

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .710 | 305. | 5.7 | 653. |
| 2 | .720 | 309. | 6.0 | 654. |
| 3 | .710 | 305. | 5.7 | 654. |
| 4 | .710 | 305. | 5.7 | 655. |
| 5 | .720 | 309. | 6.0 | 654. |
| 6 | .720 | 309. | 6.0 | 653. |
| 7 | .770 | 331. | 5.7 | 655. |
| 8 | .770 | 331. | 5.7 | 653. |
| 9 | .710 | 305. | 5.7 | 655. |
| 10 | .710 | 305. | 5.7 | 653. |
| 11 | .710 | 305. | 5.7 | 656. |
| 12 | .710 | 305. | 5.7 | 659. |
| 13 | .710 | 305. | 5.7 | 660. |
| 14 | .650 | 279. | 5.5 | 664. |
| 15 | .700 | 301. | 5.5 | 664. |
| 16 | .710 | 305. | 5.7 | 668. |
| 17 | .660 | 284. | 5.7 | 667. |
| 18 | .660 | 284. | 5.7 | 662. |
| 19 | .710 | 305. | 5.7 | 664. |
| 20 | .660 | 284. | 5.7 | 664. |
| 21 | .660 | 284. | 5.7 | 667. |
| 22 | .670 | 288. | 6.0 | 666. |
| 23 | .720 | 309. | 6.0 | 663. |
| 24 | .710 | 305. | 5.7 | 707. |

DAY # 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 658. |
| 2 | .680 | 292. | 6.3 | 656. |
| 3 | .680 | 292. | 6.3 | 652. |
| 4 | .680 | 292. | 6.3 | 656. |
| 5 | .690 | 296. | 6.5 | 657. |
| 6 | .690 | 296. | 6.5 | 654. |
| 7 | .690 | 296. | 6.5 | 651. |
| 8 | .740 | 318. | 6.3 | 655. |
| 9 | .810 | 348. | 6.5 | 655. |
| 10 | .750 | 322. | 6.5 | 656. |
| 11 | .690 | 296. | 6.5 | 652. |
| 12 | .680 | 292. | 6.3 | 653. |
| 13 | .680 | 292. | 6.3 | 654. |
| 14 | .680 | 292. | 6.3 | 654. |
| 15 | .680 | 292. | 6.3 | 655. |
| 16 | .680 | 292. | 6.3 | 655. |
| 17 | .690 | 296. | 6.5 | 656. |
| 18 | .690 | 296. | 6.5 | 655. |
| 19 | .690 | 296. | 6.5 | 655. |
| 20 | .690 | 296. | 6.5 | 653. |
| 21 | .690 | 296. | 6.5 | 655. |
| 22 | .680 | 292. | 6.3 | 656. |
| 23 | .740 | 318. | 6.3 | 655. |
| 24 | .680 | 292. | 6.3 | 680. |

DAY # 89

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 657. |
| 2 | .630 | 271. | 6.5 | 646. |
| 3 | .690 | 296. | 6.5 | 585. |
| 4 | .680 | 292. | 6.3 | 652. |
| 5 | .680 | 292. | 6.3 | 655. |
| 6 | .680 | 292. | 6.3 | 656. |
| 7 | .680 | 292. | 6.3 | 653. |
| 8 | .680 | 292. | 6.3 | 654. |
| 9 | .670 | 288. | 6.0 | 653. |
| 10 | .670 | 288. | 6.0 | 653. |
| 11 | .740 | 318. | 6.3 | 651. |
| 12 | .740 | 318. | 6.3 | 650. |
| 13 | .740 | 318. | 6.3 | 650. |
| 14 | .740 | 318. | 6.3 | 653. |
| 15 | .740 | 318. | 6.3 | 655. |
| 16 | .680 | 292. | 6.3 | 651. |
| 17 | .680 | 292. | 6.3 | 651. |
| 18 | .680 | 292. | 6.3 | 652. |
| 19 | .680 | 292. | 6.3 | 653. |
| 20 | .680 | 292. | 6.3 | 653. |
| 21 | .680 | 292. | 6.3 | 653. |
| 22 | .680 | 292. | 6.3 | 656. |
| 23 | .680 | 292. | 6.3 | 652. |
| 24 | .680 | 292. | 6.3 | 637. |

DAY = 90



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 655. |
| 2 | .680 | 292. | 6.3 | 654. |
| 3 | .740 | 318. | 6.3 | 654. |
| 4 | .670 | 288. | 6.0 | 654. |
| 5 | .690 | 296. | 6.5 | 655. |
| 6 | .690 | 296. | 6.5 | 655. |
| 7 | .690 | 296. | 6.5 | 654. |
| 8 | .690 | 296. | 6.5 | 653. |
| 9 | .690 | 296. | 6.5 | 652. |
| 10 | .690 | 296. | 6.5 | 655. |
| 11 | .690 | 296. | 6.5 | 652. |
| 12 | .690 | 296. | 6.5 | 650. |
| 13 | .690 | 296. | 6.5 | 644. |
| 14 | .680 | 292. | 6.3 | 642. |
| 15 | .680 | 292. | 6.3 | 637. |
| 16 | .680 | 292. | 6.3 | 628. |
| 17 | .680 | 292. | 6.3 | 631. |
| 18 | .680 | 292. | 6.3 | 637. |
| 19 | .680 | 292. | 6.3 | 639. |
| 20 | .680 | 292. | 6.3 | 639. |
| 21 | .680 | 292. | 6.3 | 640. |
| 22 | .690 | 296. | 6.5 | 639. |
| 23 | .680 | 292. | 6.3 | 641. |
| 24 | .680 | 292. | 6.3 | 638. |

DAY = 91

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .680 | 292. | 6.3 | 641. |
| 2 | .690 | 296. | 6.5 | 646. |
| 3 | .690 | 296. | 6.5 | 644. |
| 4 | .740 | 318. | 6.3 | 641. |
| 5 | .740 | 318. | 6.3 | 643. |
| 6 | .740 | 318. | 6.3 | 647. |
| 7 | .740 | 318. | 6.3 | 649. |
| 8 | .680 | 292. | 6.3 | 648. |
| 9 | .680 | 292. | 6.3 | 645. |
| 10 | .680 | 292. | 6.3 | 648. |
| 11 | .680 | 292. | 6.3 | 646. |
| 12 | .680 | 292. | 6.3 | 651. |
| 13 | .680 | 292. | 6.3 | 653. |
| 14 | .690 | 296. | 6.5 | 648. |
| 15 | .690 | 296. | 6.5 | 650. |
| 16 | .680 | 292. | 6.3 | 647. |
| 17 | .680 | 292. | 6.3 | 653. |
| 18 | .690 | 296. | 6.5 | 653. |
| 19 | .690 | 296. | 6.5 | 653. |
| 20 | .690 | 296. | 6.5 | 652. |
| 21 | .690 | 296. | 6.5 | 653. |
| 22 | .750 | 322. | 6.5 | 656. |
| 23 | .690 | 296. | 6.5 | 650. |
| 24 | .690 | 296. | 6.5 | 671. |

DAY # 92

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .690 | 296. | 6.5 | 656. |
| 2 | .690 | 296. | 6.5 | 657. |
| 3 | .690 | 296. | 6.5 | 656. |
| 4 | .690 | 296. | 6.5 | 652. |
| 5 | .690 | 296. | 6.5 | 654. |
| 6 | .690 | 296. | 6.5 | 655. |
| 7 | .690 | 296. | 6.5 | 653. |
| 8 | .690 | 296. | 6.5 | 658. |
| 9 | .750 | 322. | 6.5 | 656. |
| 10 | .690 | 296. | 6.5 | 655. |
| 11 | .680 | 292. | 6.3 | 652. |
| 12 | .680 | 292. | 6.3 | 656. |
| 13 | .680 | 292. | 6.3 | 651. |
| 14 | .680 | 292. | 6.3 | 652. |
| 15 | .680 | 292. | 6.3 | 650. |
| 16 | .680 | 292. | 6.3 | 648. |
| 17 | .680 | 292. | 6.3 | 646. |
| 18 | .680 | 292. | 6.3 | 652. |
| 19 | .680 | 292. | 6.3 | 644. |
| 20 | .680 | 292. | 6.3 | 645. |
| 21 | .680 | 292. | 6.3 | 651. |
| 22 | .680 | 292. | 6.3 | 651. |
| 23 | .680 | 292. | 6.3 | 651. |
| 24 | .680 | 292. | 6.3 | 642. |

APPENDIX J

LOUISVILLE GAS & ELECTRIC

MILL CREEK STATION - UNIT 3

Input Data

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

LOUISVILLE GAS AND ELEC. MILL CREEK UNIT 3

B+W BOILER DUAL REGISTER BURNERS

425 MWE GROSS LOW VOLATILE BITUMINOUS

PERFORMANCE NOX = 0.623 LB/10**6BTU, 248NG/J

NOX MONITOR REL. ACC. = 17.8PC, 12.4PC

DAY 1 = 1/19/81, DAY 34 = 3/24/81

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .528 | 227. | 10.7 | 198. |
| 2 | .535 | 230. | 11.2 | 198. |
| 3 | .540 | 232. | 11.1 | 196. |
| 4 | .561 | 241. | 11.4 | 196. |
| 5 | .566 | 243. | 11.4 | 196. |
| 6 | .578 | 248. | 11.5 | 195. |
| 7 | .562 | 241. | 9.7 | 196. |
| 8 | .588 | 252. | 6.7 | 195. |
| 9 | .702 | 302. | 7.2 | 193. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .553 | 238. | 5.2 | 200. |
| 14 | .558 | 240. | 4.9 | 197. |
| 15 | .504 | 217. | 5.1 | 197. |
| 16 | .526 | 226. | 5.6 | 199. |
| 17 | .462 | 198. | 5.9 | 202. |
| 18 | .470 | 202. | 5.9 | 203. |
| 19 | .476 | 204. | 5.4 | 202. |
| 20 | .480 | 206. | 4.9 | 200. |
| 21 | .472 | 203. | 5.1 | 204. |
| 22 | .458 | 197. | 5.2 | 203. |
| 23 | .477 | 205. | 5.7 | 202. |
| 24 | .424 | 183. | 8.8 | 199. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .471 | 203. | 5.0 | 282. |
| 2 | .460 | 201. | 4.9 | 283. |
| 3 | .471 | 202. | 4.9 | 283. |
| 4 | .474 | 204. | 4.9 | 283. |
| 5 | .498 | 214. | 4.7 | 325. |
| 6 | .506 | 217. | 4.6 | 347. |
| 7 | .543 | 233. | 4.9 | 399. |
| 8 | .590 | 253. | 3.1 | 423. |
| 9 | .630 | 271. | 3.8 | 414. |
| 10 | .576 | 247. | 5.0 | 399. |
| 11 | .586 | 252. | 5.0 | 399. |
| 12 | .550 | 236. | 4.8 | 415. |
| 13 | .571 | 245. | 4.7 | 387. |
| 14 | .472 | 203. | 3.9 | 388. |
| 15 | .533 | 229. | 5.1 | 312. |
| 16 | .457 | 196. | 5.2 | 278. |
| 17 | .436 | 187. | 5.3 | 281. |
| 18 | .410 | 176. | 5.1 | 281. |
| 19 | .433 | 186. | 6.1 | 269. |
| 20 | .405 | 174. | 5.6 | 271. |

| | | | | |
|---|---|---|---|---|
| 21 | .413 | 177. | 5.4 | 271. |
| 22 | .411 | 176. | 5.3 | 272. |
| 23 | .403 | 173. | 5.3 | 267. |
| 24 | .399 | 171. | 5.3 | 264. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 5.2 | 269. |
| 2 | .395 | 170. | 5.1 | 271. |
| 3 | .385 | 165. | 4.9 | 273. |
| 4 | .397 | 171. | 5.0 | 272. |
| 5 | .406 | 174. | 5.0 | 273. |
| 6 | .411 | 177. | 5.0 | 274. |
| 7 | .404 | 191. | 4.9 | 369. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | .378 | 162. | 8.8 | 236. |
| 10 | .480 | 210. | 5.0 | 400. |
| 11 | .518 | 223. | 3.7 | 384. |
| 12 | .504 | 217. | 5.0 | 387. |
| 13 | .543 | 233. | 4.4 | 397. |
| 14 | .513 | 220. | 4.3 | 400. |
| 15 | .519 | 223. | 4.8 | 317. |
| 16 | .439 | 189. | 5.3 | 275. |
| 17 | .419 | 180. | 5.1 | 276. |
| 18 | .433 | 188. | 5.0 | 333. |
| 19 | .463 | 201. | 4.9 | 337. |
| 20 | .455 | 195. | 5.1 | 289. |
| 21 | .433 | 189. | 5.0 | 270. |
| 22 | .441 | 189. | 5.9 | 218. |
| 23 | .413 | 180. | 6.8 | 187. |
| 24 | .363 | 159. | 7.5 | 182. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 7.2 | 183. |
| 2 | .363 | 156. | 7.2 | 183. |
| 3 | .351 | 151. | 7.3 | 167. |
| 4 | .343 | 147. | 7.3 | 172. |
| 5 | .359 | 152. | 7.1 | 183. |
| 6 | .368 | 156. | 7.0 | 200. |
| 7 | .380 | 163. | 6.7 | 212. |
| 8 | .385 | 166. | 6.6 | 209. |
| 9 | .375 | 161. | 6.5 | 208. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .410 | 176. | 6.6 | 251. |
| 12 | .317 | 136. | 5.5 | 256. |
| 13 | .329 | 139. | 5.3 | 262. |
| 14 | .321 | 138. | 5.3 | 257. |
| 15 | .320 | 137. | 5.3 | 256. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .444 | 191. | 6.4 | 259. |
| 18 | .437 | 188. | 6.4 | 258. |
| 19 | .433 | 186. | 6.3 | 260. |



Reproduced from best available copy.

| | | | | |
|---|---|---|---|---|
| 20 | .446 | 192. | 6.4 | 259. |
| 21 | .462 | 198. | 6.3 | 259. |
| 22 | .448 | 191. | 6.3 | 255. |
| 23 | .420 | 180. | 6.7 | 206. |
| 24 | .380 | 167. | 8.9 | 197. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .375 | 161. | 9.5 | 169. |
| 2 | .346 | 149. | 9.1 | 169. |
| 3 | .340 | 146. | 8.7 | 170. |
| 4 | .338 | 145. | 8.7 | 170. |
| 5 | .340 | 146. | 8.7 | 170. |
| 6 | .339 | 146. | 8.8 | 169. |
| 7 | .337 | 145. | 8.6 | 176. |
| 8 | .341 | 146. | 8.4 | 181. |
| 9 | .353 | 152. | 7.9 | 202. |
| 10 | .360 | 155. | 7.3 | 201. |
| 11 | .377 | 162. | 8.0 | 198. |
| 12 | .366 | 157. | 7.9 | 199. |
| 13 | .348 | 149. | 7.5 | 197. |
| 14 | .371 | 159. | 8.0 | 196. |
| 15 | .328 | 141. | 7.9 | 185. |
| 16 | .334 | 143. | 8.5 | 187. |
| 17 | .362 | 156. | 8.3 | 189. |
| 18 | .397 | 171. | 9.2 | 190. |
| 19 | .394 | 169. | 9.3 | 187. |
| 20 | .397 | 171. | 9.5 | 188. |
| 21 | .393 | 169. | 9.1 | 187. |
| 22 | .394 | 169. | 8.9 | 189. |
| 23 | .378 | 162. | 9.0 | 166. |
| 24 | .367 | 158. | 9.6 | 161. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .361 | 155. | 9.7 | 150. |
| 2 | .358 | 154. | 10.3 | 146. |
| 3 | .350 | 150. | 10.3 | 142. |
| 4 | .364 | 156. | 10.4 | 147. |
| 5 | .368 | 158. | 10.2 | 181. |
| 6 | .383 | 165. | 9.6 | 179. |
| 7 | .370 | 159. | 9.1 | 181. |
| 8 | .358 | 154. | 8.8 | 195. |
| 9 | .378 | 162. | 8.0 | 225. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .462 | 198. | 8.3 | 243. |
| 12 | .480 | 206. | 7.0 | 239. |
| 13 | .486 | 209. | 7.0 | 246. |
| 14 | .481 | 207. | 6.9 | 245. |
| 15 | .482 | 207. | 7.0 | 245. |
| 16 | .461 | 198. | 7.3 | 195. |
| 17 | .429 | 184. | 10.8 | 86. |
| 18 | .432 | 186. | 11.0 | 92. |

| | | | | |
|---|---|---|---|---|
| 19 | .454 | 195. | 11.7 | 93. |
| 20 | .454 | 195. | 11.8 | 93. |
| 21 | .447 | 192. | 11.8 | 94. |
| 22 | .437 | 188. | 12.0 | 92. |
| 23 | .440 | 189. | 11.9 | 93. |
| 24 | .449 | 193. | 12.2 | 92. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .453 | 195. | 12.5 | 96. |
| 2 | .442 | 190. | 11.9 | 96. |
| 3 | .448 | 192. | 11.7 | 99. |
| 4 | .458 | 197. | 11.7 | 102. |
| 5 | .464 | 199. | 11.8 | 101. |
| 6 | .464 | 199. | 11.8 | 99. |
| 7 | .470 | 202. | 11.8 | 102. |
| 8 | .475 | 204. | 11.9 | 100. |
| 9 | .473 | 203. | 11.9 | 100. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .458 | 197. | 11.6 | 100. |
| 12 | .450 | 193. | 11.6 | 99. |
| 13 | .447 | 192. | 11.6 | 88. |
| 14 | .436 | 187. | 11.4 | 97. |
| 15 | .448 | 192. | 11.6 | 96. |
| 16 | .449 | 193. | 11.6 | 102. |
| 17 | .451 | 194. | 11.6 | 100. |
| 18 | .452 | 194. | 11.6 | 101. |
| 19 | .452 | 194. | 11.6 | 101. |
| 20 | .455 | 195. | 11.7 | 102. |
| 21 | .458 | 197. | 11.7 | 102. |
| 22 | .458 | 197. | 11.7 | 103. |
| 23 | .460 | 198. | 11.8 | 101. |
| 24 | .469 | 201. | 11.9 | 102. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .474 | 204. | 11.9 | 104. |
| 2 | .481 | 207. | 11.9 | 104. |
| 3 | .486 | 209. | 11.8 | 106. |
| 4 | .488 | 210. | 11.8 | 105. |
| 5 | .481 | 207. | 11.9 | 106. |
| 6 | .477 | 205. | 11.8 | 104. |
| 7 | .478 | 205. | 11.8 | 105. |
| 8 | .473 | 203. | 12.0 | 104. |
| 9 | .437 | 188. | 11.3 | 104. |
| 10 | .470 | 202. | 12.0 | 104. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .473 | 203. | 11.9 | 103. |
| 13 | .472 | 203. | 11.9 | 101. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .462 | 198. | 12.1 | 99. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .481 | 207. | 11.6 | 101. |
| 21 | .487 | 209. | 11.7 | 102. |
| 22 | .482 | 207. | 11.6 | 102. |
| 23 | .479 | 206. | 11.7 | 98. |
| 24 | .476 | 204. | 11.6 | 98. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .478 | 204. | 11.5 | 101. |
| 2 | .480 | 206. | 11.4 | 106. |
| 3 | .479 | 206. | 11.4 | 103. |
| 4 | .479 | 206. | 11.4 | 102. |
| 5 | .478 | 206. | 11.4 | 102. |
| 6 | .478 | 204. | 11.3 | 104. |
| 7 | .478 | 205. | 11.2 | 103. |
| 8 | .480 | 206. | 11.3 | 104. |
| 9 | .475 | 204. | 11.4 | 101. |
| 10 | .477 | 204. | 10.7 | 102. |
| 11 | .467 | 201. | 11.0 | 102. |
| 12 | .474 | 204. | 10.9 | 100. |
| 13 | .475 | 204. | 10.9 | 101. |
| 14 | .474 | 204. | 10.9 | 101. |
| 15 | .471 | 202. | 10.8 | 101. |
| 16 | .466 | 200. | 10.8 | 104. |
| 17 | .463 | 198. | 10.8 | 103. |
| 18 | .462 | 198. | 10.7 | 105. |
| 19 | .465 | 200. | 10.7 | 105. |
| 20 | .468 | 201. | 10.7 | 104. |
| 21 | .463 | 199. | 10.7 | 105. |
| 22 | .464 | 198. | 10.7 | 105. |
| 23 | .457 | 197. | 10.7 | 103. |
| 24 | .457 | 196. | 10.7 | 100. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .461 | 198. | 10.9 | 100. |
| 2 | .461 | 198. | 10.9 | 99. |
| 3 | .461 | 198. | 10.9 | 100. |
| 4 | .461 | 198. | 10.9 | 98. |
| 5 | .435 | 187. | 10.8 | 98. |
| 6 | .436 | 187. | 10.9 | 99. |
| 7 | .437 | 188. | 10.8 | 98. |
| 8 | .436 | 187. | 10.8 | 99. |
| 9 | .435 | 188. | 10.8 | 100. |
| 10 | .461 | 198. | 10.8 | 100. |
| 11 | .463 | 199. | 10.9 | 101. |
| 12 | .463 | 199. | 11.2 | 100. |
| 13 | .471 | 204. | 11.1 | 98. |
| 14 | .480 | 206. | 11.2 | 97. |
| 15 | .481 | 208. | 11.2 | 98. |
| 16 | .485 | 208. | 11.1 | 99. |

| | | | | |
|---|---|---|---|---|
| 17 | .488 | 210. | 11.1 | 98. |
| 18 | .485 | 208. | 11.2 | 96. |
| 19 | .489 | 210. | 11.2 | 100. |
| 20 | .487 | 209. | 11.2 | 101. |
| 21 | .485 | 208. | 11.2 | 103. |
| 22 | .488 | 210. | 11.2 | 98. |
| 23 | .492 | 211. | 11.3 | 100. |
| 24 | .494 | 212. | 11.3 | 98. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .497 | 214. | 11.2 | 102. |
| 2 | .501 | 215. | 11.3 | 102. |
| 3 | .503 | 216. | 11.3 | 100. |
| 4 | .500 | 215. | 11.3 | 100. |
| 5 | .503 | 216. | 11.1 | 105. |
| 6 | .495 | 213. | 11.4 | 98. |
| 7 | .482 | 207. | 11.2 | 158. |
| 8 | .434 | 186. | 8.1 | 266. |
| 9 | .548 | 235. | 5.3 | 392. |
| 10 | .598 | 257. | 5.3 | 394. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .588 | 253. | 4.9 | 410. |
| 13 | .542 | 233. | 4.3 | 425. |
| 14 | .541 | 232. | 4.1 | 408. |
| 15 | .524 | 225. | 4.2 | 408. |
| 16 | .527 | 226. | 4.1 | 412. |
| 17 | .535 | 230. | 4.0 | 409. |
| 18 | .531 | 228. | 4.1 | 408. |
| 19 | .542 | 233. | 4.2 | 414. |
| 20 | .552 | 237. | 4.2 | 416. |
| 21 | .561 | 241. | 4.2 | 415. |
| 22 | .554 | 240. | 4.2 | 410. |
| 23 | .552 | 237. | 4.6 | 385. |
| 24 | .581 | 251. | 5.1 | 375. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .573 | 246. | 5.1 | 378. |
| 2 | .578 | 247. | 5.0 | 380. |
| 3 | .583 | 251. | 4.9 | 383. |
| 4 | .573 | 246. | 4.9 | 385. |
| 5 | .577 | 248. | 4.8 | 384. |
| 6 | .584 | 251. | 4.7 | 383. |
| 7 | .591 | 254. | 4.7 | 380. |
| 8 | .603 | 259. | 4.8 | 389. |
| 9 | .588 | 234. | 4.4 | 381. |
| 10 | .559 | 238. | 4.5 | 393. |
| 11 | .585 | 251. | 5.1 | 395. |
| 12 | .604 | 260. | 4.8 | 396. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 16 | .570 | 245. | 5.5 | 313. |
| 17 | .588 | 235. | 5.8 | 396. |
| 18 | .622 | 267. | 5.2 | 395. |
| 19 | .619 | 266. | 5.3 | 398. |
| 20 | .617 | 265. | 5.3 | 395. |
| 21 | .598 | 257. | 5.2 | 395. |
| 22 | .574 | 247. | 5.4 | 350. |
| 23 | .535 | 230. | 5.5 | 317. |
| 24 | .530 | 228. | 5.5 | 322. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .509 | 219. | 5.7 | 275. |
| 2 | .897 | 219. | 5.7 | 275. |
| 3 | -1.000 | -430. | -1.0 | -1. |
| 4 | -1.000 | -430. | -1.0 | -1. |
| 5 | .362 | 156. | 13.3 | 98. |
| 6 | .481 | 207. | 8.7 | 324. |
| 7 | .541 | 232. | 6.1 | 339. |
| 8 | .580 | 249. | 6.3 | 393. |
| 9 | .500 | 215. | 4.9 | 388. |
| 10 | .566 | 243. | 5.2 | 397. |
| 11 | .585 | 251. | 5.3 | 397. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .560 | 241. | 4.9 | 395. |
| 14 | .559 | 238. | 4.8 | 397. |
| 15 | .539 | 232. | 4.7 | 387. |
| 16 | .522 | 224. | 4.8 | 369. |
| 17 | .541 | 232. | 4.9 | 385. |
| 18 | .549 | 236. | 4.8 | 397. |
| 19 | .550 | 236. | 4.8 | 397. |
| 20 | .549 | 236. | 4.9 | 397. |
| 21 | .553 | 238. | 4.9 | 397. |
| 22 | .556 | 239. | 4.9 | 394. |
| 23 | .555 | 238. | 4.9 | 393. |
| 24 | .541 | 232. | 4.8 | 389. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .505 | 217. | 4.0 | 388. |
| 2 | .566 | 243. | 5.4 | 388. |
| 3 | .560 | 244. | 5.1 | 380. |
| 4 | .581 | 250. | 5.0 | 395. |
| 5 | .590 | 253. | 5.0 | 395. |
| 6 | .601 | 258. | 5.1 | 395. |
| 7 | .613 | 263. | 5.0 | 407. |
| 8 | .603 | 259. | 4.9 | 398. |
| 9 | .588 | 253. | 4.9 | 397. |
| 10 | .570 | 245. | 4.9 | 403. |
| 11 | .550 | 240. | 4.8 | 397. |
| 12 | .542 | 233. | 4.3 | 423. |
| 13 | .517 | 222. | 4.0 | 424. |
| 14 | .513 | 220. | 4.0 | 395. |

| | | | | |
|---|---|---|---|---|
| 15 | .502 | 216. | 4.1 | 400. |
| 16 | .500 | 219. | 4.2 | 398. |
| 17 | .484 | 209. | 4.1 | 397. |
| 18 | .492 | 211. | 4.1 | 399. |
| 19 | .508 | 218. | 4.1 | 399. |
| 20 | .507 | 218. | 4.1 | 396. |
| 21 | .500 | 215. | 4.1 | 391. |
| 22 | .497 | 214. | 4.2 | 394. |
| 23 | .495 | 213. | 4.1 | 391. |
| 24 | .526 | 226. | 4.9 | 377. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .459 | 198. | 9.9 | 110. |
| 2 | .467 | 201. | 9.6 | 108. |
| 3 | .475 | 204. | 8.9 | 108. |
| 4 | .466 | 200. | 8.8 | 105. |
| 5 | .457 | 196. | 8.7 | 162. |
| 6 | .458 | 195. | 7.6 | 248. |
| 7 | .478 | 205. | 5.5 | 268. |
| 8 | .522 | 224. | 6.5 | 269. |
| 9 | .485 | 208. | 4.7 | 353. |
| 10 | .499 | 214. | 3.5 | 377. |
| 11 | .475 | 204. | 4.2 | 378. |
| 12 | .533 | 229. | 4.0 | 376. |
| 13 | .543 | 233. | 4.1 | 379. |
| 14 | .529 | 227. | 4.0 | 379. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .492 | 211. | 3.8 | 347. |
| 17 | .490 | 210. | 3.8 | 344. |
| 18 | .504 | 217. | 3.9 | 346. |
| 19 | .514 | 221. | 3.9 | 357. |
| 20 | .516 | 222. | 4.1 | 356. |
| 21 | .526 | 226. | 4.1 | 329. |
| 22 | .468 | 206. | 4.6 | 289. |
| 23 | .478 | 206. | 4.6 | 292. |
| 24 | .465 | 200. | 4.9 | 269. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .488 | 210. | 5.9 | 217. |
| 2 | .493 | 212. | 6.8 | 214. |
| 3 | .478 | 205. | 6.5 | 197. |
| 4 | .470 | 202. | 6.5 | 197. |
| 5 | .472 | 203. | 6.3 | 211. |
| 6 | .491 | 211. | 6.0 | 238. |
| 7 | .495 | 213. | 5.8 | 246. |
| 8 | .481 | 207. | 5.5 | 297. |
| 9 | .459 | 197. | 4.8 | 290. |
| 10 | .448 | 191. | 4.8 | 303. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .438 | 188. | 4.8 | 295. |
| 13 | .426 | 183. | 4.6 | 300. |



Reproduced from best available copy.

| | | | | |
|---|---|---|---|---|
| 14 | .455 | 195. | 3.9 | 372. |
| 15 | .460 | 198. | 3.8 | 361. |
| 16 | .477 | 205. | 3.7 | 397. |
| 17 | .467 | 201. | 3.9 | 395. |
| 18 | .483 | 207. | 3.9 | 397. |
| 19 | .498 | 212. | 4.0 | 396. |
| 20 | .491 | 211. | 4.0 | 379. |
| 21 | .491 | 211. | 4.3 | 302. |
| 22 | .419 | 180. | 5.2 | 260. |
| 23 | .418 | 178. | 5.2 | 260. |
| 24 | .423 | 182. | 5.0 | 272. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .469 | 201. | 5.9 | 219. |
| 2 | .488 | 208. | 6.8 | 210. |
| 3 | .490 | 210. | 6.9 | 215. |
| 4 | .495 | 213. | 6.7 | 234. |
| 5 | .506 | 217. | 6.6 | 238. |
| 6 | .515 | 221. | 6.6 | 266. |
| 7 | .508 | 217. | 5.9 | 294. |
| 8 | .522 | 224. | 4.0 | 394. |
| 9 | .561 | 241. | 3.9 | 403. |
| 10 | .551 | 237. | 3.8 | 413. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .491 | 211. | 3.3 | 410. |
| 13 | .500 | 215. | 3.2 | 412. |
| 14 | .512 | 220. | 3.3 | 416. |
| 15 | .535 | 230. | 4.0 | 395. |
| 16 | .561 | 241. | 4.5 | 394. |
| 17 | .578 | 247. | 4.5 | 396. |
| 18 | .560 | 240. | 4.6 | 402. |
| 19 | .577 | 248. | 4.4 | 391. |
| 20 | .569 | 244. | 4.8 | 391. |
| 21 | .572 | 246. | 4.8 | 392. |
| 22 | .569 | 244. | 4.7 | 394. |
| 23 | .552 | 237. | 4.7 | 355. |
| 24 | .546 | 235. | 4.8 | 380. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .556 | 239. | 4.8 | 377. |
| 2 | .556 | 239. | 4.8 | 343. |
| 3 | .552 | 237. | 5.0 | 355. |
| 4 | .553 | 238. | 5.0 | 358. |
| 5 | .553 | 238. | 4.9 | 361. |
| 6 | .550 | 236. | 4.6 | 375. |
| 7 | .555 | 238. | 4.3 | 394. |
| 8 | .551 | 237. | 4.2 | 399. |
| 9 | .555 | 238. | 4.2 | 400. |
| 10 | .555 | 238. | 4.1 | 395. |
| 11 | .543 | 233. | 4.1 | 370. |
| 12 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 13 | .537 | 231. | 3.8 | 396. |
| 14 | .551 | 237. | 3.7 | 403. |
| 15 | .537 | 231. | 3.6 | 402. |
| 16 | .520 | 223. | 3.6 | 400. |
| 17 | .517 | 222. | 3.7 | 400. |
| 18 | .530 | 228. | 3.7 | 409. |
| 19 | .544 | 234. | 3.8 | 408. |
| 20 | .541 | 232. | 4.0 | 401. |
| 21 | .526 | 226. | 4.1 | 401. |
| 22 | .529 | 227. | 4.1 | 400. |
| 23 | .528 | 227. | 4.4 | 394. |
| 24 | .508 | 218. | 5.3 | 280. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 5.7 | 261. |
| 2 | .413 | 177. | 5.8 | 266. |
| 3 | .420 | 180. | 5.9 | 262. |
| 4 | .459 | 197. | 5.4 | 323. |
| 5 | .459 | 197. | 5.2 | 348. |
| 6 | .497 | 214. | 5.0 | 367. |
| 7 | .492 | 211. | 5.0 | 390. |
| 8 | .552 | 237. | 5.1 | 393. |
| 9 | .545 | 234. | 5.0 | 396. |
| 10 | .551 | 237. | 5.4 | 384. |
| 11 | .594 | 255. | 5.3 | 389. |
| 12 | .573 | 246. | 5.5 | 388. |
| 13 | .540 | 232. | 5.5 | 346. |
| 14 | .562 | 241. | 5.7 | 329. |
| 15 | .557 | 239. | 6.1 | 266. |
| 16 | .506 | 217. | 6.4 | 263. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .433 | 186. | 5.9 | 267. |
| 22 | .481 | 207. | 5.3 | 265. |
| 23 | .481 | 207. | 5.8 | 247. |
| 24 | .433 | 186. | 5.9 | 255. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .504 | 217. | 7.4 | 210. |
| 2 | .483 | 209. | 8.0 | 206. |
| 3 | .472 | 203. | 8.0 | 203. |
| 4 | .478 | 205. | 7.8 | 202. |
| 5 | .434 | 186. | 7.8 | 204. |
| 6 | .481 | 207. | 7.9 | 202. |
| 7 | .517 | 222. | 7.9 | 265. |
| 8 | .530 | 228. | 5.4 | 343. |
| 9 | .591 | 254. | 5.5 | 396. |
| 10 | .605 | 260. | 5.4 | 395. |
| 11 | .513 | 220. | 5.4 | 389. |

| | | | | |
|---|---|---|---|---|
| 12 | .562 | 242. | 5.4 | 391. |
| 13 | .553 | 238. | 5.5 | 387. |
| 14 | .526 | 226. | 5.5 | 292. |
| 15 | .495 | 213. | 6.4 | 209. |
| 16 | .510 | 223. | 8.1 | 195. |
| 17 | .486 | 209. | 7.5 | 198. |
| 18 | .469 | 201. | 7.5 | 201. |
| 19 | .459 | 197. | 7.7 | 201. |
| 20 | .424 | 182. | 7.5 | 202. |
| 21 | .431 | 185. | 7.7 | 201. |
| 22 | .434 | 186. | 7.7 | 203. |
| 23 | .431 | 185. | 7.8 | 190. |
| 24 | .455 | 195. | 9.8 | 170. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .477 | 205. | 10.3 | 162. |
| 2 | .488 | 210. | 10.4 | 153. |
| 3 | .490 | 210. | 10.5 | 153. |
| 4 | .495 | 213. | 10.4 | 153. |
| 5 | .498 | 214. | 10.6 | 153. |
| 6 | .498 | 214. | 10.6 | 170. |
| 7 | .527 | 226. | 9.9 | 196. |
| 8 | .538 | 229. | 9.9 | 195. |
| 9 | .556 | 239. | 8.9 | 267. |
| 10 | .517 | 222. | 6.2 | 302. |
| 11 | .483 | 207. | 5.1 | 307. |
| 12 | .477 | 205. | 4.3 | 253. |
| 13 | .495 | 213. | 6.3 | 193. |
| 14 | .481 | 207. | 7.2 | 194. |
| 15 | .488 | 210. | 7.4 | 193. |
| 16 | .478 | 205. | 7.2 | 197. |
| 17 | .477 | 205. | 7.2 | 198. |
| 18 | .483 | 207. | 7.2 | 202. |
| 19 | .491 | 211. | 7.2 | 201. |
| 20 | .488 | 210. | 7.2 | 200. |
| 21 | .483 | 207. | 7.1 | 198. |
| 22 | .478 | 205. | 7.2 | 199. |
| 23 | .480 | 208. | 7.3 | 194. |
| 24 | .464 | 199. | 7.5 | 156. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .463 | 199. | 9.9 | 154. |
| 2 | .488 | 210. | 10.2 | 156. |
| 3 | .488 | 210. | 10.2 | 155. |
| 4 | .490 | 212. | 10.4 | 155. |
| 5 | .497 | 214. | 10.5 | 175. |
| 6 | .500 | 215. | 10.2 | 205. |
| 7 | .520 | 227. | 9.9 | 207. |
| 8 | .523 | 225. | 9.5 | 206. |
| 9 | .555 | 238. | 9.5 | 259. |
| 10 | .543 | 233. | 7.0 | 301. |

| | | | | |
|---|---|---|---|---|
| 11 | .499 | 214. | 5.7 | 304. |
| 12 | .528 | 225. | 5.5 | 393. |
| 13 | .574 | 247. | 5.4 | 398. |
| 14 | .569 | 244. | 5.7 | 387. |
| 15 | .573 | 246. | 5.6 | 382. |
| 16 | .540 | 232. | 5.5 | 337. |
| 17 | .483 | 207. | 5.5 | 269. |
| 18 | .484 | 208. | 5.1 | 341. |
| 19 | .513 | 220. | 5.0 | 360. |
| 20 | .510 | 219. | 5.0 | 346. |
| 21 | .479 | 206. | 5.1 | 272. |
| 22 | .442 | 190. | 5.2 | 268. |
| 23 | .455 | 195. | 5.7 | 257. |
| 24 | .474 | 204. | 8.2 | 169. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .459 | 197. | 9.2 | 167. |
| 2 | .458 | 197. | 9.3 | 166. |
| 3 | .458 | 197. | 9.3 | 170. |
| 4 | .459 | 197. | 9.2 | 170. |
| 5 | .469 | 201. | 8.9 | 197. |
| 6 | .474 | 204. | 8.7 | 201. |
| 7 | .483 | 207. | 6.6 | 200. |
| 8 | .463 | 199. | 4.4 | 409. |
| 9 | .544 | 234. | 5.0 | 407. |
| 10 | .521 | 223. | 4.2 | 411. |
| 11 | .530 | 228. | 4.3 | 406. |
| 12 | .516 | 222. | 4.4 | 302. |
| 13 | .463 | 199. | 4.9 | 305. |
| 14 | .443 | 191. | 5.2 | 266. |
| 15 | .445 | 191. | 5.3 | 269. |
| 16 | .454 | 196. | 5.4 | 269. |
| 17 | .460 | 198. | 5.4 | 269. |
| 18 | .465 | 200. | 5.4 | 270. |
| 19 | .467 | 201. | 5.5 | 271. |
| 20 | .464 | 200. | 5.4 | 273. |
| 21 | .473 | 203. | 5.4 | 273. |
| 22 | .471 | 202. | 5.4 | 272. |
| 23 | .473 | 203. | 5.6 | 217. |
| 24 | .477 | 205. | 7.4 | 204. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .474 | 204. | 8.7 | 164. |
| 2 | .460 | 198. | 9.6 | 159. |
| 3 | .454 | 196. | 9.6 | 159. |
| 4 | .448 | 192. | 9.5 | 161. |
| 5 | .450 | 193. | 9.5 | 161. |
| 6 | .453 | 195. | 9.1 | 196. |
| 7 | .462 | 198. | 8.7 | 198. |
| 8 | .450 | 193. | 7.0 | 240. |
| 9 | .451 | 194. | 6.3 | 249. |

| | | | | |
|---|---|---|---|---|
| 10 | .485 | 208. | 6.3 | 249. |
| 11 | .465 | 200. | 6.3 | 250. |
| 12 | .460 | 199. | 6.4 | 249. |
| 13 | .460 | 198. | 6.3 | 250. |
| 14 | .459 | 195. | 6.6 | 206. |
| 15 | .441 | 189. | 6.8 | 231. |
| 16 | .451 | 194. | 6.9 | 229. |
| 17 | .451 | 194. | 6.8 | 241. |
| 18 | .477 | 205. | 6.0 | 336. |
| 19 | .537 | 231. | 5.8 | 365. |
| 20 | .585 | 238. | 5.7 | 347. |
| 21 | .533 | 229. | 5.9 | 328. |
| 22 | .494 | 212. | 5.8 | 280. |
| 23 | .456 | 196. | 6.0 | 248. |
| 24 | .442 | 190. | 6.0 | 210. |

DAY = 33

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .467 | 201. | 7.1 | 196. |
| 4 | .466 | 200. | 7.1 | 194. |
| 5 | .472 | 203. | 7.3 | 195. |
| 6 | .486 | 209. | 7.1 | 249. |
| 7 | .477 | 205. | 5.6 | 337. |
| 8 | .520 | 223. | 4.8 | 347. |
| 9 | .478 | 204. | 4.9 | 384. |
| 10 | .551 | 237. | 5.8 | 399. |
| 11 | .560 | 241. | 6.0 | 401. |
| 12 | .552 | 237. | 4.9 | 396. |
| 13 | .520 | 223. | 4.8 | 393. |
| 14 | .530 | 232. | 6.8 | 392. |
| 15 | .558 | 240. | 6.2 | 389. |
| 16 | .586 | 252. | 5.7 | 386. |
| 17 | .531 | 228. | 5.6 | 387. |
| 18 | .577 | 248. | 5.5 | 392. |
| 19 | .509 | 219. | 6.3 | 178. |
| 20 | .447 | 192. | 8.0 | 195. |
| 21 | .435 | 187. | 7.8 | 173. |
| 22 | .401 | 172. | 9.5 | 169. |
| 23 | .365 | 157. | 9.1 | 170. |
| 24 | .365 | 157. | 9.0 | 170. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .456 | 195. | 8.5 | 263. |
| 2 | .467 | 201. | 8.8 | 266. |
| 3 | .474 | 204. | 8.8 | 268. |
| 4 | .474 | 204. | 8.7 | 265. |
| 5 | .477 | 205. | 8.8 | 261. |
| 6 | .485 | 208. | 5.2 | 332. |
| 7 | .500 | 215. | 5.5 | 308. |
| 8 | .482 | 207. | 8.7 | 339. |

| | | | | |
|---|---|---|---|---|
| 9 | .496 | 213. | 4.4 | 347. |
| 10 | .512 | 220. | 4.8 | 390. |
| 11 | .466 | 199. | 5.1 | 332. |
| 12 | .458 | 197. | 5.7 | 299. |
| 13 | .493 | 212. | 5.7 | 334. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .445 | 191. | 5.8 | 267. |
| 16 | .474 | 202. | 6.0 | 257. |
| 17 | .468 | 201. | 5.9 | 251. |
| 18 | .465 | 200. | 5.8 | 251. |
| 19 | .466 | 200. | 5.9 | 260. |
| 20 | .498 | 212. | 5.5 | 295. |
| 21 | .509 | 219. | 5.6 | 285. |
| 22 | .488 | 210. | 5.8 | 251. |
| 23 | .483 | 207. | 5.7 | 306. |
| 24 | .510 | 219. | 5.3 | 291. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .485 | 208. | 6.3 | 228. |
| 2 | .486 | 208. | 7.0 | 209. |
| 3 | .445 | 191. | 7.4 | 209. |
| 4 | .421 | 181. | 7.1 | 228. |
| 5 | .428 | 184. | 7.0 | 253. |
| 6 | .422 | 181. | 6.5 | 311. |
| 7 | .482 | 208. | 5.0 | 385. |
| 8 | .556 | 239. | 5.0 | 389. |
| 9 | .551 | 237. | 4.7 | 392. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .567 | 244. | 5.1 | 370. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .560 | 241. | 5.5 | 340. |
| 14 | .507 | 218. | 5.4 | 337. |
| 15 | .487 | 209. | 5.2 | 291. |
| 16 | .472 | 203. | 5.3 | 282. |
| 17 | .464 | 199. | 5.2 | 280. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | .467 | 201. | 5.7 | 285. |
| 20 | .474 | 204. | 5.7 | 282. |
| 21 | .488 | 210. | 5.7 | 295. |
| 22 | .516 | 222. | 5.7 | 326. |
| 23 | .509 | 219. | 5.8 | 255. |
| 24 | .466 | 200. | 6.7 | 192. |

DAY = 36

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .477 | 205. | 7.7 | 154. |
| 2 | .469 | 201. | 9.5 | 156. |
| 3 | .477 | 205. | 9.0 | 186. |
| 4 | .477 | 205. | 7.5 | 203. |
| 5 | .473 | 203. | 7.3 | 213. |
| 6 | .475 | 204. | 6.4 | 246. |
| 7 | .488 | 210. | 5.1 | 320. |

| | | | | |
|---|---|---|---|---|
| 8 | .562 | 241. | 4.5 | 388. |
| 9 | .605 | 260. | 4.6 | 399. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .604 | 259. | 5.0 | 388. |
| 12 | .571 | 247. | 4.9 | 387. |
| 13 | .572 | 246. | 5.0 | 357. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .534 | 229. | 5.8 | 290. |
| 19 | .541 | 232. | 5.8 | 298. |
| 20 | .572 | 246. | 5.5 | 340. |
| 21 | .597 | 256. | 5.4 | 379. |
| 22 | .616 | 265. | 5.4 | 346. |
| 23 | .562 | 241. | 5.9 | 269. |
| 24 | .503 | 216. | 6.9 | 180. |

DAY = 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .464 | 199. | 8.3 | 150. |
| 2 | .437 | 188. | 10.2 | 145. |
| 3 | .417 | 179. | 10.4 | 146. |
| 4 | .414 | 178. | 10.4 | 148. |
| 5 | .397 | 171. | 10.3 | 147. |
| 6 | .390 | 168. | 10.4 | 145. |
| 7 | .387 | 166. | 10.2 | 174. |
| 8 | .397 | 171. | 8.6 | 185. |
| 9 | .443 | 190. | 8.0 | 255. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .531 | 228. | 5.4 | 273. |
| 12 | .531 | 229. | 5.5 | 261. |
| 13 | .530 | 228. | 5.7 | 261. |
| 14 | .509 | 219. | 5.5 | 259. |
| 15 | .497 | 214. | 5.5 | 259. |
| 16 | .645 | 277. | 7.4 | 227. |
| 17 | .695 | 299. | 7.7 | 211. |
| 18 | .623 | 268. | 8.0 | 196. |
| 19 | .591 | 254. | 7.9 | 197. |
| 20 | .534 | 230. | 8.9 | 157. |
| 21 | .497 | 214. | 8.9 | 157. |
| 22 | -1.000 | -430. | -1.0 | -1. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 40

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 9.0 | 178. |
| 2 | .459 | 197. | 9.1 | 159. |
| 3 | .448 | 192. | 9.6 | 162. |
| 4 | .433 | 186. | 9.4 | 161. |
| 5 | .401 | 172. | 9.4 | 171. |
| 6 | .401 | 172. | 9.3 | 176. |

| | | | | |
|---|---|---|---|---|
| 7 | .410 | 176. | 9.0 | 227. |
| 8 | .515 | 221. | 7.6 | 263. |
| 9 | .493 | 212. | 5.3 | 386. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .545 | 234. | 3.8 | 391. |
| 12 | .553 | 238. | 3.9 | 387. |
| 13 | .555 | 238. | 3.9 | 391. |
| 14 | .567 | 244. | 4.1 | 394. |
| 15 | .560 | 241. | 4.0 | 392. |
| 16 | .548 | 235. | 4.0 | 377. |
| 17 | .540 | 232. | 4.0 | 370. |
| 18 | .541 | 232. | 4.1 | 354. |
| 19 | .542 | 233. | 4.4 | 358. |
| 20 | .584 | 251. | 4.5 | 394. |
| 21 | .575 | 247. | 4.4 | 388. |
| 22 | .549 | 236. | 4.4 | 336. |
| 23 | .495 | 213. | 4.7 | 268. |
| 24 | .488 | 210. | 6.0 | 226. |

DAY = 41

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .480 | 208. | 6.6 | 217. |
| 2 | .483 | 207. | 8.0 | 177. |
| 3 | .470 | 202. | 8.6 | 175. |
| 4 | .465 | 200. | 8.5 | 174. |
| 5 | .460 | 198. | 8.4 | 175. |
| 6 | .463 | 199. | 7.9 | 237. |
| 7 | .487 | 209. | 5.2 | 322. |
| 8 | .502 | 216. | 3.8 | 391. |
| 9 | .523 | 225. | 3.5 | 391. |
| 10 | .528 | 227. | 3.5 | 391. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .527 | 226. | 4.0 | 361. |
| 13 | .490 | 210. | 4.1 | 360. |
| 14 | .520 | 223. | 4.0 | 388. |
| 15 | .536 | 230. | 4.0 | 388. |
| 16 | .546 | 236. | 4.1 | 391. |
| 17 | .547 | 235. | 4.3 | 377. |
| 18 | .531 | 231. | 4.5 | 366. |
| 19 | .530 | 232. | 4.6 | 357. |
| 20 | .561 | 241. | 4.5 | 391. |
| 21 | .582 | 250. | 4.5 | 392. |
| 22 | .546 | 236. | 4.6 | 339. |
| 23 | .495 | 213. | 4.7 | 286. |
| 24 | .473 | 203. | 4.9 | 269. |

DAY = 42

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .461 | 198. | 6.5 | 197. |
| 2 | .443 | 190. | 7.3 | 194. |
| 3 | .397 | 171. | 7.5 | 200. |
| 4 | .403 | 173. | 7.5 | 202. |
| 5 | .417 | 179. | 7.4 | 202. |

| | | | | |
|---|---|---|---|---|
| 6 | .347 | 171. | 7.4 | 204. |
| 7 | .42[illegible] | 180. | 7.2 | 271. |
| 8 | .49[illegible] | 213. | 6.4 | 364. |
| 9 | .58[illegible] | 250. | 6.3 | 390. |
| 10 | .58[illegible] | 253. | 6.5 | 393. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .53[illegible] | 228. | 5.2 | 391. |
| 13 | .53[illegible] | 231. | 5.1 | 392. |
| 14 | .53[illegible] | 229. | 5.1 | 390. |
| 15 | .52[illegible] | 224. | 6.0 | 393. |
| 16 | .56[illegible] | 242. | 6.4 | 375. |
| 17 | .55[illegible] | 238. | 6.4 | 371. |
| 18 | .54[illegible] | 235. | 6.5 | 380. |
| 19 | .55[illegible] | 237. | 6.8 | 378. |
| 20 | .57[illegible] | 246. | 6.4 | 395. |
| 21 | .57[illegible] | 246. | 6.3 | 393. |
| 22 | .58[illegible] | 235. | 6.3 | 387. |
| 23 | .497 | 214. | 6.5 | 286. |
| 24 | .48[illegible] | 206. | 5.5 | 223. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .48[illegible] | 208. | 8.1 | 198. |
| 2 | .48[illegible] | 207. | 8.7 | 193. |
| 3 | .48[illegible] | 207. | 8.6 | 192. |
| 4 | .48[illegible] | 207. | 8.6 | 190. |
| 5 | .48[illegible] | 206. | 8.6 | 191. |
| 6 | .48[illegible] | 207. | 6.7 | 295. |
| 7 | .47[illegible] | 203. | 6.5 | 326. |
| 8 | .53[illegible] | 229. | 6.4 | 380. |
| 9 | .56[illegible] | 240. | 6.4 | 389. |
| 10 | .60[illegible] | 258. | 6.9 | 369. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .45[illegible] | 197. | 8.0 | 330. |
| 13 | .49[illegible] | 213. | 6.2 | 343. |
| 14 | .53[illegible] | 228. | 5.2 | 388. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .55[illegible] | 240. | 6.1 | 390. |
| 18 | .55[illegible] | 238. | 6.2 | 391. |
| 19 | .53[illegible] | 231. | 6.3 | 383. |
| 20 | .54[illegible] | 235. | 6.1 | 393. |
| 21 | .55[illegible] | 237. | 6.1 | 388. |
| 22 | .55[illegible] | 238. | 6.2 | 357. |
| 23 | .51[illegible] | 219. | 6.8 | 272. |
| 24 | .49[illegible] | 211. | 7.2 | 169. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .49[illegible] | 210. | 9.3 | 175. |
| 2 | .48[illegible] | 209. | 9.3 | 175. |
| 3 | .48[illegible] | 209. | 9.2 | 174. |
| 4 | .48[illegible] | 208. | 9.2 | 173. |

| | | | | |
|---|---|---|---|---|
| 5 | .484 | 208. | 9.3 | 173. |
| 6 | .481 | 207. | 9.2 | 173. |
| 7 | .485 | 208. | 9.3 | 174. |
| 8 | .477 | 205. | 8.2 | 215. |
| 9 | .486 | 209. | 7.8 | 238. |
| 10 | .503 | 216. | 6.5 | 248. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .523 | 225. | 6.7 | 246. |
| 13 | .526 | 226. | 6.8 | 246. |
| 14 | .523 | 225. | 6.7 | 246. |
| 15 | .514 | 221. | 6.9 | 176. |
| 16 | .475 | 204. | 9.0 | 175. |
| 17 | .463 | 199. | 8.9 | 174. |
| 18 | .462 | 198. | 8.9 | 174. |
| 19 | .462 | 198. | 8.8 | 175. |
| 20 | .462 | 198. | 8.8 | 176. |
| 21 | .438 | 188. | 9.5 | 113. |
| 22 | .391 | 168. | 10.7 | 106. |
| 23 | .415 | 178. | 11.2 | 103. |
| 24 | .412 | 177. | 11.2 | 99. |

DAY = 45

| HOUR | NOX LB/10**8 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .416 | 179. | 11.4 | 99. |
| 2 | .422 | 181. | 11.4 | 100. |
| 3 | .426 | 183. | 11.3 | 100. |
| 4 | .425 | 183. | 11.4 | 100. |
| 5 | .427 | 183. | 11.4 | 101. |
| 6 | .427 | 183. | 11.5 | 98. |
| 7 | .429 | 184. | 11.4 | 101. |
| 8 | .432 | 186. | 11.5 | 102. |
| 9 | .432 | 186. | 11.5 | 102. |
| 10 | .430 | 186. | 11.5 | 102. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .460 | 198. | 12.0 | 102. |
| 13 | .451 | 195. | 11.8 | 103. |
| 14 | .458 | 195. | 11.8 | 99. |
| 15 | .448 | 191. | 11.9 | 98. |
| 16 | .447 | 192. | 11.8 | 97. |
| 17 | .448 | 192. | 11.8 | 99. |
| 18 | .442 | 190. | 11.9 | 97. |
| 19 | .438 | 188. | 11.9 | 102. |
| 20 | .441 | 189. | 11.9 | 99. |
| 21 | .443 | 190. | 12.1 | 101. |
| 22 | .443 | 190. | 12.1 | 98. |
| 23 | .439 | 189. | 12.2 | 96. |
| 24 | .448 | 192. | 12.2 | 96. |

DAY = 46

| HOUR | NOX LB/10**8 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .449 | 193. | 12.2 | 101. |
| 2 | .453 | 195. | 12.1 | 98. |
| 3 | .458 | 195. | 12.2 | 99. |

| | | | | |
|---|---|---|---|---|
| 4 | .452 | 194. | 12.1 | 100. |
| 5 | .451 | 194. | 12.1 | 99. |
| 6 | .453 | 195. | 12.1 | 99. |
| 7 | .458 | 197. | 12.2 | 100. |
| 8 | .463 | 199. | 12.1 | 101. |
| 9 | .463 | 199. | 12.0 | 101. |
| 10 | .466 | 200. | 12.1 | 101. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .458 | 192. | 12.1 | 99. |
| 13 | .442 | 190. | 11.9 | 99. |
| 14 | .438 | 188. | 12.0 | 98. |
| 15 | .437 | 188. | 11.9 | 99. |
| 16 | .440 | 189. | 11.9 | 99. |
| 17 | .440 | 189. | 11.9 | 99. |
| 18 | .441 | 189. | 11.9 | 99. |
| 19 | .442 | 190. | 11.9 | 103. |
| 20 | .438 | 188. | 12.0 | 101. |
| 21 | .444 | 191. | 11.9 | 101. |
| 22 | .445 | 191. | 12.0 | 100. |
| 23 | .442 | 190. | 11.9 | 99. |
| 24 | .443 | 190. | 12.0 | 99. |

DAY = 47

| HOUR | NOX LB/10***6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .447 | 192. | 11.9 | 101. |
| 2 | .448 | 192. | 11.9 | 100. |
| 3 | .445 | 191. | 11.9 | 102. |
| 4 | .446 | 192. | 11.9 | 100. |
| 5 | .446 | 192. | 12.0 | 97. |
| 6 | .444 | 192. | 11.7 | 143. |
| 7 | .474 | 204. | 9.9 | 225. |
| 8 | .552 | 237. | 6.8 | 340. |
| 9 | .616 | 265. | 5.4 | 388. |
| 10 | .610 | 262. | 5.2 | 391. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .587 | 252. | 4.7 | 358. |
| 13 | .519 | 223. | 4.7 | 315. |
| 14 | .490 | 210. | 5.8 | 221. |
| 15 | .504 | 217. | 7.4 | 250. |
| 16 | .512 | 220. | 6.4 | 248. |
| 17 | .514 | 221. | 6.5 | 247. |
| 18 | .513 | 220. | 6.4 | 247. |
| 19 | .518 | 223. | 6.4 | 249. |
| 20 | .522 | 224. | 6.3 | 250. |
| 21 | .521 | 224. | 6.3 | 248. |
| 22 | .516 | 222. | 6.3 | 248. |
| 23 | .512 | 220. | 6.3 | 200. |
| 24 | .472 | 203. | 6.7 | 197. |

DAY = 48

| HOUR | NOX LB/10***6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .473 | 203. | 6.6 | 201. |
| 2 | .485 | 207. | 6.5 | 238. |

| | | | | |
|---|---|---|---|---|
| 7 | .467 | 201. | 6.5 | 196. |
| 8 | .458 | 195. | 6.7 | 194. |
| 9 | .456 | 196. | 6.7 | 194. |
| 10 | .457 | 196. | 6.6 | 238. |
| 11 | .495 | 213. | 6.0 | 250. |
| 12 | .511 | 220. | 6.0 | 278. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | .320 | 137. | 10.5 | 193. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .506 | 217. | 5.2 | 306. |
| 17 | .520 | 223. | 5.3 | 310. |
| 18 | .521 | 224. | 5.3 | 314. |
| 19 | .520 | 223. | 5.2 | 312. |
| 20 | .519 | 223. | 5.3 | 285. |
| 21 | .498 | 212. | 5.3 | 283. |
| 22 | .498 | 214. | 5.2 | 288. |
| 23 | .500 | 215. | 5.3 | 282. |
| 24 | .499 | 214. | 5.4 | 287. |

DAY = 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .504 | 215. | 8.7 | 197. |
| 2 | .499 | 214. | 8.7 | 198. |
| 3 | .497 | 214. | 8.6 | 199. |
| 4 | .494 | 211. | 8.5 | 199. |
| 5 | .494 | 211. | 8.5 | 199. |
| 6 | .490 | 210. | 8.5 | 197. |
| 7 | .488 | 210. | 8.5 | 199. |
| 8 | .488 | 210. | 8.5 | 194. |
| 9 | .496 | 213. | 6.3 | 282. |
| 10 | .469 | 201. | 4.0 | 286. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .473 | 203. | 5.3 | 283. |
| 13 | .470 | 202. | 5.1 | 236. |
| 14 | .469 | 201. | 5.1 | 286. |
| 15 | .467 | 201. | 5.1 | 287. |
| 16 | .466 | 200. | 5.1 | 277. |
| 17 | .467 | 201. | 5.1 | 277. |
| 18 | .462 | 198. | 5.2 | 278. |
| 19 | .467 | 201. | 5.1 | 275. |
| 20 | .482 | 207. | 5.1 | 322. |
| 21 | .530 | 228. | 4.6 | 380. |
| 22 | .508 | 218. | 4.8 | 318. |
| 23 | .468 | 201. | 5.1 | 262. |
| 24 | .456 | 196. | 5.5 | 249. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .498 | 214. | 7.3 | 198. |



Reproduced from best available copy.

| | | | | |
|---|---|---|---|---|
| 2 | .489 | 210. | 8.7 | 206. |
| 4 | .467 | 201. | 7.2 | 202. |
| 4 | .476 | 204. | 7.3 | 202. |
| 5 | .476 | 204. | 7.3 | 204. |
| 6 | .483 | 207. | 7.2 | 252. |
| 7 | .469 | 201. | 5.8 | 265. |
| 8 | .527 | 226. | 4.9 | 375. |
| 9 | .571 | 245. | 5.0 | 371. |
| 10 | .575 | 247. | 5.0 | 374. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .565 | 243. | 5.1 | 368. |
| 14 | .566 | 243. | 5.2 | 395. |
| 15 | .602 | 259. | 5.3 | 393. |
| 16 | .598 | 257. | 5.4 | 389. |
| 17 | .604 | 259. | 5.4 | 390. |
| 18 | .588 | 249. | 5.3 | 355. |
| 19 | .564 | 242. | 5.3 | 361. |
| 20 | .585 | 251. | 5.3 | 394. |
| 21 | .613 | 263. | 5.4 | 393. |
| 22 | .573 | 246. | 5.4 | 360. |
| 23 | .510 | 219. | 6.0 | 256. |
| 24 | .488 | 208. | 6.3 | 255. |

DAY = 51

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .456 | 196. | 5.6 | 249. |
| 2 | .451 | 194. | 5.5 | 256. |
| 3 | .451 | 194. | 5.9 | 257. |
| 4 | .447 | 192. | 5.4 | 256. |
| 5 | .450 | 193. | 5.4 | 255. |
| 6 | .448 | 192. | 5.4 | 255. |
| 7 | .448 | 192. | 5.4 | 237. |
| 8 | .447 | 192. | 5.3 | 254. |
| 9 | .483 | 207. | 4.9 | 325. |
| 10 | .537 | 231. | 4.8 | 372. |
| 11 | .587 | 252. | 4.9 | 388. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .588 | 253. | 4.9 | 385. |
| 14 | .559 | 240. | 4.9 | 387. |
| 15 | .559 | 240. | 4.8 | 390. |
| 16 | .552 | 237. | 5.3 | 324. |
| 17 | .528 | 225. | 5.3 | 336. |
| 18 | .548 | 235. | 5.4 | 389. |
| 19 | .590 | 253. | 5.4 | 387. |
| 20 | .578 | 247. | 5.2 | 391. |
| 21 | .553 | 238. | 4.9 | 375. |
| 22 | .491 | 211. | 5.2 | 279. |
| 23 | .464 | 199. | 5.6 | 279. |
| 24 | .470 | 202. | 5.5 | 293. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .472 | 203. | 5.5 | 284. |
| 2 | .463 | 199. | 5.3 | 267. |
| 3 | .450 | 193. | 5.4 | 242. |
| 4 | .466 | 200. | 7.0 | 204. |
| 5 | .447 | 192. | 7.0 | 203. |
| 6 | .446 | 192. | 7.0 | 202. |
| 7 | .446 | 192. | 6.9 | 202. |
| 8 | .456 | 196. | 6.9 | 246. |
| 9 | .475 | 204. | 6.5 | 275. |
| 10 | .458 | 195. | 4.4 | 360. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .503 | 216. | 4.2 | 374. |
| 14 | .498 | 214. | 4.1 | 372. |
| 15 | .490 | 210. | 4.1 | 359. |
| 16 | .486 | 209. | 4.2 | 362. |
| 17 | .498 | 214. | 4.1 | 369. |
| 18 | .510 | 219. | 4.4 | 366. |
| 19 | .506 | 217. | 4.5 | 366. |
| 20 | .519 | 223. | 4.5 | 390. |
| 21 | .533 | 229. | 4.5 | 386. |
| 22 | .513 | 220. | 4.5 | 353. |
| 23 | .495 | 213. | 4.6 | 321. |
| 24 | .485 | 208. | 4.7 | 300. |

DAY = 53

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .456 | 196. | 5.2 | 273. |
| 2 | .444 | 191. | 5.4 | 258. |
| 3 | .437 | 188. | 5.3 | 252. |
| 4 | .432 | 186. | 5.4 | 238. |
| 5 | .430 | 185. | 5.4 | 243. |
| 6 | .434 | 187. | 5.4 | 243. |
| 7 | .491 | 211. | 6.7 | 243. |
| 8 | .492 | 211. | 6.7 | 245. |
| 9 | .498 | 214. | 6.8 | 245. |
| 10 | .482 | 207. | 6.7 | 239. |
| 11 | .488 | 210. | 6.6 | 244. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .495 | 213. | 6.5 | 242. |
| 14 | .497 | 214. | 6.5 | 242. |
| 15 | .482 | 207. | 6.3 | 238. |
| 16 | .477 | 205. | 6.3 | 237. |
| 17 | .479 | 205. | 6.3 | 239. |
| 18 | .480 | 206. | 6.4 | 238. |
| 19 | .476 | 204. | 6.4 | 238. |
| 20 | .488 | 210. | 6.3 | 267. |
| 21 | .510 | 219. | 6.1 | 263. |
| 22 | .511 | 220. | 6.0 | 264. |
| 23 | .510 | 219. | 6.1 | 265. |
| 24 | .513 | 220. | 6.1 | 253. |

DAY = 54

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .49[illegible] | 210. | 6.8 | 248. |
| 2 | .461 | 198. | 6.7 | 197. |
| 3 | .455 | 195. | 6.8 | 200. |
| 4 | .454 | 195. | 6.7 | 197. |
| 5 | .462 | 198. | 6.6 | 246. |
| 6 | .487 | 209. | 6.4 | 252. |
| 7 | .447 | 190. | 5.2 | 281. |
| 8 | .502 | 216. | 4.5 | 370. |
| 9 | .527 | 226. | 4.4 | 394. |
| 10 | .548 | 235. | 4.7 | 408. |
| 11 | .600 | 258. | 5.3 | 407. |
| 12 | .538 | 231. | 4.8 | 398. |
| 13 | .476 | 204. | 3.9 | 336. |
| 14 | .478 | 205. | 7.1 | 175. |
| 15 | .417 | 179. | 8.2 | 160. |
| 16 | .433 | 186. | 7.2 | 175. |
| 17 | .460 | 201. | 7.9 | 152. |
| 18 | .430 | 185. | 8.8 | 170. |
| 19 | .466 | 198. | 8.3 | 168. |
| 20 | .431 | 185. | 8.9 | 163. |
| 21 | .447 | 192. | 8.2 | 250. |
| 22 | .536 | 230. | 6.2 | 301. |
| 23 | .548 | 235. | 5.7 | 303. |
| 24 | .531 | 228. | 5.1 | 333. |

DAY = 55

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .49[illegible] | 213. | 5.0 | 333. |
| 2 | .500 | 215. | 5.1 | 296. |
| 3 | .48[illegible] | 207. | 5.2 | 266. |
| 4 | .47[illegible] | 204. | 5.2 | 271. |
| 5 | .47[illegible] | 203. | 5.2 | 269. |
| 6 | .49[illegible] | 213. | 5.2 | 295. |
| 7 | .48[illegible] | 210. | 5.1 | 320. |
| 8 | .56[illegible] | 243. | 4.9 | 389. |
| 9 | .58[illegible] | 253. | 4.9 | 391. |
| 10 | .58[illegible] | 251. | 4.9 | 391. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .61[illegible] | 264. | 5.0 | 388. |
| 13 | .60[illegible] | 262. | 5.1 | 388. |
| 14 | .60[illegible] | 260. | 5.0 | 390. |
| 15 | .60[illegible] | 260. | 5.1 | 391. |
| 16 | .60[illegible] | 261. | 5.2 | 392. |
| 17 | .61[illegible] | 262. | 5.1 | 388. |
| 18 | .61[illegible] | 264. | 5.2 | 383. |
| 19 | .59[illegible] | 257. | 5.1 | 380. |
| 20 | .603 | 259. | 5.1 | 391. |
| 21 | .60[illegible] | 261. | 5.2 | 392. |
| 22 | .59[illegible] | 253. | 5.0 | 374. |
| 23 | .52[illegible] | 227. | 5.2 | 305. |
| 24 | .513 | 220. | 5.2 | 297. |

DAY = 56

| HOUR | NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .581 | 232. | 6.1 | 243. |
| 2 | .623 | 248. | 6.8 | 283. |
| 3 | .624 | 249. | 6.8 | 288. |
| 4 | .633 | 272. | 6.8 | 286. |
| 5 | .586 | 249. | 6.7 | 285. |
| 6 | .542 | 220. | 6.1 | 281. |
| 7 | .586 | 235. | 6.1 | 363. |
| 8 | .617 | 245. | 6.3 | 390. |
| 9 | .615 | 268. | 6.2 | 391. |
| 10 | -1.000 | -830. | -1.0 | -1. |
| 11 | .571 | 245. | 5.6 | 398. |
| 12 | .586 | 252. | 5.5 | 391. |
| 13 | .601 | 258. | 5.6 | 389. |
| 14 | .592 | 254. | 5.1 | 388. |
| 15 | .590 | 253. | 5.1 | 391. |
| 16 | .583 | 250. | 5.0 | 392. |
| 17 | .570 | 245. | 4.9 | 380. |
| 18 | .538 | 231. | 4.7 | 363. |
| 19 | .520 | 225. | 4.8 | 362. |
| 20 | .558 | 240. | 5.0 | 391. |
| 21 | .577 | 248. | 5.0 | 393. |
| 22 | .534 | 230. | 4.5 | 386. |
| 23 | .518 | 223. | 4.7 | 320. |
| 24 | .460 | 201. | 4.9 | 276. |

DAY = 57

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .478 | 205. | 4.8 | 302. |
| 2 | .497 | 214. | 5.1 | 287. |
| 3 | .495 | 213. | 5.3 | 279. |
| 4 | .503 | 216. | 5.3 | 288. |
| 5 | .509 | 219. | 5.0 | 312. |
| 6 | .531 | 228. | 4.9 | 334. |
| 7 | .531 | 229. | 4.8 | 354. |
| 8 | .590 | 257. | 6.1 | 261. |
| 9 | .614 | 268. | 6.8 | 253. |
| 10 | .582 | 250. | 5.3 | 394. |
| 11 | .560 | 244. | 4.6 | 397. |
| 12 | .574 | 247. | 4.3 | 101. |
| 13 | -1.000 | -830. | -1.0 | -1. |
| 14 | -1.000 | -830. | -1.0 | -1. |
| 15 | -1.000 | -830. | -1.0 | -1. |
| 16 | .524 | 226. | 4.4 | 393. |
| 17 | .547 | 235. | 4.4 | 389. |
| 18 | .540 | 232. | 4.3 | 391. |
| 19 | .557 | 239. | 4.6 | 391. |
| 20 | .573 | 246. | 4.8 | 392. |
| 21 | .554 | 240. | 4.7 | 392. |
| 22 | .565 | 243. | 4.7 | 393. |
| 23 | .560 | 248. | 4.7 | 380. |
| 24 | .503 | 216. | 4.7 | 326. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .503 | 216. | 5.7 | 262. |
| 2 | .491 | 211. | 6.3 | 265. |
| 3 | .497 | 214. | 6.3 | 266. |
| 4 | .494 | 212. | 6.3 | 263. |
| 5 | .492 | 211. | 6.2 | 262. |
| 6 | .493 | 212. | 6.2 | 280. |
| 7 | .515 | 221. | 5.8 | 335. |
| 8 | .548 | 234. | 5.0 | 390. |
| 9 | .553 | 238. | 4.7 | 389. |
| 10 | .547 | 235. | 4.7 | 392. |
| 11 | .533 | 229. | 4.5 | 394. |
| 12 | .556 | 239. | 4.6 | 388. |
| 13 | .554 | 238. | 4.5 | 394. |
| 14 | .545 | 234. | 4.4 | 395. |
| 15 | .547 | 235. | 4.4 | 393. |
| 16 | .548 | 235. | 4.5 | 391. |
| 17 | .548 | 235. | 4.5 | 392. |
| 18 | .549 | 236. | 4.5 | 392. |
| 19 | .548 | 235. | 4.5 | 390. |
| 20 | .544 | 234. | 4.5 | 400. |
| 21 | .544 | 234. | 4.4 | 392. |
| 22 | .550 | 236. | 4.5 | 390. |
| 23 | .556 | 239. | 4.6 | 393. |
| 24 | .546 | 235. | 4.8 | 263. |

DAY = 59

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .493 | 211. | 8.3 | 157. |
| 2 | .497 | 214. | 8.8 | 149. |
| 3 | .483 | 210. | 9.1 | 150. |
| 4 | .487 | 209. | 9.1 | 152. |
| 5 | .490 | 210. | 9.1 | 152. |
| 6 | .493 | 211. | 9.1 | 141. |
| 7 | .477 | 205. | 9.9 | 147. |
| 8 | .456 | 196. | 10.5 | 147. |
| 9 | .413 | 180. | 8.6 | 150. |
| 10 | .456 | 196. | 10.3 | 148. |
| 11 | .460 | 198. | 10.0 | 162. |
| 12 | .505 | 217. | 7.0 | 240. |
| 13 | .529 | 226. | 5.4 | 326. |
| 14 | .533 | 231. | 5.5 | 307. |
| 15 | .607 | 261. | 5.3 | 384. |
| 16 | .623 | 268. | 5.3 | 393. |
| 17 | .627 | 269. | 5.3 | 396. |
| 18 | .615 | 264. | 5.1 | 396. |
| 19 | .606 | 260. | 5.8 | 371. |
| 20 | .638 | 274. | 5.8 | 393. |
| 21 | .642 | 276. | 5.8 | 394. |
| 22 | .628 | 270. | 5.7 | 394. |
| 23 | .613 | 263. | 5.7 | 387. |
| 24 | .569 | 244. | 5.9 | 346. |

DAY = 60

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .514 | 221. | 6.2 | 265. |
| 2 | .501 | 215. | 6.8 | 259. |
| 3 | .494 | 212. | 6.7 | 264. |
| 4 | .570 | 245. | 6.8 | 250. |
| 5 | .607 | 261. | 6.6 | 253. |
| 6 | .603 | 258. | 6.5 | 255. |
| 7 | .574 | 247. | 7.3 | 243. |
| 8 | .574 | 247. | 6.7 | 255. |
| 9 | .562 | 241. | 6.4 | 286. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .534 | 229. | 5.0 | 319. |
| 12 | .529 | 227. | 5.0 | 318. |
| 13 | .533 | 229. | 5.0 | 325. |
| 14 | .526 | 226. | 5.0 | 318. |
| 15 | .510 | 219. | 4.9 | 315. |
| 16 | .510 | 219. | 5.0 | 307. |
| 17 | .511 | 220. | 4.9 | 297. |
| 18 | .493 | 212. | 5.3 | 283. |
| 19 | .495 | 213. | 5.3 | 298. |
| 20 | .515 | 221. | 5.0 | 362. |
| 21 | .553 | 238. | 4.9 | 364. |
| 22 | .520 | 223. | 4.8 | 339. |
| 23 | .485 | 208. | 4.9 | 323. |
| 24 | .481 | 207. | 5.3 | 295. |

DAY = 61



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .474 | 204. | 5.6 | 257. |
| 2 | .473 | 203. | 5.8 | 256. |
| 3 | .473 | 203. | 5.8 | 256. |
| 4 | .471 | 204. | 5.7 | 255. |
| 5 | .403 | 173. | 6.7 | 277. |
| 6 | .311 | 134. | 12.3 | 332. |
| 7 | .361 | 155. | 10.4 | 395. |
| 8 | .306 | 131. | 12.4 | 380. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .519 | 223. | 4.5 | 323. |
| 11 | .481 | 207. | 4.6 | 392. |
| 12 | .513 | 223. | 4.4 | 390. |
| 13 | .521 | 225. | 4.5 | 391. |
| 14 | .531 | 228. | 4.4 | 391. |
| 15 | .533 | 229. | 4.6 | 391. |
| 16 | .523 | 227. | 4.4 | 378. |
| 17 | .565 | 243. | 5.2 | 349. |
| 18 | .591 | 253. | 5.3 | 358. |
| 19 | .603 | 259. | 5.4 | 361. |
| 20 | .611 | 262. | 5.4 | 387. |
| 21 | .643 | 278. | 5.3 | 397. |
| 22 | .643 | 276. | 5.3 | 394. |
| 23 | .665 | 286. | 5.7 | 348. |
| 24 | .540 | 232. | 5.8 | 247. |

DAY = 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .549 | 236. | 8.1 | 241. |
| 2 | .568 | 244. | 8.0 | 248. |
| 3 | .563 | 242. | 7.9 | 242. |
| 4 | .559 | 240. | 8.1 | 243. |
| 5 | .528 | 227. | 7.6 | 283. |
| 6 | .500 | 215. | 6.2 | 322. |
| 7 | .566 | 243. | 6.0 | 385. |
| 8 | .615 | 264. | 6.0 | 393. |
| 9 | .592 | 254. | 5.4 | 392. |
| 10 | .578 | 248. | 5.3 | 394. |
| 11 | .555 | 238. | 4.7 | 393. |
| 12 | .548 | 235. | 4.6 | 391. |
| 13 | .558 | 240. | 4.7 | 395. |
| 14 | .563 | 242. | 4.8 | 391. |
| 15 | .518 | 223. | 4.3 | 392. |
| 16 | .576 | 247. | 4.5 | 400. |
| 17 | .578 | 248. | 4.0 | 399. |
| 18 | .571 | 245. | 4.0 | 394. |
| 19 | .569 | 244. | 4.1 | 397. |
| 20 | .583 | 250. | 4.1 | 401. |
| 21 | .584 | 252. | 4.1 | 396. |
| 22 | .569 | 244. | 4.2 | 392. |
| 23 | .559 | 240. | 4.2 | 343. |
| 24 | .504 | 217. | 5.1 | 262. |

DAY = 63

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .494 | 212. | 6.1 | 246. |
| 2 | .523 | 224. | 7.5 | 233. |
| 3 | .524 | 226. | 7.8 | 207. |
| 4 | .517 | 222. | 7.9 | 263. |
| 5 | .513 | 220. | 5.6 | 294. |
| 6 | .515 | 221. | 5.2 | 319. |
| 7 | .545 | 234. | 4.5 | 393. |
| 8 | .563 | 241. | 4.2 | 398. |
| 9 | .570 | 245. | 4.0 | 399. |
| 10 | .577 | 248. | 4.0 | 396. |
| 11 | .574 | 247. | 4.0 | 390. |
| 12 | .561 | 241. | 4.1 | 396. |
| 13 | .564 | 243. | 4.1 | 396. |
| 14 | .564 | 242. | 4.1 | 397. |
| 15 | .572 | 246. | 4.1 | 395. |
| 16 | .583 | 250. | 4.2 | 396. |
| 17 | .584 | 251. | 4.1 | 396. |
| 18 | .579 | 248. | 4.1 | 397. |
| 19 | .581 | 250. | 4.1 | 396. |
| 20 | .576 | 247. | 4.1 | 396. |
| 21 | .573 | 246. | 4.0 | 395. |
| 22 | .580 | 249. | 4.1 | 396. |
| 23 | .574 | 247. | 4.1 | 361. |
| 24 | .535 | 230. | 4.7 | 293. |

DAY = 64

| HOUR | NOx LB/10**6 BTU | NOx NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .513 | 220. | 5.6 | 255. |
| 2 | .577 | 248. | 6.9 | 237. |
| 3 | .584 | 251. | 7.1 | 235. |
| 4 | .576 | 247. | 6.9 | 239. |
| 5 | .561 | 241. | 6.8 | 239. |
| 6 | .570 | 245. | 7.0 | 300. |
| 7 | .512 | 220. | 5.7 | 360. |
| 8 | .588 | 253. | 8.7 | 397. |
| 9 | .594 | 255. | 4.6 | 398. |
| 10 | .582 | 250. | 4.5 | 396. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .590 | 253. | 4.7 | 396. |
| 13 | .585 | 251. | 4.8 | 379. |
| 14 | .522 | 224. | 4.1 | 401. |
| 15 | .519 | 223. | 3.8 | 402. |
| 16 | .507 | 218. | 3.9 | 398. |
| 17 | .501 | 215. | 3.8 | 398. |
| 18 | .513 | 220. | 4.6 | 343. |
| 19 | .548 | 234. | 4.7 | 334. |
| 20 | .565 | 243. | 4.7 | 395. |
| 21 | .559 | 240. | 4.2 | 394. |
| 22 | .505 | 217. | 3.9 | 395. |
| 23 | .512 | 220. | 3.9 | 392. |
| 24 | .519 | 223. | 3.9 | 367. |

APPENDIX K

PROPRIETARY INFORMATION - UNIT A

Input Data

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

CONFIDENTIAL INFORMATION UNIT A

COMBUSTION ENGR BOILER WITH OVERFIRE AIR 350 MWE GROSS

SUBBITUMINOUS (C) COAL

NOX MONITOR RELATIVE ACCURACY = 8.0 PC

DAY 1 = 1 JANUARY 1981

PERFORMANCE NOX = 0.61 LB/10**6BTU (262 NG/J)

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 8.3 | 213. |
| 2 | .450 | 193. | 8.2 | 240. |
| 3 | .440 | 189. | 8.3 | 230. |
| 4 | .430 | 185. | 8.3 | 214. |
| 5 | .420 | 180. | 8.7 | 211. |
| 6 | .460 | 198. | 8.7 | 216. |
| 7 | .400 | 172. | 8.5 | 199. |
| 8 | .460 | 198. | 8.5 | 228. |
| 9 | .490 | 210. | 8.3 | 236. |
| 10 | .520 | 223. | 8.0 | 262. |
| 11 | .560 | 241. | 7.5 | 283. |
| 12 | .590 | 253. | 7.4 | 294. |
| 13 | .560 | 241. | 7.4 | 292. |
| 14 | .530 | 228. | 7.5 | 276. |
| 15 | .490 | 210. | 7.7 | 257. |
| 16 | .470 | 202. | 7.8 | 243. |
| 17 | .460 | 198. | 7.9 | 234. |
| 18 | .520 | 223. | 7.6 | 257. |
| 19 | .590 | 253. | 7.3 | 299. |
| 20 | .590 | 253. | 7.3 | 296. |
| 21 | .620 | 266. | 7.3 | 297. |
| 22 | .620 | 266. | 7.4 | 294. |
| 23 | .580 | 249. | 7.7 | 282. |
| 24 | .430 | 185. | 9.6 | 163. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 9.7 | 148. |
| 2 | .350 | 150. | 9.8 | 149. |
| 3 | .360 | 155. | 9.9 | 149. |
| 4 | .370 | 159. | 10.0 | 149. |
| 5 | .370 | 159. | 9.8 | 155. |
| 6 | .400 | 172. | 9.0 | 196. |
| 7 | .420 | 180. | 8.7 | 218. |
| 8 | .480 | 206. | 8.1 | 265. |
| 9 | .540 | 232. | 7.6 | 305. |
| 10 | .560 | 241. | 7.4 | 311. |
| 11 | .560 | 241. | 7.3 | 313. |
| 12 | .550 | 236. | 7.2 | 313. |
| 13 | .530 | 228. | 7.2 | 309. |
| 14 | .550 | 236. | 7.2 | 307. |
| 15 | .560 | 241. | 7.1 | 308. |
| 16 | .560 | 241. | 7.1 | 303. |
| 17 | .570 | 245. | 7.2 | 297. |
| 18 | .570 | 245. | 7.3 | 290. |
| 19 | .580 | 249. | 7.1 | 291. |
| 20 | .620 | 266. | 7.2 | 289. |

| | | | | |
|---|---|---|---|---|
| 21 | .610 | 262. | 7.2 | 288. |
| 22 | .550 | 236. | 7.4 | 272. |
| 23 | .460 | 198. | 8.3 | 216. |
| 24 | .330 | 142. | 9.7 | 153. |

DAY # 3

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 9.7 | 149. |
| 2 | .280 | 120. | 9.7 | 149. |
| 3 | .270 | 116. | 9.8 | 150. |
| 4 | .270 | 116. | 9.8 | 149. |
| 5 | .280 | 120. | 10.0 | 149. |
| 6 | .300 | 129. | 10.0 | 149. |
| 7 | .300 | 129. | 10.0 | 149. |
| 8 | .330 | 142. | 8.8 | 213. |
| 9 | .550 | 236. | 7.7 | 298. |
| 10 | .570 | 245. | 7.5 | 304. |
| 11 | .570 | 245. | 7.4 | 302. |
| 12 | .570 | 245. | 7.4 | 298. |
| 13 | .550 | 236. | 7.6 | 281. |
| 14 | .540 | 232. | 7.6 | 274. |
| 15 | .480 | 206. | 7.6 | 253. |
| 16 | .470 | 202. | 7.8 | 247. |
| 17 | .490 | 210. | 7.8 | 254. |
| 18 | .580 | 249. | 7.4 | 289. |
| 19 | .600 | 258. | 7.2 | 303. |
| 20 | .590 | 253. | 7.1 | 302. |
| 21 | .500 | 215. | 8.2 | 228. |
| 22 | .380 | 163. | 9.2 | 179. |
| 23 | .360 | 155. | 9.2 | 179. |
| 24 | .370 | 159. | 9.3 | 174. |

DAY # 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 9.7 | 174. |
| 2 | .410 | 176. | 9.2 | 174. |
| 3 | .410 | 176. | 9.0 | 174. |
| 4 | .410 | 176. | 9.0 | 173. |
| 5 | .400 | 172. | 9.0 | 174. |
| 6 | .390 | 168. | 9.1 | 174. |
| 7 | .400 | 172. | 9.0 | 174. |
| 8 | .400 | 172. | 8.8 | 185. |
| 9 | .450 | 193. | 7.8 | 228. |
| 10 | .490 | 210. | 7.6 | 268. |
| 11 | .500 | 215. | 7.7 | 268. |
| 12 | .520 | 223. | 7.7 | 268. |
| 13 | .530 | 228. | 7.7 | 268. |
| 14 | .510 | 219. | 7.7 | 268. |
| 15 | .480 | 206. | 7.6 | 267. |
| 16 | .500 | 215. | 7.6 | 261. |
| 17 | .520 | 223. | 7.6 | 256. |
| 18 | .560 | 241. | 7.4 | 263. |
| 19 | .600 | 258. | 7.2 | 295. |

| | | | | |
|---|---|---|---|---|
| 20 | .570 | 245. | 7.2 | 292. |
| 21 | .570 | 245. | 7.3 | 288. |
| 22 | .560 | 241. | 7.4 | 277. |
| 23 | .520 | 223. | 7.7 | 253. |
| 24 | .420 | 180. | 8.2 | 218. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 7.9 | 255. |
| 2 | .520 | 223. | 7.9 | 251. |
| 3 | .450 | 193. | 8.7 | 186. |
| 4 | .400 | 172. | 9.2 | 159. |
| 5 | .420 | 180. | 8.9 | 183. |
| 6 | .480 | 206. | 8.0 | 253. |
| 7 | .520 | 223. | 7.6 | 283. |
| 8 | .540 | 232. | 7.2 | 305. |
| 9 | .580 | 249. | 7.3 | 300. |
| 10 | .610 | 262. | 7.2 | 312. |
| 11 | .650 | 279. | 7.1 | 314. |
| 12 | .600 | 258. | 7.2 | 312. |
| 13 | .570 | 245. | 7.1 | 312. |
| 14 | .560 | 241. | 7.1 | 313. |
| 15 | .620 | 266. | 7.0 | 314. |
| 16 | .630 | 271. | 7.0 | 313. |
| 17 | .690 | 296. | 7.1 | 314. |
| 18 | .730 | 314. | 7.0 | 313. |
| 19 | .710 | 305. | 7.0 | 313. |
| 20 | .620 | 266. | 7.3 | 286. |
| 21 | .480 | 206. | 7.5 | 254. |
| 22 | .430 | 185. | 8.4 | 216. |
| 23 | .430 | 185. | 9.4 | 185. |
| 24 | .300 | 129. | 9.8 | 154. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 8.0 | 195. |
| 2 | .230 | 99. | 10.0 | 149. |
| 3 | .210 | 90. | 10.1 | 150. |
| 4 | .220 | 95. | 10.0 | 149. |
| 5 | .210 | 90. | 9.7 | 150. |
| 6 | .220 | 95. | 9.1 | 156. |
| 7 | .260 | 112. | 8.6 | 207. |
| 8 | .260 | 112. | 8.0 | 237. |
| 9 | .270 | 116. | 7.7 | 265. |
| 10 | .320 | 137. | 7.3 | 303. |
| 11 | .310 | 133. | 7.0 | 315. |
| 12 | .310 | 133. | 6.9 | 320. |
| 13 | .330 | 142. | 6.9 | 319. |
| 14 | .330 | 142. | 6.9 | 319. |
| 15 | .360 | 155. | 8.0 | 227. |
| 16 | .400 | 172. | 7.9 | 229. |
| 17 | .430 | 185. | 7.8 | 252. |
| 18 | .460 | 198. | 7.6 | 267. |

| | | | | |
|---|---|---|---|---|
| 19 | .520 | 223. | 7.3 | 286. |
| 20 | .570 | 245. | 7.2 | 297. |
| 21 | .550 | 236. | 7.3 | 287. |
| 22 | .550 | 236. | 7.4 | 283. |
| 23 | .470 | 202. | 8.1 | 236. |
| 24 | .290 | 125. | 9.6 | 160. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 9.7 | 149. |
| 2 | .270 | 116. | 9.5 | 149. |
| 3 | .260 | 112. | 9.5 | 149. |
| 4 | .250 | 107. | 9.5 | 149. |
| 5 | .230 | 99. | 9.5 | 149. |
| 6 | .230 | 99. | 9.5 | 149. |
| 7 | .250 | 107. | 9.4 | 173. |
| 8 | .400 | 172. | 8.1 | 254. |
| 9 | .490 | 210. | 7.5 | 299. |
| 10 | .490 | 210. | 7.5 | 299. |
| 11 | .490 | 210. | 7.4 | 299. |
| 12 | .500 | 215. | 7.4 | 298. |
| 13 | .480 | 206. | 7.3 | 298. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .350 | 150. | 7.3 | 298. |
| 16 | .520 | 223. | 7.3 | 297. |
| 17 | .530 | 228. | 7.6 | 292. |
| 18 | .510 | 219. | 7.5 | 286. |
| 19 | .530 | 228. | 7.5 | 286. |
| 20 | .520 | 223. | 7.6 | 286. |
| 21 | .530 | 228. | 7.6 | 286. |
| 22 | .530 | 228. | 7.9 | 264. |
| 23 | .410 | 176. | 8.5 | 199. |
| 24 | .370 | 159. | 9.6 | 167. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 9.6 | 170. |
| 2 | .400 | 172. | 8.9 | 209. |
| 3 | .380 | 163. | 9.0 | 193. |
| 4 | .320 | 137. | 9.3 | 176. |
| 5 | .300 | 129. | 9.5 | 173. |
| 6 | .300 | 129. | 9.4 | 174. |
| 7 | .310 | 133. | 9.2 | 188. |
| 8 | .320 | 137. | 8.9 | 211. |
| 9 | .420 | 180. | 8.0 | 236. |
| 10 | .550 | 236. | 7.7 | 295. |
| 11 | .580 | 249. | 7.3 | 298. |
| 12 | .490 | 210. | 7.3 | 279. |
| 13 | .490 | 210. | 7.3 | 278. |
| 14 | .500 | 215. | 7.3 | 278. |
| 15 | .510 | 219. | 7.3 | 280. |
| 16 | .500 | 215. | 7.3 | 283. |
| 17 | .500 | 215. | 7.3 | 283. |

| | | | | |
|---|---|---|---|---|
| 18 | .480 | 206. | 7.3 | 283. |
| 19 | .490 | 210. | 7.2 | 284. |
| 20 | .490 | 210. | 7.1 | 283. |
| 21 | .500 | 215. | 7.2 | 280. |
| 22 | .410 | 176. | 8.2 | 222. |
| 23 | .380 | 163. | 8.0 | 208. |
| 24 | .430 | 185. | 8.0 | 245. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 9.5 | 179. |
| 2 | .300 | 129. | 10.0 | 149. |
| 3 | .300 | 129. | 9.9 | 149. |
| 4 | .310 | 133. | 9.8 | 157. |
| 5 | .340 | 146. | 9.1 | 191. |
| 6 | .390 | 168. | 8.7 | 208. |
| 7 | .380 | 163. | 8.7 | 214. |
| 8 | .440 | 189. | 8.3 | 245. |
| 9 | .500 | 215. | 7.8 | 284. |
| 10 | .530 | 228. | 7.5 | 304. |
| 11 | .550 | 236. | 7.4 | 308. |
| 12 | .530 | 228. | 7.4 | 298. |
| 13 | .510 | 219. | 7.6 | 295. |
| 14 | .510 | 219. | 7.4 | 291. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .450 | 193. | 7.8 | 259. |
| 17 | .450 | 193. | 7.9 | 258. |
| 18 | .500 | 215. | 7.3 | 278. |
| 19 | .460 | 198. | 7.7 | 264. |
| 20 | .420 | 180. | 8.0 | 246. |
| 21 | .430 | 185. | 8.0 | 247. |
| 22 | .440 | 189. | 8.1 | 244. |
| 23 | .400 | 172. | 9.0 | 181. |
| 24 | .350 | 150. | 9.4 | 149. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 9.6 | 149. |
| 2 | .360 | 155. | 9.5 | 149. |
| 3 | .400 | 172. | 8.8 | 185. |
| 4 | .470 | 202. | 8.4 | 244. |
| 5 | .470 | 202. | 8.3 | 252. |
| 6 | .520 | 223. | 8.0 | 273. |
| 7 | .550 | 236. | 7.9 | 289. |
| 8 | .540 | 232. | 7.7 | 291. |
| 9 | .580 | 249. | 7.6 | 303. |
| 10 | .540 | 232. | 7.8 | 222. |
| 11 | .530 | 228. | 8.0 | 273. |
| 12 | .550 | 236. | 8.0 | 273. |
| 13 | .500 | 215. | 8.2 | 246. |
| 14 | .330 | 142. | 8.2 | 237. |
| 15 | .320 | 137. | 7.8 | 237. |
| 16 | .340 | 146. | 8.6 | 237. |

| | | | | |
|---|---|---|---|---|
| 17 | .410 | 176. | 8.4 | 238. |
| 18 | .520 | 223. | 8.0 | 267. |
| 19 | .520 | 223. | 7.9 | 272. |
| 20 | .530 | 228. | 7.9 | 277. |
| 21 | .570 | 245. | 7.9 | 286. |
| 22 | .570 | 245. | 7.8 | 286. |
| 23 | .480 | 206. | 8.6 | 243. |
| 24 | .310 | 133. | 9.6 | 154. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 10.5 | 153. |
| 2 | .370 | 159. | 10.9 | 139. |
| 3 | .360 | 155. | 11.0 | 136. |
| 4 | .380 | 163. | 11.0 | 134. |
| 5 | .390 | 168. | 11.1 | 134. |
| 6 | .340 | 146. | 10.7 | 151. |
| 7 | .310 | 133. | 9.9 | 179. |
| 8 | .440 | 189. | 9.0 | 222. |
| 9 | .420 | 180. | 8.9 | 225. |
| 10 | .420 | 180. | 8.6 | 238. |
| 11 | .420 | 180. | 8.9 | 238. |
| 12 | .440 | 189. | 8.8 | 239. |
| 13 | .430 | 185. | 8.5 | 238. |
| 14 | .440 | 189. | 8.5 | 239. |
| 15 | .430 | 185. | 8.5 | 238. |
| 16 | .420 | 180. | 8.3 | 239. |
| 17 | .510 | 219. | 7.9 | 275. |
| 18 | .550 | 236. | 7.5 | 300. |
| 19 | .550 | 236. | 7.4 | 300. |
| 20 | .560 | 241. | 7.5 | 299. |
| 21 | .530 | 228. | 7.4 | 297. |
| 22 | .350 | 150. | 8.4 | 228. |
| 23 | .290 | 125. | 8.5 | 198. |
| 24 | .310 | 133. | 9.0 | 192. |

DAY = 14

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 10.6 | 149. |
| 2 | .320 | 137. | 10.5 | 149. |
| 3 | .320 | 137. | 10.4 | 149. |
| 4 | .320 | 137. | 10.5 | 149. |
| 5 | .310 | 133. | 10.5 | 151. |
| 6 | .290 | 125. | 9.8 | 175. |
| 7 | .310 | 133. | 9.1 | 209. |
| 8 | .340 | 146. | 9.1 | 219. |
| 9 | .360 | 155. | 9.3 | 222. |
| 10 | .390 | 168. | 8.9 | 238. |
| 11 | .390 | 168. | 8.8 | 237. |
| 12 | .390 | 168. | 8.8 | 237. |
| 13 | .350 | 150. | 9.1 | 218. |
| 14 | .360 | 155. | 9.0 | 219. |
| 15 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 16 | .340 | 146. | 5.2 | 219. |
| 17 | .330 | 142. | 5.7 | 217. |
| 18 | .320 | 137. | 3.6 | 246. |
| 19 | .320 | 137. | 2.9 | 255. |
| 20 | .350 | 150. | 4.5 | 261. |
| 21 | .450 | 193. | 7.8 | 261. |
| 22 | .450 | 193. | 8.0 | 261. |
| 23 | .380 | 163. | 8.0 | 221. |
| 24 | .360 | 155. | 9.6 | 188. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 9.9 | 159. |
| 2 | .370 | 159. | 10.1 | 158. |
| 3 | .370 | 159. | 10.2 | 159. |
| 4 | .370 | 159. | 10.2 | 159. |
| 5 | .370 | 159. | 10.3 | 158. |
| 6 | .370 | 159. | 10.0 | 178. |
| 7 | .380 | 163. | 9.6 | 193. |
| 8 | .420 | 180. | 9.6 | 216. |
| 9 | .520 | 223. | 7.9 | 299. |
| 10 | .530 | 228. | 7.6 | 318. |
| 11 | .510 | 219. | 7.6 | 306. |
| 12 | .500 | 215. | 7.6 | 298. |
| 13 | .490 | 210. | 7.7 | 278. |
| 14 | .530 | 228. | 7.7 | 307. |
| 15 | .540 | 232. | 7.6 | 314. |
| 16 | .530 | 228. | 7.8 | 300. |
| 17 | .540 | 232. | 7.4 | 294. |
| 18 | .520 | 223. | 7.5 | 284. |
| 19 | .520 | 223. | 7.5 | 288. |
| 20 | .510 | 219. | 7.7 | 274. |
| 21 | .410 | 176. | 8.1 | 224. |
| 22 | .440 | 189. | 8.5 | 222. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | .370 | 159. | 9.6 | 153. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 8.0 | 195. |
| 2 | .230 | 99. | 10.0 | 149. |
| 3 | .210 | 90. | 10.1 | 150. |
| 4 | .220 | 95. | 10.0 | 149. |
| 5 | .210 | 90. | 9.7 | 150. |
| 6 | .220 | 95. | 9.1 | 156. |
| 7 | .260 | 112. | 8.6 | 207. |
| 8 | .260 | 112. | 8.0 | 237. |
| 9 | .270 | 116. | 7.7 | 265. |
| 10 | .320 | 137. | 7.3 | 303. |
| 11 | .560 | 241. | 7.6 | 236. |
| 12 | .570 | 245. | 7.6 | 316. |
| 13 | .550 | 236. | 7.7 | 319. |
| 14 | .520 | 223. | 7.6 | 316. |

| | | | | |
|---|---|---|---|---|
| 15 | .510 | 219. | 7.6 | 316. |
| 16 | .530 | 228. | 7.7 | 305. |
| 17 | .590 | 253. | 7.8 | 306. |
| 18 | .560 | 241. | 7.7 | 303. |
| 19 | .570 | 245. | 7.8 | 304. |
| 20 | .570 | 245. | 7.9 | 291. |
| 21 | .490 | 210. | 8.6 | 243. |
| 22 | .380 | 163. | 8.9 | 208. |
| 23 | .280 | 120. | 8.9 | 199. |
| 24 | .330 | 142. | 8.9 | 198. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 9.0 | 199. |
| 2 | .370 | 159. | 9.5 | 177. |
| 3 | .370 | 159. | 9.9 | 148. |
| 4 | .360 | 155. | 10.0 | 149. |
| 5 | .350 | 150. | 9.9 | 149. |
| 6 | .340 | 146. | 10.0 | 149. |
| 7 | .330 | 142. | 9.9 | 172. |
| 8 | .450 | 193. | 9.3 | 216. |
| 9 | .530 | 228. | 8.7 | 261. |
| 10 | .580 | 249. | 8.1 | 290. |
| 11 | .570 | 245. | 7.8 | 299. |
| 12 | .570 | 245. | 7.8 | 299. |
| 13 | .570 | 245. | 7.8 | 299. |
| 14 | .580 | 249. | 7.8 | 299. |
| 15 | .580 | 249. | 7.7 | 299. |
| 16 | .570 | 245. | 7.8 | 291. |
| 17 | .500 | 215. | 8.2 | 261. |
| 18 | .500 | 215. | 8.2 | 258. |
| 19 | .490 | 210. | 8.2 | 258. |
| 20 | .510 | 219. | 8.2 | 258. |
| 21 | .510 | 219. | 8.3 | 253. |
| 22 | .400 | 172. | 8.7 | 208. |
| 23 | .400 | 172. | 9.4 | 193. |
| 24 | .390 | 168. | 10.8 | 158. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 11.8 | 153. |
| 2 | .380 | 163. | 10.8 | 149. |
| 3 | .380 | 163. | 10.5 | 150. |
| 4 | .370 | 159. | 10.4 | 149. |
| 5 | .370 | 159. | 10.6 | 149. |
| 6 | .360 | 155. | 10.6 | 149. |
| 7 | .360 | 155. | 10.5 | 148. |
| 8 | .350 | 150. | 9.6 | 181. |
| 9 | .360 | 155. | 9.4 | 199. |
| 10 | .400 | 172. | 9.1 | 213. |
| 11 | .470 | 202. | 8.7 | 250. |
| 12 | .470 | 202. | 8.6 | 254. |
| 13 | .470 | 202. | 8.6 | 253. |

| | | | | |
|---|---|---|---|---|
| 14 | .470 | 202. | 8.6 | 255. |
| 15 | .470 | 202. | 8.4 | 254. |
| 16 | .420 | 180. | 8.9 | 221. |
| 17 | .390 | 168. | 9.3 | 199. |
| 18 | .400 | 172. | 9.1 | 206. |
| 19 | .430 | 185. | 8.6 | 226. |
| 20 | .420 | 180. | 8.7 | 228. |
| 21 | .430 | 185. | 8.7 | 228. |
| 22 | .380 | 163. | 9.6 | 216. |
| 23 | .280 | 120. | 9.9 | 162. |
| 24 | .300 | 129. | 10.1 | 154. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 10.2 | 154. |
| 2 | .330 | 142. | 10.1 | 153. |
| 3 | .330 | 142. | 10.2 | 154. |
| 4 | .320 | 137. | 10.1 | 154. |
| 5 | .310 | 133. | 10.2 | 153. |
| 6 | .310 | 133. | 10.2 | 154. |
| 7 | .310 | 133. | 10.1 | 154. |
| 8 | .330 | 142. | 9.2 | 195. |
| 9 | .350 | 150. | 9.0 | 223. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .400 | 172. | 8.4 | 364. |
| 12 | .430 | 185. | 7.6 | 272. |
| 13 | .410 | 176. | 7.6 | 258. |
| 14 | .410 | 176. | 7.6 | 248. |
| 15 | .400 | 172. | 6.9 | 253. |
| 16 | .400 | 172. | 7.8 | 252. |
| 17 | .380 | 163. | 8.1 | 242. |
| 18 | .390 | 168. | 8.2 | 243. |
| 19 | .410 | 176. | 7.9 | 255. |
| 20 | .400 | 172. | 7.9 | 255. |
| 21 | .400 | 172. | 8.0 | 251. |
| 22 | .370 | 159. | 8.3 | 229. |
| 23 | .370 | 159. | 8.6 | 224. |
| 24 | .340 | 146. | 8.6 | 208. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 9.8 | 159. |
| 2 | .340 | 146. | 9.6 | 149. |
| 3 | .340 | 146. | 10.2 | 149. |
| 4 | .320 | 137. | 10.3 | 149. |
| 5 | .320 | 137. | 10.3 | 149. |
| 6 | .340 | 146. | 10.3 | 149. |
| 7 | .330 | 142. | 10.4 | 150. |
| 8 | .310 | 133. | 9.4 | 184. |
| 9 | .420 | 180. | 9.0 | 220. |
| 10 | .410 | 176. | 8.9 | 223. |
| 11 | .430 | 185. | 8.7 | 228. |
| 12 | .410 | 176. | 8.5 | 229. |

| | | | | |
|---|---|---|---|---|
| 13 | .400 | 172. | 8.7 | 228. |
| 14 | .430 | 185. | 8.7 | 242. |
| 15 | .440 | 189. | 8.3 | 257. |
| 16 | .430 | 185. | 8.2 | 249. |
| 17 | .430 | 185. | 8.3 | 250. |
| 18 | .450 | 193. | 8.2 | 250. |
| 19 | .470 | 202. | 8.0 | 262. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .330 | 142. | 13.3 | 83. |
| 22 | .360 | 155. | 11.3 | 114. |
| 23 | .300 | 129. | 9.3 | 147. |
| 24 | .330 | 142. | 9.9 | 150. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 10.4 | 149. |
| 2 | .340 | 146. | 10.2 | 149. |
| 3 | .340 | 146. | 10.0 | 150. |
| 4 | .310 | 133. | 8.9 | 149. |
| 5 | .310 | 133. | 9.0 | 149. |
| 6 | .300 | 129. | 9.0 | 149. |
| 7 | .310 | 133. | 8.9 | 153. |
| 8 | .400 | 172. | 8.5 | 234. |
| 9 | .520 | 223. | 7.9 | 290. |
| 10 | .370 | 159. | 8.6 | 253. |
| 11 | .310 | 133. | 8.2 | 252. |
| 12 | .420 | 180. | 8.5 | 252. |
| 13 | .560 | 241. | 8.2 | 272. |
| 14 | .610 | 262. | 7.5 | 301. |
| 15 | .600 | 258. | 7.2 | 318. |
| 16 | .630 | 271. | 7.6 | 314. |
| 17 | .640 | 275. | 7.6 | 314. |
| 18 | .650 | 279. | 7.5 | 314. |
| 19 | .650 | 279. | 7.5 | 315. |
| 20 | .640 | 275. | 7.5 | 314. |
| 21 | .610 | 262. | 7.5 | 299. |
| 22 | .510 | 219. | 8.2 | 253. |
| 23 | .400 | 172. | 8.6 | 216. |
| 24 | .380 | 163. | 8.6 | 197. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 9.9 | 149. |
| 2 | .380 | 163. | 9.8 | 149. |
| 3 | .370 | 159. | 9.5 | 149. |
| 4 | .340 | 146. | 8.7 | 149. |
| 5 | .330 | 142. | 9.3 | 150. |
| 6 | .320 | 137. | 8.9 | 160. |
| 7 | .330 | 142. | 8.9 | 165. |
| 8 | .460 | 198. | 8.0 | 239. |
| 9 | .490 | 210. | 7.7 | 259. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 12 | .460 | 198. | 8.3 | 243. |
| 13 | .500 | 215. | 8.3 | 242. |
| 14 | .580 | 249. | 8.3 | 243. |
| 15 | .410 | 176. | 8.0 | 248. |
| 16 | .410 | 176. | 8.0 | 237. |
| 17 | .230 | 99. | 8.0 | 242. |
| 18 | .410 | 176. | 8.1 | 241. |
| 19 | .400 | 172. | 8.1 | 244. |
| 20 | .380 | 163. | 7.9 | 242. |
| 21 | .400 | 172. | 8.0 | 241. |
| 22 | .400 | 172. | 7.5 | 237. |
| 23 | .370 | 159. | 7.3 | 212. |
| 24 | .340 | 146. | 8.6 | 185. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 9.4 | 173. |
| 2 | .270 | 116. | 9.9 | 148. |
| 3 | .270 | 116. | 10.0 | 149. |
| 4 | .280 | 120. | 10.0 | 149. |
| 5 | .270 | 116. | 10.1 | 149. |
| 6 | .270 | 116. | 10.1 | 148. |
| 7 | .260 | 112. | 9.7 | 155. |
| 8 | .260 | 112. | 9.4 | 173. |
| 9 | .250 | 107. | 9.4 | 180. |
| 10 | .290 | 125. | 9.1 | 198. |
| 11 | .280 | 120. | 9.1 | 199. |
| 12 | .290 | 125. | 9.0 | 198. |
| 13 | .280 | 120. | 8.8 | 210. |
| 14 | .280 | 120. | 8.8 | 213. |
| 15 | .290 | 125. | 8.7 | 213. |
| 16 | .280 | 120. | 8.6 | 211. |
| 17 | .270 | 116. | 8.6 | 213. |
| 18 | .260 | 112. | 8.6 | 214. |
| 19 | .270 | 116. | 8.6 | 227. |
| 20 | .300 | 129. | 8.1 | 253. |
| 21 | .450 | 193. | 7.7 | 290. |
| 22 | .490 | 210. | 7.7 | 296. |
| 23 | .470 | 202. | 7.7 | 288. |
| 24 | .350 | 150. | 8.5 | 221. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 10.0 | 150. |
| 2 | .280 | 120. | 10.1 | 148. |
| 3 | .280 | 120. | 10.1 | 149. |
| 4 | .300 | 129. | 10.2 | 148. |
| 5 | .290 | 125. | 10.1 | 149. |
| 6 | .290 | 125. | 10.2 | 150. |
| 7 | .310 | 133. | 9.3 | 181. |
| 8 | .430 | 185. | 8.7 | 247. |
| 9 | .410 | 176. | 8.8 | 258. |
| 10 | .350 | 150. | 9.1 | 262. |

| | | | | |
|---|---|---|---|---|
| 11 | .400 | 172. | 8.2 | 278. |
| 12 | .390 | 168. | 8.2 | 261. |
| 13 | .360 | 155. | 8.2 | 253. |
| 14 | .340 | 146. | 8.4 | 234. |
| 15 | .330 | 142. | 8.9 | 209. |
| 16 | .320 | 137. | 9.4 | 181. |
| 17 | .230 | 99. | 9.0 | 171. |
| 18 | .240 | 103. | 9.8 | 162. |
| 19 | .270 | 116. | 8.6 | 217. |
| 20 | .310 | 133. | 8.1 | 255. |
| 21 | .280 | 120. | 8.7 | 221. |
| 22 | .270 | 116. | 8.8 | 194. |
| 23 | .280 | 120. | 9.8 | 152. |
| 24 | .280 | 120. | 9.8 | 149. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 10.1 | 136. |
| 2 | .370 | 159. | 11.1 | 124. |
| 3 | .340 | 146. | 11.0 | 123. |
| 4 | .350 | 150. | 11.0 | 124. |
| 5 | .350 | 150. | 11.1 | 124. |
| 6 | .310 | 133. | 10.6 | 133. |
| 7 | .260 | 112. | 9.3 | 188. |
| 8 | .350 | 150. | 8.6 | 251. |
| 9 | .370 | 159. | 9.0 | 238. |
| 10 | .400 | 172. | 8.6 | 253. |
| 11 | .390 | 168. | 8.5 | 253. |
| 12 | .370 | 159. | 8.4 | 251. |
| 13 | .360 | 155. | 8.9 | 219. |
| 14 | .360 | 155. | 9.5 | 201. |
| 15 | .360 | 155. | 10.2 | 191. |
| 16 | .310 | 133. | 10.1 | 167. |
| 17 | .290 | 125. | 9.5 | 163. |
| 18 | .290 | 125. | 9.0 | 177. |
| 19 | .320 | 137. | 8.1 | 232. |
| 20 | .360 | 155. | 8.1 | 264. |
| 21 | .350 | 150. | 8.2 | 248. |
| 22 | .340 | 146. | 8.2 | 241. |
| 23 | .330 | 142. | 8.8 | 195. |
| 24 | .310 | 133. | 9.9 | 149. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 11.3 | 129. |
| 2 | .400 | 172. | 11.1 | 124. |
| 3 | .410 | 176. | 11.1 | 124. |
| 4 | .400 | 172. | 11.2 | 124. |
| 5 | .400 | 172. | 11.3 | 124. |
| 6 | .380 | 163. | 11.1 | 125. |
| 7 | .330 | 142. | 9.8 | 179. |
| 8 | .370 | 159. | 8.7 | 245. |
| 9 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | .360 | 155. | 8.7 | 211. |
| 15 | .460 | 198. | 8.6 | 230. |
| 16 | .420 | 180. | 8.6 | 218. |
| 17 | .400 | 172. | 8.4 | 219. |
| 18 | .400 | 172. | 8.3 | 224. |
| 19 | .520 | 223. | 7.6 | 282. |
| 20 | .630 | 271. | 7.6 | 296. |
| 21 | .580 | 249. | 7.8 | 267. |
| 22 | .470 | 202. | 8.0 | 238. |
| 23 | .340 | 146. | 8.8 | 172. |
| 24 | .310 | 133. | 9.8 | 149. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 10.0 | 149. |
| 2 | .380 | 163. | 10.7 | 137. |
| 3 | .530 | 228. | 11.2 | 124. |
| 4 | .490 | 210. | 11.0 | 124. |
| 5 | .470 | 202. | 11.0 | 124. |
| 6 | .340 | 146. | 10.2 | 141. |
| 7 | .340 | 146. | 9.6 | 150. |
| 8 | .380 | 163. | 9.2 | 179. |
| 9 | .390 | 168. | 8.8 | 208. |
| 10 | .530 | 228. | 8.6 | 219. |
| 11 | .560 | 241. | 8.6 | 219. |
| 12 | .560 | 241. | 8.4 | 222. |
| 13 | .590 | 253. | 8.1 | 257. |
| 14 | .690 | 296. | 7.5 | 295. |
| 15 | .690 | 296. | 7.2 | 296. |
| 16 | .740 | 318. | 8.1 | 268. |
| 17 | .590 | 253. | 8.3 | 224. |
| 18 | .550 | 236. | 8.3 | 220. |
| 19 | .680 | 292. | 8.0 | 263. |
| 20 | .780 | 335. | 7.9 | 282. |
| 21 | .760 | 326. | 8.0 | 270. |
| 22 | .660 | 284. | 8.4 | 232. |
| 23 | .550 | 236. | 9.3 | 151. |
| 24 | .550 | 236. | 9.4 | 148. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 9.4 | 149. |
| 2 | .540 | 232. | 9.4 | 149. |
| 3 | .520 | 223. | 9.5 | 148. |
| 4 | .520 | 223. | 9.9 | 149. |
| 5 | .550 | 236. | 9.9 | 149. |
| 6 | .520 | 223. | 9.4 | 170. |
| 7 | .700 | 301. | 8.4 | 245. |
| 8 | .830 | 357. | 8.0 | 298. |

| | | | | |
|---|---|---|---|---|
| 9 | .860 | 369. | 7.9 | 298. |
| 10 | .870 | 374. | 7.3 | 306. |
| 11 | .860 | 369. | 7.3 | 316. |
| 12 | .880 | 378. | 7.2 | 316. |
| 13 | .850 | 365. | 7.3 | 316. |
| 14 | .900 | 387. | 7.6 | 316. |
| 15 | .830 | 357. | 7.5 | 300. |
| 16 | .660 | 284. | 8.0 | 259. |
| 17 | .640 | 275. | 8.3 | 222. |
| 18 | .660 | 284. | 8.4 | 232. |
| 19 | .680 | 292. | 8.1 | 261. |
| 20 | .780 | 335. | 7.9 | 290. |
| 21 | .890 | 382. | 8.0 | 298. |
| 22 | .880 | 378. | 7.9 | 296. |
| 23 | .890 | 382. | 7.9 | 296. |
| 24 | .820 | 352. | 8.3 | 255. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .620 | 266. | 8.8 | 203. |
| 2 | .600 | 258. | 8.6 | 218. |
| 3 | .560 | 241. | 8.8 | 200. |
| 4 | .570 | 245. | 8.9 | 189. |
| 5 | .590 | 253. | 8.9 | 189. |
| 6 | .580 | 249. | 8.9 | 187. |
| 7 | .590 | 253. | 9.0 | 181. |
| 8 | .570 | 245. | 8.9 | 183. |
| 9 | .550 | 236. | 8.9 | 182. |
| 10 | .610 | 262. | 8.5 | 239. |
| 11 | .640 | 275. | 8.1 | 268. |
| 12 | .440 | 189. | 8.5 | 230. |
| 13 | .500 | 215. | 8.5 | 219. |
| 14 | .530 | 228. | 8.5 | 218. |
| 15 | .550 | 236. | 8.7 | 217. |
| 16 | .550 | 236. | 9.1 | 213. |
| 17 | .550 | 236. | 9.2 | 209. |
| 18 | .540 | 232. | 8.3 | 217. |
| 19 | .570 | 245. | 8.4 | 239. |
| 20 | .450 | 193. | 8.8 | 226. |
| 21 | .430 | 185. | 9.0 | 214. |
| 22 | .430 | 185. | 9.3 | 198. |
| 23 | .440 | 189. | 9.1 | 192. |
| 24 | .450 | 193. | 9.6 | 157. |

DAY = 32

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 9.4 | 161. |
| 2 | .390 | 168. | 9.3 | 164. |
| 3 | .360 | 155. | 8.9 | 187. |
| 4 | .420 | 180. | 9.1 | 174. |
| 5 | .410 | 176. | 9.2 | 173. |
| 6 | .410 | 176. | 9.1 | 174. |
| 7 | .400 | 172. | 9.3 | 174. |

| | | | | |
|---|---|---|---|---|
| 8 | .410 | 176. | 9.6 | 173. |
| 9 | .360 | 155. | 9.6 | 174. |
| 10 | .380 | 163. | 9.2 | 174. |
| 11 | .380 | 163. | 9.2 | 169. |
| 12 | .400 | 172. | 9.7 | 149. |
| 13 | .510 | 219. | 9.8 | 148. |
| 14 | .390 | 168. | 9.2 | 147. |
| 15 | .430 | 185. | 9.3 | 147. |
| 16 | .430 | 185. | 10.1 | 155. |
| 17 | .430 | 185. | 9.9 | 163. |
| 18 | .410 | 176. | 9.8 | 169. |
| 19 | .390 | 168. | 9.1 | 188. |
| 20 | .400 | 172. | 8.9 | 194. |
| 21 | .390 | 168. | 8.9 | 190. |
| 22 | .390 | 168. | 9.1 | 179. |
| 23 | .390 | 168. | 9.0 | 184. |
| 24 | .390 | 168. | 9.0 | 180. |

DAY = 33

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 9.0 | 182. |
| 2 | .380 | 163. | 9.3 | 171. |
| 3 | .420 | 180. | 9.3 | 169. |
| 4 | .430 | 185. | 9.3 | 169. |
| 5 | .380 | 163. | 9.2 | 179. |
| 6 | .410 | 176. | 9.0 | 196. |
| 7 | .430 | 185. | 8.6 | 211. |
| 8 | .460 | 198. | 8.8 | 223. |
| 9 | .510 | 219. | 8.7 | 223. |
| 10 | .550 | 236. | 8.6 | 223. |
| 11 | .510 | 219. | 8.5 | 223. |
| 12 | .520 | 223. | 8.3 | 223. |
| 13 | .540 | 232. | 8.4 | 223. |
| 14 | .550 | 236. | 8.4 | 223. |
| 15 | .500 | 215. | 8.6 | 219. |
| 16 | .470 | 202. | 8.8 | 204. |
| 17 | .490 | 210. | 10.2 | 200. |
| 18 | .440 | 189. | 9.7 | 198. |
| 19 | .410 | 176. | 9.1 | 212. |
| 20 | .410 | 176. | 9.1 | 214. |
| 21 | .380 | 163. | 9.1 | 207. |
| 22 | .380 | 163. | 9.2 | 203. |
| 23 | .440 | 189. | 9.2 | 209. |
| 24 | .400 | 172. | 10.9 | 163. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 10.6 | 163. |
| 2 | .380 | 163. | 10.0 | 198. |
| 3 | .360 | 155. | 9.8 | 202. |
| 4 | .500 | 215. | 9.3 | 216. |
| 5 | .550 | 236. | 9.3 | 218. |
| 6 | .560 | 241. | 9.4 | 218. |

| | | | | |
|---|---|---|---|---|
| 7 | .570 | 245. | 9.3 | 223. |
| 8 | .560 | 241. | 9.0 | 240. |
| 9 | .680 | 292. | 8.8 | 261. |
| 10 | .800 | 344. | 8.9 | 261. |
| 11 | .840 | 361. | 9.0 | 277. |
| 12 | .720 | 309. | 9.5 | 257. |
| 13 | .660 | 284. | 9.3 | 246. |
| 14 | .570 | 245. | 9.4 | 226. |
| 15 | .580 | 249. | 9.2 | 236. |
| 16 | .560 | 241. | 9.3 | 237. |
| 17 | .560 | 241. | 9.7 | 234. |
| 18 | .560 | 241. | 9.9 | 224. |
| 19 | .520 | 223. | 9.9 | 223. |
| 20 | .420 | 180. | 9.9 | 213. |
| 21 | .390 | 168. | 9.8 | 212. |
| 22 | .360 | 155. | 9.9 | 212. |
| 23 | .380 | 163. | 10.0 | 207. |
| 24 | .630 | 271. | 12.1 | 159. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 12.1 | 148. |
| 2 | .580 | 249. | 12.2 | 149. |
| 3 | .610 | 262. | 12.3 | 148. |
| 4 | .610 | 262. | 11.9 | 148. |
| 5 | .630 | 271. | 11.9 | 149. |
| 6 | .550 | 236. | 11.0 | 179. |
| 7 | .760 | 326. | 9.8 | 244. |
| 8 | .770 | 331. | 9.6 | 245. |
| 9 | .720 | 309. | 9.8 | 222. |
| 10 | .780 | 335. | 10.6 | 205. |
| 11 | .790 | 339. | 10.6 | 203. |
| 12 | .780 | 335. | 10.6 | 201. |
| 13 | .780 | 335. | 10.6 | 197. |
| 14 | .750 | 322. | 10.6 | 195. |
| 15 | .720 | 309. | 10.1 | 190. |
| 16 | .690 | 296. | 10.2 | 186. |
| 17 | .540 | 232. | 10.2 | 188. |
| 18 | .630 | 271. | 9.7 | 211. |
| 19 | .780 | 335. | 8.6 | 267. |
| 20 | .690 | 296. | 8.4 | 258. |
| 21 | .740 | 318. | 8.5 | 260. |
| 22 | .780 | 335. | 8.5 | 251. |
| 23 | .750 | 322. | 9.5 | 222. |
| 24 | .620 | 266. | 10.4 | 181. |

DAY = 36

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 10.3 | 176. |
| 2 | .640 | 275. | 9.6 | 211. |
| 3 | .680 | 292. | 9.9 | 194. |
| 4 | .520 | 223. | 10.8 | 164. |
| 5 | .540 | 232. | 10.8 | 168. |

| | | | | |
|---|---|---|---|---|
| 6 | .590 | 253. | 10.0 | 198. |
| 7 | .700 | 301. | 9.7 | 224. |
| 8 | .740 | 318. | 8.9 | 266. |
| 9 | .800 | 344. | 7.4 | 298. |
| 10 | .760 | 326. | 9.4 | 264. |
| 11 | .690 | 296. | 9.3 | 248. |
| 12 | .630 | 271. | 9.0 | 246. |
| 13 | .650 | 279. | 9.6 | 242. |
| 14 | .700 | 301. | 10.6 | 238. |
| 15 | .680 | 292. | 10.7 | 217 |
| 16 | .650 | 279. | 11.0 | 20[illegible] |
| 17 | .580 | 249. | 11.4 | 185. |
| 18 | .590 | 253. | 11.5 | 179. |
| 19 | .670 | 288. | 10.5 | 224. |
| 20 | .690 | 296. | 10.0 | 243. |
| 21 | .670 | 288. | 10.2 | 225. |
| 22 | .640 | 275. | 10.7 | 201. |
| 23 | .580 | 249. | 11.2 | 174. |
| 24 | .440 | 189. | 12.6 | 151. |

DAY = 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 13.0 | 138. |
| 2 | .480 | 206. | 12.9 | 146. |
| 3 | .410 | 176. | 12.8 | 152. |
| 4 | .490 | 210. | 12.4 | 162. |
| 5 | .580 | 249. | 12.6 | 162. |
| 6 | .580 | 249. | 12.0 | 187. |
| 7 | .630 | 271. | 11.0 | 200. |
| 8 | .660 | 284. | 11.0 | 211. |
| 9 | .610 | 262. | 10.2 | 239. |
| 10 | .620 | 266. | 9.1 | 258. |
| 11 | .710 | 305. | 8.7 | 258. |
| 12 | .720 | 309. | 8.7 | 257. |
| 13 | .690 | 296. | 8.7 | 240. |
| 14 | .640 | 275. | 8.3 | 228. |
| 15 | .620 | 266. | 8.8 | 213. |
| 16 | .590 | 253. | 9.2 | 193. |
| 17 | .570 | 245. | 9.7 | 178. |
| 18 | .520 | 223. | 10.0 | 171. |
| 19 | .350 | 150. | 10.3 | 149. |
| 20 | .290 | 125. | 10.4 | 147. |
| 21 | .330 | 142. | 10.5 | 147. |
| 22 | .330 | 142. | 10.4 | 147. |
| 23 | .330 | 142. | 10.4 | 147. |
| 24 | .340 | 146. | 10.5 | 147. |

DAY = 38

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 10.6 | 147. |
| 2 | .410 | 176. | 10.7 | 147. |
| 3 | .400 | 172. | 10.5 | 147. |
| 4 | .390 | 168. | 10.5 | 147. |

| | | | | |
|---|---|---|---|---|
| 5 | .400 | 172. | 10.7 | 147. |
| 6 | .380 | 163. | 10.3 | 147. |
| 7 | .360 | 155. | 10.7 | 145. |
| 8 | .350 | 150. | 10.3 | 149. |
| 9 | .380 | 163. | 10.7 | 149. |
| 10 | .420 | 180. | 10.3 | 148. |
| 11 | .430 | 185. | 10.7 | 147. |
| 12 | .430 | 185. | 10.3 | 147. |
| 13 | .410 | 176. | 10.3 | 146. |
| 14 | .350 | 150. | 10.4 | 147. |
| 15 | .370 | 159. | 10.5 | 144. |
| 16 | .380 | 163. | 10.5 | 147. |
| 17 | .390 | 168. | 10.5 | 147. |
| 18 | .370 | 159. | 10.4 | 149. |
| 19 | .360 | 155. | 10.4 | 149. |
| 20 | .420 | 180. | 10.5 | 147. |
| 21 | .450 | 193. | 10.5 | 148. |
| 22 | .450 | 193. | 10.5 | 148. |
| 23 | .460 | 198. | 10.4 | 148. |
| 24 | .420 | 180. | 10.4 | 147. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 10.3 | 159. |
| 2 | .520 | 223. | 9.9 | 179. |
| 3 | .560 | 241. | 9.3 | 209. |
| 4 | .620 | 266. | 9.0 | 224. |
| 5 | -1.000 | -430. | -1.0 | -1. |
| 6 | -1.000 | -430. | -1.0 | -1. |
| 7 | -1.000 | -430. | -1.0 | -1. |
| 8 | .710 | 305. | 8.3 | 284. |
| 9 | .740 | 318. | 8.3 | 302. |
| 10 | .780 | 335. | 8.3 | 302. |
| 11 | .760 | 326. | 8.2 | 301. |
| 12 | .730 | 314. | 8.2 | 302. |
| 13 | .740 | 318. | 8.2 | 301. |
| 14 | .780 | 335. | 8.0 | 303. |
| 15 | .840 | 361. | 8.5 | 291. |
| 16 | .770 | 331. | 8.1 | 286. |
| 17 | .700 | 301. | 8.2 | 276. |
| 18 | .650 | 279. | 8.4 | 251. |
| 19 | .640 | 275. | 8.4 | 252. |
| 20 | .720 | 309. | 8.0 | 284. |
| 21 | .660 | 284. | 8.4 | 253. |
| 22 | .520 | 223. | 9.0 | 204. |
| 23 | .400 | 172. | 9.2 | 174. |
| 24 | .460 | 198. | 9.8 | 157. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 10.3 | 156. |
| 2 | .550 | 236. | 10.1 | 162. |
| 3 | .550 | 236. | 9.6 | 173. |

| | | | | |
|---|---|---|---|---|
| 4 | .520 | 223. | 10.0 | 166. |
| 5 | .530 | 228. | 10.1 | 162. |
| 6 | .520 | 223. | 10.0 | 168. |
| 7 | .540 | 232. | 9.6 | 186. |
| 8 | .560 | 241. | 9.6 | 195. |
| 9 | .530 | 228. | 9.6 | 194. |
| 10 | .470 | 202. | 9.3 | 194. |
| 11 | .480 | 206. | 9.3 | 194. |
| 12 | .490 | 210. | 9.2 | 193. |
| 13 | .510 | 219. | 9.3 | 185. |
| 14 | .490 | 210. | 9.3 | 186. |
| 15 | .500 | 215. | 9.3 | 186. |
| 16 | .540 | 232. | 9.8 | 166. |
| 17 | .510 | 219. | 10.0 | 159. |
| 18 | .470 | 202. | 9.7 | 179. |
| 19 | .490 | 210. | 10.0 | 190. |
| 20 | .490 | 210. | 9.8 | 197. |
| 21 | .500 | 215. | 9.9 | 197. |
| 22 | .500 | 215. | 10.0 | 193. |
| 23 | .520 | 223. | 10.0 | 186. |
| 24 | .510 | 219. | 10.3 | 178. |

DAY = 46

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .530 | 228. | 10.9 | 156. |
| 2 | .520 | 223. | 10.8 | 158. |
| 3 | .490 | 210. | 10.7 | 156. |
| 4 | .500 | 215. | 10.7 | 165. |
| 5 | .520 | 223. | 11.0 | 158. |
| 6 | .510 | 219. | 10.7 | 173. |
| 7 | .490 | 210. | 10.7 | 173. |
| 8 | .490 | 210. | 10.7 | 169. |
| 9 | .500 | 215. | 10.7 | 173. |
| 10 | .500 | 215. | 10.3 | 173. |
| 11 | .510 | 219. | 10.3 | 173. |
| 12 | .500 | 215. | 10.3 | 164. |
| 13 | .490 | 210. | 10.8 | 158. |
| 14 | .510 | 219. | 11.2 | 159. |
| 15 | .540 | 232. | 11.3 | 155. |
| 16 | .540 | 232. | 11.3 | 152. |
| 17 | .510 | 219. | 11.2 | 158. |
| 18 | .500 | 215. | 10.7 | 175. |
| 19 | .490 | 210. | 10.2 | 198. |
| 20 | .640 | 275. | 9.3 | 252. |
| 21 | .580 | 249. | 9.4 | 231. |
| 22 | .550 | 236. | 9.7 | 212. |
| 23 | .430 | 185. | 10.5 | 168. |
| 24 | .480 | 206. | 10.5 | 151. |

DAY = 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .490 | 210. | 10.8 | 148. |
| 2 | .480 | 206. | 10.6 | 149. |

| | | | | |
|---|---|---|---|---|
| 3 | .480 | 206. | 10.6 | 148. |
| 4 | .480 | 206. | 10.6 | 149. |
| 5 | .490 | 210. | 10.7 | 149. |
| 6 | .500 | 215. | 10.6 | 148. |
| 7 | .480 | 206. | 10.6 | 154. |
| 8 | .460 | 198. | 10.3 | 160. |
| 9 | .490 | 210. | 10.0 | 194. |
| 10 | .550 | 236. | 9.4 | 225. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .430 | 185. | 9.9 | 170. |
| 16 | .450 | 193. | 9.5 | 168. |
| 17 | .440 | 189. | 9.3 | 169. |
| 18 | .420 | 180. | 9.3 | 168. |
| 19 | .410 | 176. | 9.3 | 170. |
| 20 | .400 | 172. | 9.0 | 197. |
| 21 | .390 | 168. | 9.1 | 191. |
| 22 | .390 | 168. | 9.2 | 187. |
| 23 | .460 | 198. | 9.8 | 157. |
| 24 | .450 | 193. | 10.1 | 144. |

DAY = 48

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 10.0 | 147. |
| 2 | .450 | 193. | 9.9 | 150. |
| 3 | .460 | 198. | 9.9 | 149. |
| 4 | .450 | 193. | 9.8 | 149. |
| 5 | .460 | 198. | 9.9 | 151. |
| 6 | .450 | 193. | 9.9 | 149. |
| 7 | .440 | 189. | 9.7 | 165. |
| 8 | .430 | 185. | 9.5 | 169. |
| 9 | .460 | 198. | 9.6 | 163. |
| 10 | .450 | 193. | 9.6 | 164. |
| 11 | .440 | 189. | 10.2 | 157. |
| 12 | .430 | 185. | 10.1 | 158. |
| 13 | .380 | 163. | 10.2 | 148. |
| 14 | .330 | 142. | 10.2 | 149. |
| 15 | .330 | 142. | 10.3 | 148. |
| 16 | .300 | 129. | 10.3 | 149. |
| 17 | .310 | 133. | 10.2 | 150. |
| 18 | .310 | 133. | 10.2 | 149. |
| 19 | .300 | 129. | 10.1 | 154. |
| 20 | .290 | 125. | 10.2 | 154. |
| 21 | .280 | 120. | 10.2 | 151. |
| 22 | .290 | 125. | 10.2 | 148. |
| 23 | .290 | 125. | 10.2 | 149. |
| 24 | .320 | 137. | 10.2 | 149. |

DAY = 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 10.4 | 148. |

| | | | | |
|---|---|---|---|---|
| 2 | .340 | 146. | 10.3 | 149. |
| 3 | .350 | 150. | 10.3 | 148. |
| 4 | .350 | 150. | 10.3 | 148. |
| 5 | .350 | 150. | 10.3 | 152. |
| 6 | .410 | 176. | 9.7 | 177. |
| 7 | .500 | 215. | 8.4 | 236. |
| 8 | .610 | 262. | 7.7 | 283. |
| 9 | .570 | 245. | 7.9 | 266. |
| 10 | .450 | 193. | 8.9 | 199. |
| 11 | .470 | 202. | 8.9 | 199. |
| 12 | .460 | 198. | 8.9 | 199. |
| 13 | .470 | 202. | 8.9 | 198. |
| 14 | .480 | 206. | 8.6 | 199. |
| 15 | .440 | 189. | 8.4 | 198. |
| 16 | .440 | 189. | 8.6 | 197. |
| 17 | .410 | 176. | 9.2 | 188. |
| 18 | .410 | 176. | 9.2 | 189. |
| 19 | .420 | 180. | 9.2 | 195. |
| 20 | .430 | 185. | 8.9 | 209. |
| 21 | .450 | 193. | 8.8 | 209. |
| 22 | .450 | 193. | 8.8 | 207. |
| 23 | .470 | 202. | 9.2 | 191. |
| 24 | .460 | 198. | 10.0 | 154. |

DAY = 50

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.1 | 151. |
| 2 | .430 | 185. | 10.0 | 149. |
| 3 | .330 | 142. | 10.1 | 149. |
| 4 | .320 | 137. | 10.2 | 149. |
| 5 | .320 | 137. | 10.2 | 149. |
| 6 | .340 | 146. | 10.2 | 149. |
| 7 | .330 | 142. | 10.2 | 149. |
| 8 | .380 | 163. | 9.8 | 170. |
| 9 | .450 | 193. | 9.3 | 198. |
| 10 | .530 | 228. | 9.1 | 205. |
| 11 | .530 | 228. | 8.8 | 223. |
| 12 | .510 | 219. | 8.8 | 224. |
| 13 | .500 | 215. | 8.7 | 224. |
| 14 | .490 | 210. | 8.5 | 223. |
| 15 | .500 | 215. | 8.5 | 223. |
| 16 | .490 | 210. | 8.5 | 223. |
| 17 | .510 | 219. | 8.5 | 223. |
| 18 | .510 | 219. | 8.4 | 224. |
| 19 | .500 | 215. | 8.4 | 225. |
| 20 | .510 | 219. | 8.4 | 224. |
| 21 | .500 | 215. | 8.4 | 220. |
| 22 | .480 | 206. | 8.5 | 221. |
| 23 | .350 | 150. | 9.1 | 181. |
| 24 | .340 | 146. | 9.8 | 153. |

DAY = 51

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .340 | 146. | 10.0 | 148. |
| 2 | .330 | 142. | 10.0 | 148. |
| 3 | .360 | 155. | 10.0 | 149. |
| 4 | -1.000 | -430. | -1.0 | -1. |
| 5 | .420 | 180. | 10.2 | 77. |
| 6 | .430 | 185. | 10.1 | 148. |
| 7 | .420 | 180. | 10.1 | 151. |
| 8 | .410 | 176. | 9.7 | 170. |
| 9 | .430 | 185. | 9.3 | 179. |
| 10 | .430 | 185. | 9.3 | 176. |
| 11 | .420 | 180. | 9.0 | 191. |
| 12 | .520 | 223. | 8.9 | 215. |
| 13 | .500 | 215. | 8.5 | 223. |
| 14 | .490 | 210. | 8.4 | 224. |
| 15 | .490 | 210. | 8.4 | 224. |
| 16 | .470 | 202. | 8.4 | 223. |
| 17 | .470 | 202. | 8.5 | 218. |
| 18 | .480 | 206. | 8.4 | 220. |
| 19 | .470 | 202. | 8.5 | 214. |
| 20 | .460 | 198. | 8.5 | 211. |
| 21 | .440 | 189. | 8.5 | 203. |
| 22 | .500 | 215. | 8.4 | 209. |
| 23 | .430 | 185. | 9.5 | 185. |
| 24 | .310 | 133. | 9.7 | 150. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 10.1 | 149. |
| 2 | .340 | 146. | 10.0 | 148. |
| 3 | .340 | 146. | 10.2 | 148. |
| 4 | .350 | 150. | 10.2 | 148. |
| 5 | .350 | 150. | 10.3 | 149. |
| 6 | .380 | 163. | 10.3 | 148. |
| 7 | .380 | 163. | 10.4 | 148. |
| 8 | .460 | 198. | 10.2 | 156. |
| 9 | .460 | 198. | 9.7 | 177. |
| 10 | .520 | 223. | 9.1 | 215. |
| 11 | .560 | 241. | 8.9 | 223. |
| 12 | .550 | 236. | 8.8 | 223. |
| 13 | .550 | 236. | 8.8 | 223. |
| 14 | .440 | 189. | 8.9 | 204. |
| 15 | .410 | 176. | 9.1 | 198. |
| 16 | .410 | 176. | 9.3 | 189. |
| 17 | .420 | 180. | 9.5 | 174. |
| 18 | .410 | 176. | 9.4 | 177. |
| 19 | .400 | 172. | 9.2 | 193. |
| 20 | .410 | 176. | 9.1 | 202. |
| 21 | .410 | 176. | 9.3 | 186. |
| 22 | .430 | 185. | 9.4 | 171. |
| 23 | .430 | 185. | 9.3 | 169. |
| 24 | .450 | 193. | 9.7 | 157. |

DAY = 53

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| HOUR | | | | |
|---|---|---|---|---|
| 1 | .350 | 150. | 10.4 | 148. |
| 2 | .330 | 142. | 10.2 | 148. |
| 3 | .340 | 146. | 10.2 | 148. |
| 4 | .330 | 142. | 10.2 | 149. |
| 5 | .320 | 137. | 10.3 | 149. |
| 6 | .310 | 133. | 10.3 | 149. |
| 7 | .320 | 137. | 10.3 | 149. |
| 8 | .320 | 137. | 10.3 | 150. |
| 9 | .350 | 150. | 10.3 | 152. |
| 10 | .360 | 155. | 10.3 | 149. |
| 11 | .350 | 150. | 10.3 | 147. |
| 12 | .340 | 146. | 10.2 | 149. |
| 13 | .320 | 137. | 10.1 | 149. |
| 14 | .320 | 137. | 10.1 | 148. |
| 15 | .330 | 142. | 10.1 | 149. |
| 16 | .340 | 146. | 10.0 | 148. |
| 17 | .330 | 142. | 10.1 | 150. |
| 18 | .330 | 142. | 9.8 | 158. |
| 19 | .320 | 137. | 9.8 | 160. |
| 20 | .320 | 137. | 9.8 | 161. |
| 21 | .340 | 146. | 9.8 | 159. |
| 22 | .330 | 142. | 9.8 | 158. |
| 23 | .350 | 150. | 9.7 | 152. |
| 24 | .330 | 142. | 9.9 | 148. |

DAY = 54

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 9.9 | 149. |
| 2 | .320 | 137. | 9.8 | 148. |
| 3 | .320 | 137. | 9.7 | 150. |
| 4 | .330 | 142. | 9.7 | 149. |
| 5 | .320 | 137. | 9.8 | 149. |
| 6 | .330 | 142. | 9.9 | 148. |
| 7 | .360 | 155. | 9.8 | 155. |
| 8 | .410 | 176. | 9.2 | 191. |
| 9 | .420 | 180. | 9.1 | 200. |
| 10 | .490 | 210. | 8.9 | 214. |
| 11 | .520 | 223. | 8.6 | 225. |
| 12 | .500 | 215. | 8.6 | 224. |
| 13 | .500 | 215. | 8.6 | 212. |
| 14 | .450 | 193. | 8.7 | 199. |
| 15 | .450 | 193. | 8.7 | 199. |
| 16 | .440 | 189. | 8.7 | 199. |
| 17 | .430 | 185. | 8.8 | 196. |
| 18 | .420 | 180. | 9.1 | 182. |
| 19 | .400 | 172. | 9.4 | 181. |
| 20 | .410 | 176. | 9.1 | 203. |
| 21 | .420 | 180. | 9.0 | 200. |
| 22 | .450 | 193. | 9.0 | 203. |
| 23 | .460 | 198. | 9.3 | 191. |
| 24 | .320 | 137. | 9.9 | 147. |

DAY = 55

| NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 9.9 | 148. |
| 2 | .300 | 129. | 9.9 | 149. |
| 3 | .310 | 133. | 10.0 | 149. |
| 4 | .310 | 133. | 10.0 | 149. |
| 5 | .310 | 133. | 10.0 | 150. |
| 6 | .320 | 137. | 10.1 | 148. |
| 7 | .310 | 133. | 10.1 | 150. |
| 8 | .370 | 159. | 9.7 | 167. |
| 9 | .410 | 176. | 8.9 | 197. |
| 10 | .440 | 189. | 8.6 | 224. |
| 11 | .440 | 189. | 8.5 | 224. |
| 12 | .420 | 180. | 8.1 | 224. |
| 13 | .400 | 172. | 8.0 | 222. |
| 14 | .390 | 168. | 7.9 | 225. |
| 15 | .400 | 172. | 8.0 | 222. |
| 16 | .280 | 120. | 8.5 | 203. |
| 17 | .300 | 129. | 8.8 | 199. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | .320 | 137. | 8.8 | 60. |
| 20 | .280 | 120. | 8.6 | 206. |
| 21 | .320 | 137. | 9.2 | 172. |
| 22 | .260 | 112. | 9.6 | 157. |
| 23 | .270 | 116. | 9.7 | 157. |
| 24 | .280 | 120. | 10.0 | 149. |

DAY = 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 10.1 | 148. |
| 2 | .320 | 137. | 9.5 | 175. |
| 3 | .340 | 146. | 9.5 | 173. |
| 4 | .360 | 155. | 9.6 | 170. |
| 5 | .340 | 146. | 9.4 | 179. |
| 6 | .390 | 168. | 8.9 | 210. |
| 7 | .640 | 275. | 7.8 | 298. |
| 8 | .710 | 305. | 7.4 | 328. |
| 9 | .670 | 288. | 7.4 | 321. |
| 10 | .620 | 266. | 7.3 | 322. |
| 11 | .620 | 266. | 7.1 | 321. |
| 12 | .620 | 266. | 7.1 | 321. |
| 13 | .620 | 266. | 6.9 | 321. |
| 14 | .620 | 266. | 6.9 | 322. |
| 15 | .650 | 279. | 7.0 | 321. |
| 16 | .660 | 284. | 7.0 | 321. |
| 17 | .650 | 279. | 6.9 | 321. |
| 18 | .570 | 245. | 7.1 | 299. |
| 19 | .550 | 236. | 7.0 | 300. |
| 20 | .590 | 253. | 7.0 | 302. |
| 21 | .560 | 241. | 7.2 | 281. |
| 22 | .570 | 245. | 7.2 | 283. |
| 23 | .530 | 228. | 7.9 | 241. |
| 24 | .390 | 168. | 8.8 | 176. |

DAY = 57

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 9.8 | 148. |
| 2 | .270 | 116. | 9.8 | 149. |
| 3 | .240 | 103. | 9.8 | 149. |
| 4 | .250 | 107. | 9.9 | 149. |
| 5 | .280 | 120. | 9.9 | 149. |
| 6 | .280 | 120. | 9.9 | 149. |
| 7 | .270 | 116. | 9.9 | 150. |
| 8 | .250 | 107. | 9.9 | 149. |
| 9 | .280 | 120. | 9.9 | 149. |
| 10 | .290 | 125. | 9.8 | 150. |
| 11 | .350 | 150. | 9.4 | 169. |
| 12 | .390 | 168. | 8.9 | 199. |
| 13 | .380 | 163. | 9.1 | 180. |
| 14 | .390 | 168. | 9.1 | 176. |
| 15 | .380 | 163. | 9.2 | 174. |
| 16 | .360 | 155. | 8.8 | 194. |
| 17 | .340 | 146. | 8.7 | 204. |
| 18 | .350 | 150. | 8.4 | 214. |
| 19 | .370 | 159. | 8.2 | 232. |
| 20 | .520 | 223. | 7.3 | 303. |
| 21 | .630 | 271. | 6.9 | 327. |
| 22 | .620 | 266. | 7.0 | 318. |
| 23 | .450 | 193. | 7.9 | 245. |
| 24 | .300 | 129. | 9.5 | 159. |

DAY # 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 9.7 | 159. |
| 2 | .260 | 112. | 9.6 | 159. |
| 3 | .260 | 112. | 9.7 | 159. |
| 4 | .270 | 116. | 9.7 | 159. |
| 5 | .250 | 107. | 9.8 | 159. |
| 6 | .310 | 133. | 9.3 | 175. |
| 7 | .320 | 137. | 8.7 | 198. |
| 8 | .490 | 210. | 8.3 | 224. |
| 9 | .580 | 249. | 7.9 | 272. |
| 10 | .680 | 292. | 7.8 | 296. |
| 11 | .690 | 296. | 7.3 | 316. |
| 12 | .730 | 314. | 7.2 | 324. |
| 13 | .730 | 314. | 7.1 | 324. |
| 14 | .730 | 314. | 7.1 | 323. |
| 15 | .730 | 314. | 7.1 | 324. |
| 16 | .720 | 309. | 7.1 | 324. |
| 17 | .740 | 318. | 7.1 | 323. |
| 18 | .750 | 322. | 7.1 | 324. |
| 19 | .760 | 326. | 7.2 | 324. |
| 20 | .760 | 326. | 7.2 | 324. |
| 21 | .760 | 326. | 7.2 | 321. |
| 22 | .690 | 296. | 7.2 | 310. |
| 23 | .720 | 309. | 7.2 | 315. |
| 24 | .710 | 305. | 7.3 | 306. |

DAY # 59

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 7.6 | 269. |
| 2 | .400 | 172. | 8.0 | 221. |
| 3 | .350 | 150. | 8.3 | 198. |
| 4 | .350 | 150. | 8.4 | 199. |
| 5 | .360 | 155. | 8.4 | 198. |
| 6 | .370 | 159. | 8.4 | 199. |
| 7 | .380 | 163. | 8.4 | 199. |
| 8 | .510 | 219. | 8.1 | 234. |
| 9 | .550 | 236. | 7.9 | 254. |
| 10 | .640 | 275. | 7.5 | 297. |
| 11 | .630 | 271. | 7.3 | 305. |
| 12 | .720 | 309. | 7.2 | 323. |
| 13 | .700 | 301. | 7.2 | 314. |
| 14 | .620 | 266. | 7.2 | 297. |
| 15 | .550 | 236. | 7.4 | 267. |
| 16 | .530 | 228. | 7.6 | 248. |
| 17 | .530 | 228. | 7.7 | 243. |
| 18 | .550 | 236. | 7.7 | 250. |
| 19 | .580 | 249. | 7.5 | 258. |
| 20 | .580 | 249. | 7.4 | 274. |
| 21 | .620 | 266. | 7.4 | 285. |
| 22 | .700 | 301. | 7.3 | 307. |
| 23 | .770 | 331. | 7.2 | 318. |
| 24 | .670 | 288. | 7.5 | 279. |

DAY = 60

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 8.2 | 218. |
| 2 | .460 | 198. | 8.2 | 218. |
| 3 | .420 | 180. | 8.6 | 194. |
| 4 | .360 | 155. | 8.9 | 168. |
| 5 | .380 | 163. | 8.9 | 169. |
| 6 | .420 | 180. | 9.1 | 168. |
| 7 | .410 | 176. | 9.5 | 169. |
| 8 | .400 | 172. | 9.0 | 190. |
| 9 | .380 | 163. | 8.8 | 199. |
| 10 | .380 | 163. | 8.7 | 198. |
| 11 | .360 | 155. | 8.7 | 199. |
| 12 | .350 | 150. | 8.6 | 205. |
| 13 | .350 | 150. | 8.5 | 209. |
| 14 | .450 | 193. | 8.2 | 238. |
| 15 | .590 | 253. | 7.6 | 297. |
| 16 | .580 | 249. | 7.4 | 298. |
| 17 | .510 | 219. | 7.5 | 283. |
| 18 | .400 | 172. | 7.7 | 254. |
| 19 | .390 | 168. | 7.7 | 248. |
| 20 | .390 | 168. | 7.7 | 248. |
| 21 | .400 | 172. | 7.8 | 248. |
| 22 | .390 | 168. | 7.8 | 246. |
| 23 | .410 | 176. | 7.7 | 256. |
| 24 | .370 | 159. | 8.6 | 194. |

DAY = 61

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 9.2 | 153. |
| 2 | .220 | 95. | 9.3 | 154. |
| 3 | .200 | 86. | 9.3 | 153. |
| 4 | .220 | 95. | 9.4 | 154. |
| 5 | .220 | 95. | 9.4 | 153. |
| 6 | .280 | 120. | 9.0 | 180. |
| 7 | .380 | 163. | 8.4 | 228. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .670 | 288. | 7.4 | 318. |
| 11 | .660 | 284. | 7.5 | 319. |
| 12 | .690 | 296. | 7.4 | 318. |
| 13 | .710 | 305. | 7.3 | 319. |
| 14 | .710 | 305. | 7.3 | 318. |
| 15 | .680 | 292. | 7.2 | 319. |
| 16 | .660 | 284. | 7.2 | 312. |
| 17 | .570 | 245. | 7.4 | 283. |
| 18 | .590 | 253. | 7.3 | 298. |
| 19 | .650 | 279. | 7.3 | 305. |
| 20 | .740 | 318. | 7.1 | 322. |
| 21 | .710 | 305. | 7.2 | 321. |
| 22 | .670 | 288. | 7.3 | 310. |
| 23 | .460 | 198. | 7.7 | 254. |
| 24 | .230 | 99. | 8.0 | 208. |

DAY = 62



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 9.4 | 157. |
| 2 | .220 | 95. | 10.0 | 149. |
| 3 | .230 | 99. | 10.0 | 149. |
| 4 | .250 | 107. | 10.1 | 149. |
| 5 | .250 | 107. | 10.1 | 148. |
| 6 | .330 | 142. | 9.8 | 166. |
| 7 | .490 | 210. | 8.4 | 232. |
| 8 | .660 | 284. | 7.6 | 318. |
| 9 | .710 | 305. | 7.2 | 339. |
| 10 | .670 | 288. | 7.0 | 339. |
| 11 | .670 | 288. | 6.9 | 338. |
| 12 | .680 | 292. | 6.9 | 337. |
| 13 | .670 | 288. | 7.1 | 323. |
| 14 | .670 | 288. | 7.0 | 324. |
| 15 | .690 | 296. | 7.0 | 323. |
| 16 | .660 | 284. | 7.2 | 308. |
| 17 | .630 | 271. | 7.2 | 298. |
| 18 | .630 | 271. | 7.2 | 298. |
| 19 | .630 | 271. | 7.2 | 299. |
| 20 | .640 | 275. | 7.2 | 298. |
| 21 | .640 | 275. | 7.2 | 298. |
| 22 | .590 | 253. | 7.4 | 271. |
| 23 | .370 | 159. | 7.8 | 203. |
| 24 | .330 | 142. | 8.8 | 178. |

DAY = 63

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 8.8 | 149. |
| 2 | .230 | 99. | 8.7 | 149. |
| 3 | .230 | 99. | 8.7 | 148. |
| 4 | .200 | 86. | 8.7 | 149. |
| 5 | .190 | 82. | 8.9 | 149. |
| 6 | .200 | 86. | 8.8 | 148. |
| 7 | .240 | 103. | 8.7 | 159. |
| 8 | .240 | 103. | 8.8 | 189. |
| 9 | .400 | 172. | 8.0 | 280. |
| 10 | .620 | 266. | 7.8 | 298. |
| 11 | .640 | 275. | 7.8 | 297. |
| 12 | .580 | 249. | 8.0 | 264. |
| 13 | .530 | 228. | 7.8 | 248. |
| 14 | .540 | 232. | 7.9 | 248. |
| 15 | .560 | 241. | 7.9 | 249. |
| 16 | .580 | 249. | 8.2 | 248. |
| 17 | .590 | 253. | 8.0 | 249. |
| 18 | .630 | 271. | 7.6 | 271. |
| 19 | .610 | 262. | 7.6 | 273. |
| 20 | .620 | 266. | 7.5 | 273. |
| 21 | .690 | 296. | 7.6 | 273. |
| 22 | .720 | 309. | 7.6 | 273. |
| 23 | .700 | 301. | 7.7 | 272. |
| 24 | .530 | 228. | 8.1 | 206. |

DAY = 64



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 10.5 | 149. |
| 2 | .280 | 120. | 10.3 | 148. |
| 3 | .290 | 125. | 10.4 | 149. |
| 4 | .290 | 125. | 10.4 | 148. |
| 5 | .300 | 129. | 10.3 | 149. |
| 6 | .290 | 125. | 10.4 | 148. |
| 7 | .290 | 125. | 10.4 | 149. |
| 8 | .450 | 193. | 9.2 | 209. |
| 9 | .520 | 223. | 8.0 | 273. |
| 10 | .420 | 180. | 7.9 | 273. |
| 11 | .360 | 155. | 8.0 | 253. |
| 12 | .320 | 137. | 8.0 | 249. |
| 13 | .380 | 163. | 8.3 | 226. |
| 14 | .390 | 168. | 8.4 | 219. |
| 15 | .270 | 116. | 8.4 | 219. |
| 16 | .250 | 107. | 8.3 | 219. |
| 17 | .290 | 125. | 8.4 | 219. |
| 18 | .260 | 112. | 8.3 | 219. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .320 | 137. | 7.7 | 270. |
| 21 | .300 | 129. | 7.6 | 273. |
| 22 | .330 | 142. | 7.8 | 255. |
| 23 | .300 | 129. | 8.1 | 249. |
| 24 | .360 | 155. | 8.4 | 232. |

DAY = 65

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 9.0 | 177. |
| 2 | .350 | 150. | 9.2 | 169. |
| 3 | .330 | 142. | 9.4 | 160. |
| 4 | .360 | 155. | 9.4 | 159. |
| 5 | .360 | 155. | 9.4 | 159. |
| 6 | .370 | 159. | 9.0 | 187. |
| 7 | .400 | 172. | 8.8 | 209. |
| 8 | .500 | 215. | 8.6 | 209. |
| 9 | .450 | 193. | 8.3 | 253. |
| 10 | .500 | 215. | 7.3 | 322. |
| 11 | .840 | 361. | 7.4 | 324. |
| 12 | .570 | 245. | 7.3 | 323. |
| 13 | .480 | 206. | 7.4 | 302. |
| 14 | .430 | 185. | 7.3 | 273. |
| 15 | .440 | 189. | 7.3 | 274. |
| 16 | .430 | 185. | 7.3 | 274. |
| 17 | .440 | 189. | 7.3 | 273. |
| 18 | .430 | 185. | 7.3 | 273. |
| 19 | .430 | 185. | 7.5 | 274. |
| 20 | .430 | 185. | 7.5 | 273. |
| 21 | .440 | 189. | 7.5 | 274. |
| 22 | .420 | 180. | 7.6 | 255. |
| 23 | .400 | 172. | 8.0 | 241. |
| 24 | .390 | 168. | 8.4 | 215. |

DAY = 66



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 9.0 | 171. |
| 2 | .280 | 120. | 9.8 | 150. |
| 3 | .240 | 103. | 10.1 | 149. |
| 4 | .230 | 99. | 10.1 | 149. |
| 5 | .240 | 103. | 10.1 | 148. |
| 6 | .250 | 107. | 10.1 | 155. |
| 7 | .300 | 129. | 9.4 | 187. |
| 8 | .310 | 133. | 9.3 | 192. |
| 9 | .300 | 129. | 9.4 | 192. |
| 10 | .360 | 155. | 8.9 | 218. |
| 11 | .410 | 176. | 8.4 | 243. |
| 12 | .380 | 163. | 8.8 | 224. |
| 13 | .390 | 168. | 8.9 | 213. |
| 14 | .290 | 125. | 9.5 | 174. |
| 15 | .300 | 129. | 9.6 | 174. |
| 16 | .300 | 129. | 9.8 | 193. |
| 17 | .310 | 133. | 9.2 | 198. |
| 18 | .370 | 159. | 8.9 | 218. |
| 19 | .400 | 172. | 8.9 | 223. |
| 20 | .400 | 172. | 9.0 | 224. |
| 21 | .330 | 142. | 9.2 | 203. |
| 22 | .330 | 142. | 8.9 | 198. |
| 23 | .330 | 142. | 9.0 | 199. |
| 24 | .330 | 142. | 9.1 | 187. |

DAY = 67

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 9.4 | 206. |
| 2 | .360 | 155. | 9.8 | 174. |
| 3 | .360 | 155. | 9.9 | 174. |
| 4 | .360 | 155. | 9.8 | 173. |
| 5 | .360 | 155. | 9.9 | 174. |
| 6 | .370 | 159. | 9.9 | 174. |
| 7 | .360 | 155. | 9.9 | 173. |
| 8 | .370 | 159. | 9.9 | 174. |
| 9 | .370 | 159. | 9.9 | 173. |
| 10 | .380 | 163. | 9.8 | 174. |
| 11 | .370 | 159. | 9.7 | 174. |
| 12 | .360 | 155. | 9.3 | 173. |
| 13 | .360 | 155. | 9.3 | 174. |
| 14 | .350 | 150. | 9.5 | 173. |
| 15 | .340 | 146. | 9.5 | 173. |
| 16 | .320 | 137. | 9.4 | 174. |
| 17 | .310 | 133. | 9.5 | 173. |
| 18 | .310 | 133. | 9.4 | 174. |
| 19 | .320 | 137. | 9.5 | 173. |
| 20 | .380 | 163. | 8.7 | 224. |
| 21 | .420 | 180. | 8.4 | 249. |
| 22 | .400 | 172. | 8.5 | 230. |
| 23 | .320 | 137. | 8.8 | 208. |
| 24 | .310 | 133. | 9.1 | 187. |

DAY = 68



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 9.5 | 168. |
| 2 | .360 | 155. | 10.0 | 158. |
| 3 | .350 | 150. | 10.1 | 158. |
| 4 | .360 | 155. | 10.2 | 158. |
| 5 | .360 | 155. | 10.1 | 158. |
| 6 | .360 | 155. | 9.5 | 180. |
| 7 | .370 | 159. | 8.7 | 234. |
| 8 | .350 | 150. | 8.1 | 293. |
| 9 | .530 | 228. | 7.5 | 335. |
| 10 | .580 | 249. | 7.3 | 323. |
| 11 | .580 | 249. | 7.2 | 324. |
| 12 | .560 | 241. | 7.2 | 311. |
| 13 | .530 | 228. | 7.2 | 299. |
| 14 | .520 | 223. | 7.2 | 287. |
| 15 | .510 | 219. | 7.4 | 274. |
| 16 | .510 | 219. | 7.4 | 273. |
| 17 | .500 | 215. | 7.3 | 274. |
| 18 | .540 | 232. | 7.3 | 274. |
| 19 | .520 | 223. | 7.5 | 273. |
| 20 | .530 | 228. | 7.5 | 274. |
| 21 | .530 | 228. | 7.5 | 274. |
| 22 | .540 | 232. | 7.5 | 273. |
| 23 | .540 | 232. | 7.5 | 277. |
| 24 | .500 | 215. | 7.8 | 251. |

DAY = 69

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 8.2 | 243. |
| 2 | .460 | 198. | 8.3 | 226. |
| 3 | .370 | 159. | 8.3 | 194. |
| 4 | .370 | 159. | 8.8 | 194. |
| 5 | .370 | 159. | 8.7 | 194. |
| 6 | .460 | 198. | 8.5 | 222. |
| 7 | .580 | 249. | 7.9 | 280. |
| 8 | .640 | 275. | 7.8 | 313. |
| 9 | .630 | 271. | 7.4 | 323. |
| 10 | .620 | 266. | 7.3 | 324. |
| 11 | .620 | 266. | 7.2 | 324. |
| 12 | .630 | 271. | 7.2 | 323. |
| 13 | .650 | 279. | 7.2 | 324. |
| 14 | .700 | 301. | 7.1 | 335. |
| 15 | .710 | 305. | 7.1 | 336. |
| 16 | .730 | 314. | 7.0 | 335. |
| 17 | .760 | 326. | 7.1 | 335. |
| 18 | .770 | 331. | 7.1 | 336. |
| 19 | .740 | 318. | 7.1 | 336. |
| 20 | .710 | 305. | 7.0 | 335. |
| 21 | .730 | 314. | 7.1 | 335. |
| 22 | .680 | 292. | 7.2 | 315. |
| 23 | .600 | 258. | 7.8 | 281. |
| 24 | .430 | 185. | 8.1 | 209. |

DAY = 70



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .200 | 86. | 8.8 | 154. |
| 2 | .190 | 82. | 9.7 | 155. |
| 3 | .310 | 133. | 9.3 | 178. |
| 4 | .420 | 180. | 8.7 | 217. |
| 5 | .470 | 202. | 8.5 | 230. |
| 6 | .490 | 210. | 8.3 | 248. |
| 7 | .540 | 232. | 7.9 | 276. |
| 8 | .610 | 262. | 7.5 | 311. |
| 9 | .640 | 275. | 7.3 | 324. |
| 10 | .660 | 284. | 7.2 | 323. |
| 11 | .670 | 288. | 7.2 | 324. |
| 12 | .660 | 284. | 7.2 | 323. |
| 13 | .650 | 279. | 7.1 | 324. |
| 14 | .690 | 296. | 7.1 | 323. |
| 15 | .650 | 279. | 7.1 | 315. |
| 16 | .680 | 292. | 7.1 | 321. |
| 17 | .700 | 301. | 7.2 | 322. |
| 18 | .700 | 301. | 7.1 | 322. |
| 19 | .670 | 288. | 7.1 | 315. |
| 20 | .690 | 296. | 7.1 | 318. |
| 21 | .700 | 301. | 7.1 | 320. |
| 22 | .700 | 301. | 7.1 | 318. |
| 23 | .700 | 301. | 7.2 | 308. |
| 24 | .470 | 202. | 7.3 | 230. |

DAY = 71

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 9.1 | 149. |
| 2 | .200 | 86. | 9.0 | 149. |
| 3 | .200 | 86. | 9.6 | 149. |
| 4 | .220 | 95. | 9.7 | 151. |
| 5 | .240 | 103. | 9.2 | 177. |
| 6 | .410 | 176. | 8.3 | 245. |
| 7 | .640 | 275. | 7.5 | 319. |
| 8 | .680 | 292. | 7.3 | 333. |
| 9 | .670 | 288. | 7.4 | 333. |
| 10 | .680 | 292. | 7.3 | 334. |
| 11 | .650 | 279. | 7.2 | 320. |
| 12 | .480 | 206. | 7.3 | 290. |
| 13 | .510 | 219. | 7.4 | 282. |
| 14 | .490 | 210. | 7.4 | 271. |
| 15 | .470 | 202. | 7.4 | 268. |
| 16 | .490 | 210. | 7.5 | 266. |
| 17 | .480 | 206. | 7.6 | 250. |
| 18 | .480 | 206. | 7.5 | 249. |
| 19 | .480 | 206. | 7.5 | 249. |
| 20 | .460 | 198. | 7.5 | 256. |
| 21 | .450 | 193. | 7.5 | 252. |
| 22 | .440 | 189. | 8.9 | 171. |
| 23 | .310 | 133. | 9.2 | 152. |
| 24 | .380 | 163. | 9.3 | 164. |

DAY = 72



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 8.5 | 208. |
| 2 | .390 | 168. | 8.5 | 197. |
| 3 | .370 | 159. | 8.7 | 185. |
| 4 | .380 | 163. | 8.9 | 176. |
| 5 | .380 | 163. | 9.2 | 175. |
| 6 | .380 | 163. | 9.2 | 179. |
| 7 | .490 | 210. | 8.6 | 229. |
| 8 | .550 | 236. | 8.2 | 265. |
| 9 | .550 | 236. | 8.0 | 289. |
| 10 | .560 | 241. | 7.9 | 294. |
| 11 | .560 | 241. | 7.8 | 292. |
| 12 | .570 | 245. | 7.7 | 294. |
| 13 | .560 | 241. | 7.7 | 284. |
| 14 | .540 | 232. | 7.6 | 283. |
| 15 | .540 | 232. | 7.6 | 283. |
| 16 | .520 | 223. | 7.4 | 273. |
| 17 | .530 | 228. | 7.4 | 273. |
| 18 | .530 | 228. | 7.3 | 274. |
| 19 | .540 | 232. | 7.4 | 274. |
| 20 | .550 | 236. | 7.2 | 290. |
| 21 | .560 | 241. | 7.2 | 298. |
| 22 | .560 | 241. | 7.2 | 290. |
| 23 | .550 | 236. | 7.4 | 272. |
| 24 | .600 | 258. | 7.3 | 286. |

DAY = 73

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 7.4 | 283. |
| 2 | .540 | 232. | 7.5 | 258. |
| 3 | .510 | 219. | 8.0 | 232. |
| 4 | .340 | 146. | 9.5 | 159. |
| 5 | .270 | 116. | 9.8 | 149. |
| 6 | .300 | 129. | 9.8 | 157. |
| 7 | .350 | 150. | 9.0 | 186. |
| 8 | .340 | 146. | 8.7 | 202. |
| 9 | .340 | 146. | 8.5 | 227. |
| 10 | .380 | 163. | 7.9 | 275. |
| 11 | .490 | 210. | 7.7 | 298. |
| 12 | .470 | 202. | 7.6 | 297. |
| 13 | .480 | 206. | 7.5 | 297. |
| 14 | .460 | 198. | 7.6 | 280. |
| 15 | .450 | 193. | 7.6 | 275. |
| 16 | .490 | 210. | 7.5 | 290. |
| 17 | .500 | 215. | 7.5 | 289. |
| 18 | .520 | 223. | 7.7 | 288. |
| 19 | .540 | 232. | 7.5 | 292. |
| 20 | .520 | 223. | 7.6 | 297. |
| 21 | .520 | 223. | 7.5 | 294. |
| 22 | .480 | 206. | 7.9 | 258. |
| 23 | .380 | 163. | 8.2 | 203. |
| 24 | .350 | 150. | 9.4 | 155. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 9.8 | 149. |
| 2 | .290 | 125. | 9.8 | 149. |
| 3 | .290 | 125. | 9.8 | 148. |
| 4 | .300 | 129. | 9.8 | 149. |
| 5 | .310 | 133. | 9.7 | 150. |
| 6 | .350 | 150. | 9.5 | 157. |
| 7 | .370 | 159. | 9.5 | 161. |
| 8 | .370 | 159. | 9.6 | 159. |
| 9 | .360 | 155. | 9.2 | 172. |
| 10 | .390 | 168. | 8.7 | 196. |
| 11 | .420 | 180. | 8.7 | 198. |
| 12 | .420 | 180. | 8.5 | 207. |
| 13 | .410 | 176. | 8.3 | 209. |
| 14 | .400 | 172. | 8.3 | 207. |
| 15 | .400 | 172. | 8.3 | 206. |
| 16 | .410 | 176. | 8.5 | 190. |
| 17 | .400 | 172. | 8.7 | 184. |
| 18 | .400 | 172. | 8.6 | 178. |
| 19 | .390 | 168. | 8.6 | 186. |
| 20 | .390 | 168. | 8.5 | 194. |
| 21 | .400 | 172. | 8.8 | 199. |
| 22 | .400 | 172. | 8.9 | 194. |
| 23 | .370 | 159. | 8.9 | 189. |
| 24 | .380 | 163. | 8.9 | 192. |

DAY = 75

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 9.4 | 166. |
| 2 | .380 | 163. | 9.8 | 152. |
| 3 | .370 | 159. | 9.7 | 153. |
| 4 | .370 | 159. | 9.8 | 157. |
| 5 | .370 | 159. | 9.4 | 162. |
| 6 | .370 | 159. | 9.0 | 184. |
| 7 | .490 | 210. | 8.2 | 256. |
| 8 | .550 | 236. | 7.7 | 299. |
| 9 | .570 | 245. | 7.7 | 302. |
| 10 | .580 | 249. | 7.4 | 319. |
| 11 | .550 | 236. | 7.4 | 319. |
| 12 | .540 | 232. | 7.3 | 320. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .590 | 253. | 7.2 | 317. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .680 | 292. | 7.1 | 319. |
| 19 | .570 | 245. | 7.1 | 320. |
| 20 | .590 | 253. | 7.2 | 321. |
| 21 | .590 | 253. | 7.2 | 317. |
| 22 | .590 | 253. | 7.2 | 316. |
| 23 | .500 | 215. | 7.6 | 268. |
| 24 | .360 | 155. | 8.4 | 208. |

DAY = 76



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 9.4 | 169. |
| 2 | .330 | 142. | 8.9 | 180. |
| 3 | .470 | 202. | 8.1 | 242. |
| 4 | .460 | 198. | 8.1 | 239. |
| 5 | .440 | 189. | 8.2 | 234. |
| 6 | .450 | 193. | 8.2 | 234. |
| 7 | .460 | 198. | 8.2 | 236. |
| 8 | .490 | 210. | 8.0 | 256. |
| 9 | .510 | 219. | 7.7 | 295. |
| 10 | .540 | 232. | 7.6 | 296. |
| 11 | .540 | 232. | 7.4 | 298. |
| 12 | .520 | 223. | 7.5 | 298. |
| 13 | .500 | 215. | 7.4 | 295. |
| 14 | .520 | 223. | 7.4 | 298. |
| 15 | .500 | 215. | 7.6 | 285. |
| 16 | .460 | 198. | 7.8 | 260. |
| 17 | .440 | 189. | 8.1 | 227. |
| 18 | .420 | 180. | 8.1 | 228. |
| 19 | .450 | 193. | 8.6 | 229. |
| 20 | .510 | 219. | 7.9 | 266. |
| 21 | .540 | 232. | 7.6 | 288. |
| 22 | .540 | 232. | 7.7 | 286. |
| 23 | .500 | 215. | 8.0 | 257. |
| 24 | .400 | 172. | 8.9 | 206. |

DAY = 77

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 9.8 | 161. |
| 2 | .360 | 155. | 10.2 | 148. |
| 3 | .370 | 159. | 10.2 | 147. |
| 4 | .380 | 163. | 10.3 | 148. |
| 5 | .390 | 168. | 10.2 | 147. |
| 6 | .380 | 163. | 9.5 | 156. |
| 7 | .410 | 176. | 9.4 | 195. |
| 8 | .480 | 206. | 8.7 | 238. |
| 9 | .550 | 236. | 8.4 | 272. |
| 10 | .580 | 249. | 7.8 | 304. |
| 11 | .580 | 249. | 7.6 | 318. |
| 12 | .610 | 262. | 7.5 | 318. |
| 13 | .580 | 249. | 7.4 | 316. |
| 14 | .590 | 253. | 7.3 | 314. |
| 15 | .560 | 241. | 7.4 | 298. |
| 16 | .550 | 236. | 7.4 | 298. |
| 17 | .580 | 249. | 7.3 | 306. |
| 18 | .540 | 232. | 7.3 | 298. |
| 19 | .550 | 236. | 7.2 | 301. |
| 20 | .620 | 266. | 7.1 | 319. |
| 21 | .620 | 266. | 7.0 | 317. |
| 22 | .610 | 262. | 7.1 | 312. |
| 23 | .520 | 223. | 7.3 | 270. |
| 24 | .360 | 155. | 8.0 | 200. |

DAY = 78



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 8.2 | 198. |
| 2 | .330 | 142. | 8.2 | 195. |
| 3 | .330 | 142. | 8.3 | 189. |
| 4 | .340 | 146. | 8.7 | 188. |
| 5 | .340 | 146. | 8.8 | 189. |
| 6 | .340 | 146. | 8.7 | 197. |
| 7 | .550 | 236. | 7.5 | 276. |
| 8 | .550 | 236. | 7.2 | 300. |
| 9 | .570 | 245. | 7.1 | 316. |
| 10 | .580 | 249. | 7.0 | 320. |
| 11 | .600 | 258. | 6.9 | 318. |
| 12 | .590 | 253. | 6.8 | 318. |
| 13 | .600 | 258. | 6.7 | 317. |
| 14 | .590 | 253. | 6.8 | 318. |
| 15 | .580 | 249. | 6.8 | 319. |
| 16 | .580 | 249. | 6.9 | 317. |
| 17 | .620 | 266. | 7.0 | 319. |
| 18 | .640 | 275. | 6.9 | 318. |
| 19 | .640 | 275. | 6.9 | 319. |
| 20 | .650 | 279. | 6.9 | 320. |
| 21 | .650 | 279. | 7.0 | 318. |
| 22 | .660 | 284. | 7.1 | 315. |
| 23 | .520 | 223. | 7.8 | 259. |
| 24 | .390 | 168. | 8.5 | 205. |

DAY = 81

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 9.6 | 153. |
| 2 | .390 | 168. | 9.7 | 150. |
| 3 | .410 | 176. | 9.7 | 148. |
| 4 | .400 | 172. | 9.8 | 146. |
| 5 | .390 | 168. | 9.8 | 147. |
| 6 | .380 | 163. | 9.7 | 149. |
| 7 | .390 | 168. | 9.7 | 149. |
| 8 | .370 | 159. | 9.3 | 178. |
| 9 | .500 | 215. | 8.5 | 238. |
| 10 | .650 | 279. | 7.8 | 293. |
| 11 | .480 | 206. | 9.0 | 201. |
| 12 | .460 | 198. | 8.9 | 199. |
| 13 | .460 | 198. | 8.9 | 202. |
| 14 | .460 | 198. | 9.0 | 181. |
| 15 | .420 | 180. | 9.5 | 156. |
| 16 | .370 | 159. | 9.5 | 148. |
| 17 | .360 | 155. | 9.7 | 149. |
| 18 | .350 | 150. | 9.5 | 155. |
| 19 | .330 | 142. | 9.2 | 174. |
| 20 | .470 | 202. | 8.3 | 247. |
| 21 | .490 | 210. | 8.0 | 260. |
| 22 | .470 | 202. | 8.2 | 238. |
| 23 | .430 | 185. | 8.7 | 190. |
| 24 | .260 | 112. | 9.5 | 149. |

DAY = 84

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | -1.000 | -430. | -1.0 | -1. |
| 4 | -1.000 | -430. | -1.0 | -1. |
| 5 | .290 | 125. | 14.0 | 34. |
| 6 | .430 | 185. | 11.0 | 106. |
| 7 | .320 | 137. | 9.6 | 165. |
| 8 | .360 | 155. | 9.4 | 187. |
| 9 | .530 | 228. | 8.5 | 275. |
| 10 | .560 | 241. | 8.0 | 277. |
| 11 | .570 | 245. | 8.0 | 277. |
| 12 | .590 | 253. | 8.0 | 292. |
| 13 | .590 | 253. | 7.8 | 309. |
| 14 | .590 | 253. | 7.6 | 323. |
| 15 | .570 | 245. | 7.5 | 321. |
| 16 | .540 | 232. | 7.4 | 322. |
| 17 | .530 | 228. | 7.4 | 321. |
| 18 | .550 | 236. | 7.4 | 322. |
| 19 | .600 | 258. | 7.4 | 324. |
| 20 | .640 | 275. | 7.3 | 330. |
| 21 | .610 | 262. | 7.3 | 322. |
| 22 | .620 | 266. | 7.4 | 319. |
| 23 | .610 | 262. | 7.5 | 310. |
| 24 | .500 | 215. | 8.0 | 255. |

DAY = 87

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 9.0 | 179. |
| 2 | .330 | 142. | 9.5 | 161. |
| 3 | .340 | 146. | 9.5 | 175. |
| 4 | .350 | 150. | 9.1 | 196. |
| 5 | .380 | 163. | 8.9 | 207. |
| 6 | .360 | 155. | 9.3 | 173. |
| 7 | .340 | 146. | 9.4 | 179. |
| 8 | .380 | 163. | 9.1 | 212. |
| 9 | .610 | 262. | 8.3 | 295. |
| 10 | .650 | 279. | 8.0 | 296. |
| 11 | .610 | 262. | 8.0 | 289. |
| 12 | .600 | 258. | 8.0 | 288. |
| 13 | .620 | 266. | 8.1 | 288. |
| 14 | .620 | 266. | 8.0 | 288. |
| 15 | .610 | 262. | 8.0 | 287. |
| 16 | .620 | 266. | 8.0 | 287. |
| 17 | .650 | 279. | 8.0 | 288. |
| 18 | .680 | 292. | 8.0 | 289. |
| 19 | .660 | 284. | 8.0 | 288. |
| 20 | .660 | 284. | 7.9 | 289. |
| 21 | .670 | 288. | 8.0 | 288. |
| 22 | .580 | 249. | 8.1 | 265. |
| 23 | .380 | 163. | 8.7 | 198. |
| 24 | .350 | 150. | 9.5 | 167. |

DAY = 88



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .330 | 142. | 9.9 | 161. |
| 2 | .350 | 150. | 9.9 | 159. |
| 3 | .350 | 150. | 9.9 | 160. |
| 4 | .360 | 155. | 9.9 | 159. |
| 5 | .360 | 155. | 10.1 | 159. |
| 6 | .350 | 150. | 10.0 | 158. |
| 7 | .350 | 150. | 10.0 | 166. |
| 8 | .480 | 206. | 9.5 | 184. |
| 9 | .500 | 215. | 9.2 | 219. |
| 10 | .540 | 232. | 9.0 | 240. |
| 11 | .540 | 232. | 8.8 | 245. |
| 12 | .520 | 223. | 8.5 | 253. |
| 13 | .510 | 219. | 8.5 | 255. |
| 14 | .490 | 210. | 8.5 | 246. |
| 15 | .470 | 202. | 8.5 | 232. |
| 16 | .440 | 189. | 8.8 | 215. |
| 17 | .440 | 189. | 8.9 | 210. |
| 18 | .460 | 198. | 8.7 | 224. |
| 19 | .490 | 210. | 8.5 | 238. |
| 20 | .550 | 236. | 8.5 | 260. |
| 21 | .480 | 206. | 8.5 | 248. |
| 22 | .490 | 210. | 8.6 | 242. |
| 23 | .420 | 180. | 9.1 | 193. |
| 24 | .320 | 137. | 9.9 | 154. |

DAY = 89

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 9.1 | 154. |
| 2 | .300 | 129. | 9.3 | 154. |
| 3 | .300 | 129. | 9.1 | 153. |
| 4 | .300 | 129. | 9.1 | 154. |
| 5 | .290 | 125. | 9.0 | 154. |
| 6 | .350 | 150. | 9.4 | 183. |
| 7 | .530 | 228. | 8.5 | 269. |
| 8 | .540 | 232. | 8.2 | 300. |
| 9 | .570 | 245. | 7.9 | 312. |
| 10 | .490 | 210. | 7.5 | 299. |
| 11 | .510 | 219. | 7.4 | 304. |
| 12 | .560 | 241. | 7.3 | 311. |
| 13 | .560 | 241. | 7.3 | 313. |
| 14 | .550 | 236. | 7.2 | 316. |
| 15 | .570 | 245. | 7.3 | 315. |
| 16 | .580 | 249. | 7.2 | 316. |
| 17 | .620 | 266. | 7.2 | 313. |
| 18 | .650 | 279. | 7.3 | 312. |
| 19 | .580 | 249. | 7.2 | 313. |
| 20 | .540 | 232. | 7.3 | 312. |
| 21 | .570 | 245. | 7.3 | 313. |
| 22 | .570 | 245. | 7.3 | 313. |
| 23 | .580 | 249. | 7.3 | 312. |
| 24 | .590 | 253. | 7.3 | 311. |

DAY # 90



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 7.9 | 240. |
| 2 | .310 | 133. | 8.5 | 209. |
| 3 | .320 | 137. | 8.7 | 209. |
| 4 | .330 | 141. | 8.5 | 209. |
| 5 | .350 | 150. | 8.5 | 210. |
| 6 | .350 | 150. | 8.6 | 215. |
| 7 | .530 | 228. | 8.2 | 282. |
| 8 | .600 | 25[illegible]. | 7.7 | 313. |
| 9 | .550 | 236. | 7.1 | 324. |
| 10 | .550 | 236. | 7.1 | 324. |
| 11 | .560 | 241. | 7.0 | 324. |
| 12 | .560 | 241. | 6.9 | 324. |
| 13 | .550 | 236. | 6.9 | 324. |
| 14 | .590 | 253. | 7.0 | 325. |
| 15 | .660 | 284. | 7.4 | 324. |
| 16 | .700 | 301. | 7.4 | 324. |
| 17 | .720 | 309. | 7.5 | 324. |
| 18 | .730 | 314. | 7.6 | 324. |
| 19 | .730 | 314. | 7.5 | 325. |
| 20 | .760 | 326. | 7.5 | 324. |
| 21 | .760 | 326. | 7.5 | 324. |
| 22 | .730 | 314. | 7.6 | 324. |
| 23 | .770 | 331. | 7.5 | 324. |
| 24 | .760 | 326. | 7.5 | 318. |

APPENDIX L

PROPRIETARY INFORMATION - UNIT B

Input Data

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

CONFIDENTIAL INFORMATION UNIT B

COMBUSTION ENGR BOILER WITH OVERFIRE AIR 350 MWE GROSS

SUBBITUMINOUS (C) COAL

NOX MON. REL. ACCURACY = 6.5 PC

DAY 1 = 1 JANUARY 1981

PERFORMANCE NOX = 0.49 LB/10**6BTU (211 NG/J)

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .210 | 90. | 6.4 | 174. |
| 2 | .190 | 82. | 6.0 | 200. |
| 3 | .190 | 82. | 6.1 | 198. |
| 4 | .190 | 82. | 6.1 | 198. |
| 5 | .190 | 82. | 6.5 | 186. |
| 6 | .250 | 107. | 7.0 | 147. |
| 7 | .250 | 107. | 6.9 | 147. |
| 8 | .220 | 95. | 6.5 | 173. |
| 9 | .220 | 95. | 6.0 | 216. |
| 10 | .270 | 116. | 5.6 | 261. |
| 11 | .290 | 125. | 5.3 | 294. |
| 12 | .300 | 129. | 5.3 | 297. |
| 13 | .280 | 120. | 5.3 | 281. |
| 14 | .250 | 107. | 5.3 | 264. |
| 15 | .250 | 107. | 5.4 | 261. |
| 16 | .260 | 112. | 5.4 | 262. |
| 17 | .280 | 120. | 5.5 | 252. |
| 18 | .250 | 107. | 5.5 | 247. |
| 19 | .290 | 125. | 5.4 | 284. |
| 20 | .270 | 116. | 5.4 | 271. |
| 21 | .250 | 107. | 5.5 | 241. |
| 22 | .260 | 112. | 5.8 | 233. |
| 23 | .260 | 112. | 6.2 | 214. |
| 24 | .280 | 120. | 5.7 | 234. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 6.0 | 207. |
| 2 | .270 | 116. | 6.2 | 195. |
| 3 | .270 | 116. | 6.5 | 187. |
| 4 | .270 | 116. | 6.4 | 188. |
| 5 | .270 | 116. | 6.4 | 188. |
| 6 | .270 | 116. | 6.5 | 186. |
| 7 | .260 | 112. | 6.2 | 210. |
| 8 | .270 | 116. | 5.6 | 256. |
| 9 | .300 | 129. | 5.5 | 316. |
| 10 | .300 | 129. | 5.6 | 322. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .340 | 146. | 5.3 | 316. |
| 16 | .370 | 159. | 5.4 | 313. |
| 17 | .290 | 125. | 5.2 | 300. |
| 18 | .250 | 107. | 5.2 | 290. |
| 19 | .300 | 129. | 5.2 | 315. |
| 20 | .290 | 125. | 5.2 | 296. |

| | | | | |
|---|---|---|---|---|
| 21 | .290 | 125. | 5.3 | 269. |
| 22 | .260 | 112. | 5.3 | 263. |
| 23 | .260 | 112. | 5.3 | 267. |
| 24 | .240 | 103. | 5.5 | 242. |

DAY = 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 6.0 | 205. |
| 2 | .270 | 116. | 6.3 | 195. |
| 3 | .280 | 120. | 6.4 | 197. |
| 4 | .280 | 120. | 6.3 | 204. |
| 5 | .290 | 125. | 6.3 | 209. |
| 6 | .310 | 133. | 6.3 | 219. |
| 7 | .310 | 133. | 6.0 | 232. |
| 8 | .300 | 129. | 5.7 | 250. |
| 9 | .310 | 133. | 5.7 | 252. |
| 10 | .310 | 133. | 5.6 | 259. |
| 11 | .300 | 129. | 5.5 | 264. |
| 12 | .290 | 125. | 5.5 | 260. |
| 13 | .300 | 129. | 5.5 | 260. |
| 14 | .300 | 129. | 5.7 | 247. |
| 15 | .290 | 125. | 5.9 | 225. |
| 16 | .280 | 120. | 6.1 | 202. |
| 17 | .310 | 133. | 6.1 | 203. |
| 18 | .290 | 125. | 5.7 | 239. |
| 19 | .310 | 133. | 5.4 | 291. |
| 20 | .300 | 129. | 5.3 | 304. |
| 21 | .260 | 112. | 5.2 | 290. |
| 22 | .300 | 129. | 5.3 | 275. |
| 23 | .280 | 120. | 5.6 | 249. |
| 24 | .310 | 133. | 5.9 | 221. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 5.7 | 248. |
| 2 | .270 | 116. | 5.5 | 260. |
| 3 | .300 | 129. | 5.6 | 266. |
| 4 | .280 | 120. | 5.7 | 249. |
| 5 | .290 | 125. | 6.2 | 209. |
| 6 | .260 | 112. | 6.7 | 159. |
| 7 | .310 | 133. | 6.2 | 238. |
| 8 | .250 | 107. | 5.3 | 312. |
| 9 | .230 | 99. | 5.4 | 316. |
| 10 | .220 | 95. | 5.5 | 316. |
| 11 | .220 | 95. | 5.4 | 315. |
| 12 | .230 | 99. | 5.4 | 310. |
| 13 | .230 | 99. | 5.3 | 311. |
| 14 | .270 | 116. | 5.4 | 315. |
| 15 | .300 | 129. | 5.3 | 314. |
| 16 | .290 | 125. | 5.4 | 310. |
| 17 | .260 | 112. | 5.3 | 310. |
| 18 | .240 | 103. | 5.3 | 313. |
| 19 | .250 | 107. | 5.3 | 319. |

| | | | | |
|---|---|---|---|---|
| 20 | .280 | 120. | 5.3 | 312. |
| 21 | .270 | 116. | 5.3 | 313. |
| 22 | .250 | 107. | 5.2 | 316. |
| 23 | .260 | 112. | 5.3 | 315. |
| 24 | .230 | 99. | 5.4 | 281. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 5.8 | 222. |
| 2 | .230 | 99. | 6.2 | 199. |
| 3 | .230 | 99. | 6.4 | 185. |
| 4 | .240 | 103. | 6.5 | 181. |
| 5 | .250 | 107. | 6.4 | 191. |
| 6 | .250 | 107. | 6.3 | 205. |
| 7 | .260 | 112. | 5.8 | 251. |
| 8 | .260 | 112. | 5.4 | 294. |
| 9 | .260 | 112. | 5.3 | 298. |
| 10 | .250 | 107. | 5.3 | 287. |
| 11 | .250 | 107. | 5.3 | 277. |
| 12 | .230 | 99. | 5.3 | 271. |
| 13 | .240 | 103. | 5.4 | 263. |
| 14 | .240 | 103. | 5.5 | 257. |
| 15 | .230 | 99. | 5.4 | 270. |
| 16 | .230 | 99. | 5.3 | 271. |
| 17 | .240 | 103. | 5.1 | 279. |
| 18 | .270 | 116. | 5.1 | 291. |
| 19 | .270 | 116. | 4.9 | 297. |
| 20 | .260 | 112. | 4.7 | 299. |
| 21 | .220 | 95. | 4.5 | 296. |
| 22 | .210 | 90. | 4.4 | 298. |
| 23 | .220 | 95. | 4.4 | 298. |
| 24 | .260 | 112. | 5.0 | 303. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 5.1 | 283. |
| 2 | .220 | 95. | 4.8 | 297. |
| 3 | .210 | 90. | 4.7 | 299. |
| 4 | .220 | 95. | 4.6 | 302. |
| 5 | .240 | 103. | 4.6 | 307. |
| 6 | .290 | 125. | 5.1 | 260. |
| 7 | .290 | 125. | 5.5 | 225. |
| 8 | .310 | 133. | 4.9 | 309. |
| 9 | .340 | 146. | 5.3 | 299. |
| 10 | .350 | 150. | 5.4 | 321. |
| 11 | .330 | 142. | 5.4 | 321. |
| 12 | .310 | 133. | 5.3 | 319. |
| 13 | .350 | 150. | 5.2 | 318. |
| 14 | .320 | 137. | 5.3 | 308. |
| 15 | .310 | 133. | 5.2 | 314. |
| 16 | .320 | 137. | 5.2 | 318. |
| 17 | .320 | 137. | 5.2 | 322. |
| 18 | .330 | 142. | 5.1 | 322. |

| | | | | |
|---|---|---|---|---|
| 19 | .320 | 137. | 5.1 | 322. |
| 20 | .320 | 137. | 5.1 | 317. |
| 21 | .350 | 150. | 5.2 | 323. |
| 22 | .350 | 150. | 5.3 | 324. |
| 23 | .330 | 142. | 5.4 | 310. |
| 24 | .240 | 103. | 6.4 | 182. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 6.4 | 154. |
| 2 | .210 | 90. | 6.9 | 153. |
| 3 | .210 | 90. | 6.8 | 162. |
| 4 | .240 | 103. | 6.7 | 172. |
| 5 | .240 | 103. | 6.7 | 178. |
| 6 | .230 | 99. | 6.5 | 186. |
| 7 | .280 | 120. | 6.1 | 246. |
| 8 | .270 | 116. | 5.5 | 322. |
| 9 | .270 | 116. | 5.5 | 323. |
| 10 | .250 | 107. | 5.4 | 322. |
| 11 | .250 | 107. | 5.6 | 321. |
| 12 | .250 | 107. | 5.5 | 324. |
| 13 | .260 | 112. | 5.6 | 294. |
| 14 | .210 | 90. | 5.8 | 209. |
| 15 | .210 | 90. | 6.2 | 191. |
| 16 | .260 | 112. | 6.4 | 240. |
| 17 | .240 | 103. | 6.0 | 250. |
| 18 | .260 | 112. | 5.7 | 264. |
| 19 | .310 | 133. | 5.6 | 287. |
| 20 | .290 | 125. | 5.5 | 295. |
| 21 | .270 | 116. | 5.6 | 293. |
| 22 | .240 | 103. | 5.6 | 279. |
| 23 | .220 | 95. | 5.7 | 236. |
| 24 | .230 | 99. | 6.3 | 208. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 6.6 | 169. |
| 2 | .220 | 95. | 6.8 | 174. |
| 3 | .220 | 95. | 6.7 | 170. |
| 4 | .220 | 95. | 6.7 | 173. |
| 5 | .210 | 90. | 6.6 | 177. |
| 6 | .220 | 95. | 6.5 | 184. |
| 7 | .250 | 107. | 6.4 | 232. |
| 8 | .280 | 120. | 5.7 | 318. |
| 9 | .300 | 129. | 5.6 | 323. |
| 10 | .330 | 142. | 5.6 | 321. |
| 11 | .310 | 133. | 5.6 | 322. |
| 12 | .300 | 129. | 5.7 | 321. |
| 13 | .300 | 129. | 6.0 | 299. |
| 14 | .330 | 142. | 5.7 | 304. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .330 | 142. | 5.6 | 223. |
| 17 | .290 | 125. | 5.4 | 322. |

| | | | | |
|---|---|---|---|---|
| 18 | .290 | 125. | 5.4 | 311. |
| 19 | .270 | 116. | 5.3 | 319. |
| 20 | .250 | 107. | 5.3 | 315. |
| 21 | .260 | 112. | 5.4 | 316. |
| 22 | .260 | 112. | 5.4 | 311. |
| 23 | .240 | 103. | 5.3 | 304. |
| 24 | .240 | 103. | 5.6 | 267. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 6.3 | 202. |
| 2 | .230 | 99. | 7.1 | 139. |
| 3 | .240 | 103. | 7.2 | 139. |
| 4 | .230 | 99. | 7.0 | 142. |
| 5 | .220 | 95. | 6.9 | 148. |
| 6 | .210 | 90. | 6.7 | 160. |
| 7 | .240 | 103. | 6.4 | 191. |
| 8 | .250 | 107. | 6.1 | 240. |
| 9 | .260 | 112. | 5.6 | 317. |
| 10 | .260 | 112. | 5.6 | 324. |
| 11 | .250 | 107. | 5.5 | 322. |
| 12 | .260 | 112. | 5.6 | 323. |
| 13 | .260 | 112. | 5.5 | 326. |
| 14 | .260 | 112. | 5.5 | 324. |
| 15 | .250 | 107. | 5.5 | 322. |
| 16 | .260 | 112. | 5.5 | 322. |
| 17 | .260 | 112. | 5.4 | 324. |
| 18 | .250 | 107. | 5.4 | 322. |
| 19 | .250 | 107. | 5.4 | 322. |
| 20 | .280 | 120. | 5.4 | 320. |
| 21 | .290 | 125. | 5.4 | 321. |
| 22 | .300 | 129. | 5.4 | 323. |
| 23 | .300 | 129. | 5.4 | 328. |
| 24 | .310 | 133. | 5.4 | 319. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 5.5 | 308. |
| 2 | .310 | 133. | 5.4 | 318. |
| 3 | .300 | 129. | 5.4 | 313. |
| 4 | .250 | 107. | 5.6 | 264. |
| 5 | .230 | 99. | 5.9 | 235. |
| 6 | .240 | 103. | 6.0 | 239. |
| 7 | .230 | 99. | 5.9 | 244. |
| 8 | .250 | 107. | 5.8 | 264. |
| 9 | .280 | 120. | 5.6 | 295. |
| 10 | .340 | 146. | 5.6 | 323. |
| 11 | .320 | 137. | 5.5 | 322. |
| 12 | .320 | 137. | 5.5 | 321. |
| 13 | .320 | 137. | 5.5 | 316. |
| 14 | .310 | 133. | 5.7 | 310. |
| 15 | .270 | 116. | 5.7 | 296. |
| 16 | .260 | 112. | 5.8 | 267. |

| | | | | |
|---|---|---|---|---|
| 17 | .290 | 125. | 5.9 | 265. |
| 18 | .310 | 133. | 5.7 | 287. |
| 19 | .300 | 129. | 5.9 | 271. |
| 20 | .260 | 112. | 6.0 | 252. |
| 21 | .280 | 120. | 6.1 | 252. |
| 22 | .290 | 125. | 6.1 | 254. |
| 23 | .270 | 116. | 6.1 | 255. |
| 24 | .260 | 112. | 6.2 | 247. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 6.1 | 257. |
| 2 | .260 | 112. | 6.2 | 252. |
| 3 | .260 | 112. | 6.6 | 212. |
| 4 | .260 | 112. | 7.5 | 148. |
| 5 | .260 | 112. | 7.4 | 148. |
| 6 | .270 | 116. | 7.5 | 149. |
| 7 | .280 | 120. | 6.8 | 203. |
| 8 | .250 | 107. | 6.4 | 225. |
| 9 | .270 | 116. | 5.6 | 298. |
| 10 | .200 | 86. | 5.5 | 309. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .300 | 129. | 5.6 | 265. |
| 16 | .320 | 137. | 5.0 | 280. |
| 17 | .330 | 142. | 4.9 | 282. |
| 18 | .340 | 146. | 4.8 | 307. |
| 19 | .340 | 146. | 4.9 | 311. |
| 20 | .340 | 146. | 4.9 | 312. |
| 21 | .360 | 155. | 4.9 | 318. |
| 22 | .360 | 155. | 4.9 | 318. |
| 23 | .360 | 155. | 5.0 | 294. |
| 24 | .330 | 142. | 6.0 | 185. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.4 | 153. |
| 2 | .330 | 142. | 6.4 | 151. |
| 3 | .350 | 150. | 6.5 | 150. |
| 4 | .350 | 150. | 6.5 | 157. |
| 5 | .340 | 146. | 6.5 | 159. |
| 6 | .320 | 137. | 6.3 | 176. |
| 7 | .380 | 163. | 6.0 | 221. |
| 8 | .390 | 168. | 5.1 | 319. |
| 9 | .420 | 180. | 5.1 | 324. |
| 10 | .460 | 198. | 5.8 | 322. |
| 11 | .480 | 206. | 6.0 | 321. |
| 12 | .450 | 193. | 6.2 | 315. |
| 13 | .460 | 198. | 6.1 | 321. |
| 14 | .430 | 185. | 6.2 | 320. |
| 15 | .430 | 185. | 6.2 | 319. |

| | | | | |
|---|---|---|---|---|
| 16 | .430 | 185. | 6.1 | 319. |
| 17 | .490 | 210. | 6.1 | 323. |
| 18 | .490 | 210. | 6.2 | 327. |
| 19 | .420 | 180. | 6.1 | 324. |
| 20 | .390 | 168. | 6.1 | 314. |
| 21 | .410 | 176. | 6.1 | 312. |
| 22 | .440 | 189. | 6.2 | 316. |
| 23 | .430 | 185. | 6.2 | 307. |
| 24 | .400 | 172. | 6.2 | 288. |

DAY = 14

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .220 | 95. | 6.6 | 169. |
| 2 | .220 | 95. | 6.8 | 174. |
| 3 | .220 | 95. | 6.7 | 170. |
| 4 | .220 | 95. | 6.7 | 173. |
| 5 | .210 | 90. | 6.6 | 177. |
| 6 | .220 | 95. | 6.5 | 184. |
| 7 | .250 | 107. | 6.4 | 232. |
| 8 | .280 | 120. | 5.7 | 318. |
| 9 | .300 | 129. | 5.6 | 323. |
| 10 | .330 | 142. | 5.6 | 321. |
| 11 | .310 | 133. | 5.6 | 322. |
| 12 | .300 | 129. | 5.7 | 321. |
| 13 | .300 | 129. | 6.0 | 299. |
| 14 | .330 | 142. | 5.7 | 304. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .350 | 150. | 5.8 | 238. |
| 17 | .500 | 215. | 6.2 | 217. |
| 18 | .510 | 219. | 6.1 | 310. |
| 19 | .510 | 219. | 6.1 | 324. |
| 20 | .520 | 223. | 6.2 | 325. |
| 21 | .550 | 236. | 6.1 | 324. |
| 22 | .540 | 232. | 6.2 | 321. |
| 23 | .430 | 185. | 6.2 | 290. |
| 24 | .380 | 163. | 6.7 | 240. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 6.8 | 233. |
| 2 | .450 | 193. | 6.9 | 232. |
| 3 | .450 | 193. | 6.9 | 232. |
| 4 | .450 | 193. | 6.9 | 233. |
| 5 | .450 | 193. | 6.9 | 232. |
| 6 | .430 | 185. | 6.9 | 233. |
| 7 | .390 | 168. | 6.9 | 234. |
| 8 | .460 | 198. | 6.4 | 308. |
| 9 | .480 | 206. | 6.4 | 324. |
| 10 | .510 | 219. | 6.3 | 118. |
| 11 | .450 | 193. | 6.3 | 306. |
| 12 | .370 | 159. | 6.3 | 272. |
| 13 | .380 | 163. | 6.4 | 265. |
| 14 | .380 | 163. | 6.2 | 284. |

| | | | | |
|---|---|---|---|---|
| 15 | .450 | 193. | 6.1 | 309. |
| 16 | .490 | 210. | 6.1 | 322. |
| 17 | .390 | 168. | 6.1 | 310. |
| 18 | .380 | 163. | 6.2 | 293. |
| 19 | .400 | 172. | 6.0 | 311. |
| 20 | .430 | 185. | 6.1 | 317. |
| 21 | .460 | 198. | 6.2 | 318. |
| 22 | .480 | 206. | 6.2 | 311. |
| 23 | .430 | 185. | 6.3 | 278. |
| 24 | .380 | 163. | 7.0 | 204. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 7.7 | 173. |
| 2 | .420 | 180. | 8.1 | 152. |
| 3 | .430 | 185. | 8.1 | 149. |
| 4 | .430 | 185. | 8.1 | 149. |
| 5 | .440 | 189. | 8.2 | 150. |
| 6 | .380 | 163. | 7.7 | 179. |
| 7 | .420 | 180. | 7.3 | 229. |
| 8 | .380 | 163. | 6.7 | 290. |
| 9 | .390 | 168. | 6.3 | 321. |
| 10 | .390 | 168. | 6.3 | 321. |
| 11 | .380 | 163. | 6.3 | 321. |
| 12 | .400 | 172. | 6.3 | 318. |
| 13 | .470 | 202. | 6.1 | 320. |
| 14 | .450 | 193. | 6.1 | 322. |
| 15 | .450 | 193. | 6.1 | 318. |
| 16 | .440 | 189. | 6.2 | 316. |
| 17 | .430 | 185. | 6.2 | 305. |
| 18 | .410 | 176. | 6.2 | 293. |
| 19 | .430 | 185. | 6.2 | 309. |
| 20 | .420 | 180. | 6.3 | 288. |
| 21 | .400 | 172. | 6.3 | 277. |
| 22 | .410 | 176. | 6.3 | 266. |
| 23 | .430 | 185. | 6.6 | 249. |
| 24 | .340 | 146. | 7.2 | 189. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 7.9 | 168. |
| 2 | .370 | 159. | 7.9 | 167. |
| 3 | .350 | 150. | 7.6 | 184. |
| 4 | .340 | 146. | 7.7 | 181. |
| 5 | .310 | 133. | 7.7 | 182. |
| 6 | .310 | 133. | 7.5 | 192. |
| 7 | .390 | 168. | 7.2 | 217. |
| 8 | .440 | 189. | 7.0 | 240. |
| 9 | .400 | 172. | 6.8 | 248. |
| 10 | .400 | 172. | 6.8 | 249. |
| 11 | .420 | 180. | 6.4 | 290. |
| 12 | .410 | 176. | 6.2 | 293. |
| 13 | .420 | 180. | 6.2 | 297. |

| | | | | |
|---|---|---|---|---|
| 14 | .400 | 172. | 6.2 | 275. |
| 15 | .380 | 163. | 6.3 | 255. |
| 16 | .390 | 168. | 6.8 | 227. |
| 17 | .390 | 168. | 6.7 | 239. |
| 18 | .410 | 176. | 6.5 | 262. |
| 19 | .460 | 198. | 6.2 | 300. |
| 20 | .440 | 189. | 6.2 | 291. |
| 21 | .440 | 189. | 6.3 | 269. |
| 22 | .410 | 176. | 6.3 | 269. |
| 23 | .410 | 176. | 6.4 | 258. |
| 24 | .330 | 142. | 6.7 | 219. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 7.8 | 163. |
| 2 | .370 | 159. | 7.9 | 158. |
| 3 | .370 | 159. | 7.8 | 158. |
| 4 | .380 | 163. | 7.9 | 155. |
| 5 | .370 | 159. | 7.8 | 158. |
| 6 | .340 | 146. | 7.8 | 159. |
| 7 | .340 | 146. | 7.6 | 172. |
| 8 | .400 | 172. | 7.3 | 196. |
| 9 | .330 | 142. | 6.9 | 221. |
| 10 | .300 | 129. | 6.6 | 244. |
| 11 | .290 | 125. | 6.5 | 241. |
| 12 | .300 | 129. | 6.5 | 246. |
| 13 | .290 | 125. | 6.4 | 247. |
| 14 | .300 | 129. | 6.7 | 231. |
| 15 | .310 | 133. | 6.8 | 213. |
| 16 | .320 | 137. | 6.9 | 208. |
| 17 | .310 | 133. | 7.0 | 200. |
| 18 | .320 | 137. | 7.2 | 209. |
| 19 | .310 | 133. | 6.5 | 247. |
| 20 | .310 | 133. | 6.5 | 250. |
| 21 | .310 | 133. | 6.7 | 234. |
| 22 | .310 | 133. | 6.7 | 234. |
| 23 | .300 | 129. | 6.5 | 239. |
| 24 | .330 | 142. | 7.1 | 191. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .360 | 155. | 7.5 | 191. |
| 2 | .350 | 150. | 6.8 | 212. |
| 3 | .340 | 146. | 6.9 | 212. |
| 4 | .480 | 206. | 6.7 | 248. |
| 5 | .420 | 180. | 6.4 | 269. |
| 6 | .410 | 176. | 6.3 | 271. |
| 7 | .430 | 185. | 6.1 | 299. |
| 8 | .470 | 202. | 6.1 | 301. |
| 9 | .470 | 202. | 6.1 | 301. |
| 10 | .420 | 180. | 6.1 | 301. |
| 11 | .410 | 176. | 6.0 | 311. |
| 12 | .450 | 193. | 6.0 | 322. |

| | | | | |
|---|---|---|---|---|
| 13 | .440 | 189. | 5.9 | 322. |
| 14 | .430 | 185. | 6.0 | 322. |
| 15 | .440 | 189. | 5.9 | 322. |
| 16 | .460 | 198. | 5.9 | 318. |
| 17 | .460 | 198. | 5.9 | 319. |
| 18 | .470 | 202. | 5.9 | 321. |
| 19 | .520 | 223. | 5.9 | 324. |
| 20 | .520 | 223. | 5.9 | 324. |
| 21 | .470 | 202. | 5.8 | 325. |
| 22 | .470 | 202. | 5.9 | 319. |
| 23 | .440 | 189. | 6.0 | 300. |
| 24 | .330 | 142. | 6.5 | 229. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 7.0 | 187. |
| 2 | .360 | 155. | 7.2 | 187. |
| 3 | .330 | 142. | 7.3 | 187. |
| 4 | .350 | 150. | 7.3 | 187. |
| 5 | .340 | 146. | 7.4 | 187. |
| 6 | .320 | 137. | 7.3 | 187. |
| 7 | .320 | 137. | 7.0 | 188. |
| 8 | .390 | 168. | 6.9 | 228. |
| 9 | .420 | 180. | 6.1 | 297. |
| 10 | .410 | 176. | 6.0 | 306. |
| 11 | .410 | 176. | 5.9 | 307. |
| 12 | .410 | 176. | 5.9 | 307. |
| 13 | .420 | 180. | 5.9 | 306. |
| 14 | .420 | 180. | 5.8 | 318. |
| 15 | .450 | 193. | 5.9 | 320. |
| 16 | .420 | 180. | 5.9 | 304. |
| 17 | .410 | 176. | 5.8 | 308. |
| 18 | .410 | 176. | 5.8 | 308. |
| 19 | .420 | 180. | 5.7 | 321. |
| 20 | .500 | 215. | 5.9 | 350. |
| 21 | .500 | 215. | 5.8 | 335. |
| 22 | .480 | 206. | 5.8 | 338. |
| 23 | .480 | 206. | 5.9 | 334. |
| 24 | .420 | 180. | 6.1 | 282. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 6.6 | 219. |
| 2 | .260 | 112. | 7.1 | 190. |
| 3 | .370 | 159. | 7.9 | 149. |
| 4 | .370 | 159. | 7.9 | 149. |
| 5 | .390 | 168. | 7.9 | 149. |
| 6 | .370 | 159. | 7.8 | 151. |
| 7 | .270 | 116. | 6.9 | 187. |
| 8 | .390 | 168. | 6.4 | 253. |
| 9 | .420 | 180. | 6.2 | 306. |
| 10 | .460 | 198. | 6.1 | 324. |
| 11 | .460 | 198. | 6.1 | 320. |

| | | | | |
|---|---|---|---|---|
| 12 | .490 | 210. | 6.0 | 319. |
| 13 | .420 | 180. | 6.5 | 242. |
| 14 | .390 | 168. | 7.0 | 183. |
| 15 | .360 | 155. | 7.1 | 183. |
| 16 | .360 | 155. | 7.1 | 183. |
| 17 | .350 | 150. | 7.0 | 190. |
| 18 | .380 | 163. | 6.8 | 199. |
| 19 | .410 | 176. | 6.8 | 226. |
| 20 | .380 | 163. | 6.1 | 265. |
| 21 | .410 | 176. | 5.9 | 286. |
| 22 | .420 | 180. | 5.9 | 306. |
| 23 | .410 | 176. | 6.0 | 295. |
| 24 | .360 | 155. | 6.7 | 216. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 6.7 | 209. |
| 2 | .310 | 133. | 7.0 | 198. |
| 3 | .310 | 133. | 7.0 | 197. |
| 4 | .310 | 133. | 7.0 | 193. |
| 5 | .320 | 137. | 7.0 | 199. |
| 6 | .330 | 142. | 6.9 | 215. |
| 7 | .430 | 185. | 6.2 | 280. |
| 8 | .450 | 193. | 6.0 | 322. |
| 9 | .440 | 189. | 5.9 | 322. |
| 10 | .500 | 215. | 5.9 | 321. |
| 11 | .470 | 202. | 5.9 | 320. |
| 12 | .420 | 180. | 5.8 | 320. |
| 13 | .440 | 189. | 5.8 | 319. |
| 14 | .460 | 198. | 5.8 | 320. |
| 15 | .460 | 198. | 5.8 | 327. |
| 16 | .450 | 193. | 5.7 | 313. |
| 17 | .410 | 176. | 5.7 | 306. |
| 18 | .370 | 159. | 5.6 | 305. |
| 19 | .410 | 176. | 5.6 | 322. |
| 20 | .400 | 172. | 5.6 | 317. |
| 21 | .390 | 168. | 5.4 | 316. |
| 22 | .410 | 176. | 5.5 | 313. |
| 23 | .370 | 159. | 5.8 | 266. |
| 24 | .340 | 146. | 6.8 | 188. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 7.4 | 163. |
| 2 | .380 | 163. | 7.5 | 158. |
| 3 | .380 | 163. | 7.5 | 155. |
| 4 | .390 | 168. | 7.7 | 148. |
| 5 | .390 | 168. | 7.7 | 150. |
| 6 | .350 | 150. | 7.1 | 181. |
| 7 | .410 | 176. | 6.2 | 274. |
| 8 | .380 | 163. | 5.5 | 324. |
| 9 | .390 | 168. | 5.6 | 330. |
| 10 | .440 | 189. | 5.6 | 330. |

| | | | | |
|---|---|---|---|---|
| 11 | .430 | 185. | 5.7 | 325. |
| 12 | .420 | 180. | 5.7 | 322. |
| 13 | .420 | 180. | 5.5 | 321. |
| 14 | .450 | 193. | 5.8 | 322. |
| 15 | .450 | 193. | 5.8 | 321. |
| 16 | .460 | 198. | 5.8 | 322. |
| 17 | .470 | 202. | 5.8 | 322. |
| 18 | .480 | 206. | 5.8 | 321. |
| 19 | .480 | 206. | 5.8 | 324. |
| 20 | .430 | 185. | 5.8 | 319. |
| 21 | .450 | 193. | 5.8 | 321. |
| 22 | .470 | 202. | 5.9 | 322. |
| 23 | .430 | 185. | 5.9 | 320. |
| 24 | .440 | 189. | 6.0 | 311. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 6.0 | 276. |
| 2 | .380 | 163. | 6.1 | 260. |
| 3 | .400 | 172. | 6.2 | 250. |
| 4 | .410 | 176. | 6.3 | 247. |
| 5 | .400 | 172. | 6.3 | 247. |
| 6 | .390 | 168. | 6.3 | 252. |
| 7 | .400 | 172. | 6.1 | 268. |
| 8 | .400 | 172. | 5.8 | 302. |
| 9 | .440 | 189. | 5.9 | 323. |
| 10 | .470 | 202. | 5.4 | 324. |
| 11 | .550 | 236. | 6.0 | 323. |
| 12 | .550 | 236. | 6.0 | 321. |
| 13 | .540 | 232. | 5.8 | 321. |
| 14 | .510 | 219. | 6.0 | 322. |
| 15 | .530 | 228. | 5.9 | 322. |
| 16 | .510 | 219. | 5.9 | 321. |
| 17 | .520 | 223. | 5.8 | 322. |
| 18 | .460 | 198. | 5.8 | 323. |
| 19 | .450 | 193. | 5.8 | 322. |
| 20 | .440 | 189. | 5.7 | 317. |
| 21 | .420 | 180. | 5.7 | 306. |
| 22 | .410 | 176. | 5.7 | 300. |
| 23 | .410 | 176. | 6.1 | 270. |
| 24 | .330 | 142. | 6.5 | 217. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 6.8 | 198. |
| 2 | .360 | 155. | 7.8 | 163. |
| 3 | .370 | 159. | 7.8 | 149. |
| 4 | .360 | 155. | 7.7 | 149. |
| 5 | .340 | 146. | 7.7 | 148. |
| 6 | .330 | 142. | 7.7 | 149. |
| 7 | .320 | 137. | 7.6 | 163. |
| 8 | .350 | 150. | 6.8 | 218. |
| 9 | .420 | 180. | 6.3 | 269. |

| | | | | |
|---|---|---|---|---|
| 10 | .400 | 172. | 6.0 | 294. |
| 11 | .380 | 163. | 5.9 | 296. |
| 12 | .400 | 172. | 5.9 | 305. |
| 13 | .400 | 172. | 5.9 | 300. |
| 14 | .380 | 163. | 5.9 | 278. |
| 15 | .380 | 163. | 6.3 | 259. |
| 16 | .390 | 168. | 6.4 | 243. |
| 17 | .370 | 159. | 6.5 | 234. |
| 18 | .380 | 163. | 6.3 | 260. |
| 19 | .420 | 180. | 6.1 | 315. |
| 20 | .420 | 180. | 6.1 | 315. |
| 21 | .370 | 159. | 6.4 | 250. |
| 22 | .370 | 159. | 6.7 | 235. |
| 23 | .370 | 159. | 7.3 | 188. |
| 24 | .400 | 172. | 8.1 | 149. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 7.9 | 149. |
| 2 | .400 | 172. | 8.0 | 149. |
| 3 | .400 | 172. | 7.9 | 148. |
| 4 | .390 | 168. | 8.0 | 152. |
| 5 | .370 | 159. | 7.6 | 168. |
| 6 | .390 | 168. | 7.1 | 203. |
| 7 | .380 | 163. | 6.6 | 264. |
| 8 | .390 | 168. | 5.8 | 340. |
| 9 | .380 | 163. | 5.6 | 344. |
| 10 | .380 | 163. | 5.6 | 344. |
| 11 | .400 | 172. | 5.6 | 344. |
| 12 | .410 | 176. | 5.6 | 344. |
| 13 | .460 | 198. | 5.5 | 344. |
| 14 | .460 | 198. | 5.6 | 344. |
| 15 | .490 | 210. | 5.6 | 344. |
| 16 | .490 | 210. | 5.5 | 344. |
| 17 | .450 | 193. | 5.5 | 344. |
| 18 | .460 | 198. | 5.5 | 344. |
| 19 | .490 | 210. | 5.4 | 345. |
| 20 | .470 | 202. | 5.4 | 343. |
| 21 | .480 | 206. | 5.5 | 344. |
| 22 | .500 | 215. | 5.5 | 344. |
| 23 | .490 | 210. | 5.5 | 344. |
| 24 | .510 | 219. | 5.5 | 344. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .510 | 219. | 5.6 | 344. |
| 2 | .430 | 185. | 5.5 | 344. |
| 3 | .430 | 185. | 5.5 | 344. |
| 4 | .410 | 176. | 5.5 | 344. |
| 5 | .430 | 185. | 5.5 | 344. |
| 6 | .430 | 185. | 5.5 | 344. |
| 7 | .420 | 180. | 5.5 | 344. |
| 8 | .440 | 189. | 5.6 | 344. |

| | | | | |
|---|---|---|---|---|
| 9 | .510 | 219. | 5.5 | 344. |
| 10 | .540 | 232. | 5.6 | 343. |
| 11 | .540 | 232. | 6.0 | 344. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | .370 | 159. | 6.0 | 344. |
| 15 | .550 | 236. | 6.0 | 344. |
| 16 | .490 | 210. | 6.0 | 344. |
| 17 | .480 | 206. | 6.0 | 344. |
| 18 | .470 | 202. | 5.9 | 344. |
| 19 | .490 | 210. | 6.0 | 344. |
| 20 | .470 | 202. | 5.9 | 344. |
| 21 | .490 | 210. | 5.9 | 344. |
| 22 | .460 | 198. | 5.9 | 344. |
| 23 | .490 | 210. | 6.0 | 344. |
| 24 | .450 | 193. | 5.9 | 344. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 5.9 | 344. |
| 2 | .470 | 202. | 6.0 | 344. |
| 3 | .500 | 215. | 5.9 | 344. |
| 4 | .570 | 245. | 5.9 | 344. |
| 5 | .540 | 232. | 5.9 | 344. |
| 6 | .560 | 241. | 5.9 | 344. |
| 7 | .530 | 228. | 5.9 | 343. |
| 8 | .550 | 236. | 5.8 | 344. |
| 9 | .570 | 245. | 5.7 | 344. |
| 10 | .540 | 232. | 5.5 | 343. |
| 11 | .540 | 232. | 5.6 | 344. |
| 12 | .590 | 253. | 5.6 | 344. |
| 13 | .600 | 258. | 5.5 | 344. |
| 14 | .550 | 236. | 5.3 | 344. |
| 15 | .580 | 249. | 5.2 | 344. |
| 16 | .590 | 253. | 5.2 | 344. |
| 17 | .590 | 253. | 5.3 | 344. |
| 18 | .600 | 258. | 5.2 | 344. |
| 19 | .590 | 253. | 5.1 | 344. |
| 20 | .510 | 219. | 5.0 | 344. |
| 21 | .570 | 245. | 4.9 | 345. |
| 22 | .570 | 245. | 4.8 | 344. |
| 23 | .520 | 223. | 4.7 | 344. |
| 24 | .540 | 232. | 4.7 | 344. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .560 | 241. | 4.7 | 344. |
| 2 | .480 | 206. | 4.8 | 345. |
| 3 | .500 | 215. | 4.7 | 344. |
| 4 | .510 | 219. | 4.7 | 344. |
| 5 | .510 | 219. | 4.7 | 344. |
| 6 | .490 | 210. | 4.8 | 345. |
| 7 | .450 | 193. | 4.7 | 344. |

| | | | | |
|---|---|---|---|---|
| 8 | .430 | 185. | 4.6 | 344. |
| 9 | .510 | 219. | 4.7 | 344. |
| 10 | .520 | 223. | 4.7 | 344. |
| 11 | .530 | 228. | 4.7 | 344. |
| 12 | .510 | 219. | 4.7 | 344. |
| 13 | .510 | 219. | 4.7 | 344. |
| 14 | .520 | 223. | 4.7 | 344. |
| 15 | .570 | 245. | 5.2 | 344. |
| 16 | .500 | 215. | 4.7 | 344. |
| 17 | .470 | 202. | 4.8 | 344. |
| 18 | .550 | 236. | 5.0 | 345. |
| 19 | .600 | 258. | 5.1 | 344. |
| 20 | .610 | 262. | 5.0 | 344. |
| 21 | .600 | 258. | 5.1 | 344. |
| 22 | .610 | 262. | 5.1 | 344. |
| 23 | .580 | 249. | 4.9 | 344. |
| 24 | .590 | 253. | 5.1 | 344. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .610 | 262. | 5.1 | 344. |
| 2 | .500 | 215. | 5.2 | 344. |
| 3 | .480 | 206. | 5.3 | 345. |
| 4 | .510 | 219. | 5.4 | 343. |
| 5 | .520 | 223. | 5.4 | 344. |
| 6 | .610 | 262. | 5.5 | 344. |
| 7 | .610 | 262. | 5.3 | 344. |
| 8 | .520 | 223. | 5.2 | 343. |
| 9 | .590 | 253. | 5.4 | 344. |
| 10 | .640 | 275. | 5.4 | 343. |
| 11 | .550 | 236. | 5.3 | 343. |
| 12 | .560 | 241. | 5.4 | 343. |
| 13 | .600 | 258. | 5.2 | 341. |
| 14 | .560 | 241. | 5.3 | 327. |
| 15 | .550 | 236. | 5.6 | 323. |
| 16 | .510 | 219. | 5.8 | 313. |
| 17 | .490 | 210. | 6.1 | 312. |
| 18 | .570 | 245. | 6.0 | 313. |
| 19 | .580 | 249. | 5.9 | 312. |
| 20 | .570 | 245. | 5.9 | 313. |
| 21 | .560 | 241. | 6.0 | 312. |
| 22 | .420 | 180. | 6.1 | 277. |
| 23 | .370 | 159. | 6.7 | 236. |
| 24 | .300 | 129. | 6.6 | 203. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 6.7 | 188. |
| 2 | .310 | 133. | 7.3 | 148. |
| 3 | .330 | 142. | 7.5 | 149. |
| 4 | .330 | 142. | 7.6 | 148. |
| 5 | .320 | 137. | 7.4 | 149. |
| 6 | .320 | 137. | 7.3 | 157. |

| | | | | |
|---|---|---|---|---|
| 7 | .360 | 155. | 6.8 | 203. |
| 8 | .390 | 168. | 6.3 | 261. |
| 9 | .410 | 176. | 5.8 | 315. |
| 10 | .380 | 163. | 5.3 | 322. |
| 11 | .380 | 163. | 5.3 | 316. |
| 12 | .390 | 168. | 5.4 | 321. |
| 13 | .370 | 159. | 5.5 | 297. |
| 14 | .380 | 163. | 5.7 | 273. |
| 15 | .420 | 180. | 6.2 | 240. |
| 16 | .300 | 129. | 6.5 | 213. |
| 17 | .340 | 146. | 6.7 | 205. |
| 18 | .350 | 150. | 6.8 | 217. |
| 19 | .320 | 137. | 6.3 | 246. |
| 20 | .360 | 155. | 6.0 | 278. |
| 21 | .370 | 159. | 5.8 | 280. |
| 22 | .420 | 180. | 6.2 | 265. |
| 23 | .350 | 150. | 6.4 | 227. |
| 24 | .370 | 159. | 7.2 | 187. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 8.1 | 139. |
| 2 | .440 | 189. | 8.0 | 139. |
| 3 | .420 | 180. | 7.5 | 167. |
| 4 | .400 | 172. | 7.0 | 206. |
| 5 | .390 | 168. | 6.9 | 218. |
| 6 | .390 | 168. | 7.0 | 208. |
| 7 | .380 | 163. | 6.3 | 279. |
| 8 | .380 | 163. | 6.0 | 309. |
| 9 | .370 | 159. | 6.0 | 295. |
| 10 | .370 | 159. | 6.0 | 295. |
| 11 | .350 | 150. | 6.0 | 279. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .370 | 159. | 6.3 | 229. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .400 | 172. | 6.3 | 255. |
| 16 | .400 | 172. | 6.2 | 260. |
| 17 | .420 | 180. | 6.2 | 260. |
| 18 | .430 | 185. | 6.1 | 269. |
| 19 | .460 | 198. | 5.9 | 301. |
| 20 | .380 | 163. | 5.7 | 301. |
| 21 | .380 | 163. | 5.9 | 281. |
| 22 | .380 | 163. | 6.3 | 237. |
| 23 | .430 | 185. | 7.1 | 187. |
| 24 | .430 | 185. | 7.9 | 146. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 7.9 | 147. |
| 2 | .430 | 185. | 7.9 | 148. |
| 3 | .440 | 189. | 8.0 | 148. |
| 4 | .430 | 185. | 8.0 | 148. |
| 5 | .400 | 172. | 8.0 | 151. |

| | | | | |
|---|---|---|---|---|
| 6 | .420 | 180. | 7.9 | 149. |
| 7 | .400 | 172. | 7.7 | 170. |
| 8 | .420 | 180. | 7.0 | 215. |
| 9 | .400 | 172. | 7.0 | 212. |
| 10 | .390 | 168. | 7.0 | 203. |
| 11 | .440 | 189. | 7.3 | 205. |
| 12 | .460 | 198. | 7.2 | 209. |
| 13 | .420 | 180. | 7.2 | 206. |
| 14 | .430 | 185. | 7.3 | 202. |
| 15 | .430 | 185. | 7.1 | 200. |
| 16 | .420 | 180. | 7.0 | 200. |
| 17 | .370 | 159. | 7.1 | 201. |
| 18 | .260 | 112. | 7.3 | 200. |
| 19 | .250 | 107. | 7.0 | 213. |
| 20 | .230 | 99. | 6.9 | 197. |
| 21 | .280 | 120. | 6.3 | 216. |
| 22 | .310 | 133. | 6.5 | 229. |
| 23 | .360 | 155. | 6.9 | 205. |
| 24 | .430 | 185. | 7.8 | 147. |

DAY # 37

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 7.4 | 149. |
| 2 | .290 | 125. | 7.5 | 148. |
| 3 | .310 | 133. | 7.7 | 149. |
| 4 | .300 | 129. | 7.6 | 149. |
| 5 | .310 | 133. | 7.6 | 148. |
| 6 | .310 | 133. | 7.6 | 149. |
| 7 | .340 | 146. | 7.4 | 171. |
| 8 | .320 | 137. | 6.6 | 202. |
| 9 | .260 | 112. | 5.9 | 210. |
| 10 | .310 | 133. | 6.3 | 224. |
| 11 | .330 | 142. | 6.1 | 246. |
| 12 | .340 | 146. | 5.9 | 290. |
| 13 | .340 | 146. | 5.8 | 295. |
| 14 | .330 | 142. | 5.8 | 297. |
| 15 | .320 | 137. | 5.7 | 288. |
| 16 | .320 | 137. | 5.7 | 283. |
| 17 | .330 | 142. | 5.7 | 289. |
| 18 | .320 | 137. | 5.6 | 293. |
| 19 | .320 | 137. | 5.6 | 295. |
| 20 | .330 | 142. | 5.8 | 279. |
| 21 | .320 | 137. | 6.1 | 230. |
| 22 | .320 | 137. | 6.7 | 188. |
| 23 | .330 | 142. | 7.1 | 170. |
| 24 | .300 | 129. | 7.5 | 142. |

DAY # 38

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .280 | 120. | 7.5 | 139. |
| 2 | .300 | 129. | 7.8 | 136. |
| 3 | .260 | 112. | 7.2 | 140. |
| 4 | .250 | 107. | 7.2 | 140. |

| | | | | |
|---|---|---|---|---|
| 5 | .250 | 107. | 7.1 | 140. |
| 6 | .290 | 125. | 7.2 | 159. |
| 7 | .320 | 137. | 7.1 | 182. |
| 8 | .330 | 142. | 6.9 | 189. |
| 9 | .350 | 150. | 6.7 | 217. |
| 10 | .310 | 133. | 6.1 | 261. |
| 11 | .300 | 129. | 5.9 | 276. |
| 12 | .280 | 120. | 6.1 | 251. |
| 13 | .330 | 142. | 6.7 | 200. |
| 14 | .330 | 142. | 6.9 | 182. |
| 15 | .340 | 146. | 7.2 | 175. |
| 16 | .310 | 133. | 7.4 | 149. |
| 17 | .280 | 120. | 7.4 | 144. |
| 18 | .300 | 129. | 7.4 | 154. |
| 19 | .330 | 142. | 6.7 | 223. |
| 20 | .310 | 133. | 5.9 | 273. |
| 21 | .310 | 133. | 6.3 | 233. |
| 22 | .320 | 137. | 6.5 | 210. |
| 23 | .330 | 142. | 6.6 | 208. |
| 24 | .290 | 125. | 7.4 | 153. |

DAY = 39

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 7.4 | 147. |
| 2 | .270 | 116. | 7.3 | 144. |
| 3 | .270 | 116. | 7.4 | 144. |
| 4 | .290 | 125. | 7.4 | 147. |
| 5 | .290 | 125. | 7.4 | 147. |
| 6 | .370 | 159. | 7.6 | 153. |
| 7 | .350 | 150. | 7.4 | 172. |
| 8 | .330 | 142. | 7.3 | 182. |
| 9 | .330 | 142. | 7.1 | 193. |
| 10 | .320 | 137. | 6.9 | 215. |
| 11 | .310 | 133. | 6.9 | 203. |
| 12 | .340 | 146. | 7.2 | 174. |
| 13 | .280 | 120. | 7.2 | 166. |
| 14 | .280 | 120. | 7.4 | 151. |
| 15 | .280 | 120. | 7.6 | 146. |
| 16 | .290 | 125. | 7.5 | 148. |
| 17 | .300 | 129. | 7.4 | 149. |
| 18 | .280 | 120. | 7.3 | 152. |
| 19 | .360 | 155. | 7.4 | 167. |
| 20 | .340 | 146. | 6.9 | 193. |
| 21 | .340 | 146. | 7.1 | 184. |
| 22 | .340 | 146. | 7.1 | 182. |
| 23 | .370 | 159. | 7.3 | 169. |
| 24 | .270 | 116. | 7.7 | 137. |

DAY = 40

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 7.4 | 139. |
| 2 | .260 | 112. | 7.3 | 141. |
| 3 | .270 | 116. | 7.4 | 141. |

| | | | | |
|---|---|---|---|---|
| 4 | .280 | 120. | 7.4 | 140. |
| 5 | .280 | 120. | 7.4 | 144. |
| 6 | .310 | 133. | 7.3 | 159. |
| 7 | .330 | 142. | 7.2 | 184. |
| 8 | .330 | 142. | 6.4 | 255. |
| 9 | .330 | 142. | 5.8 | 309. |
| 10 | .330 | 142. | 5.7 | 305. |
| 11 | .310 | 133. | 5.7 | 288. |
| 12 | .290 | 125. | 5.5 | 286. |
| 13 | .290 | 125. | 5.9 | 255. |
| 14 | .300 | 129. | 6.2 | 238. |
| 15 | .290 | 125. | 6.3 | 220. |
| 16 | .290 | 125. | 6.5 | 205. |
| 17 | .320 | 137. | 6.5 | 203. |
| 18 | .320 | 137. | 6.6 | 202. |
| 19 | .350 | 150. | 6.2 | 244. |
| 20 | .310 | 133. | 6.0 | 243. |
| 21 | .290 | 125. | 6.1 | 233. |
| 22 | .280 | 120. | 6.1 | 229. |
| 23 | .310 | 133. | 6.6 | 207. |
| 24 | .290 | 125. | 6.8 | 182. |

DAY = 41

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 7.2 | 161. |
| 2 | .350 | 150. | 7.4 | 155. |
| 3 | .370 | 159. | 7.5 | 150. |
| 4 | .370 | 159. | 7.5 | 148. |
| 5 | .360 | 155. | 7.4 | 149. |
| 6 | .380 | 163. | 7.5 | 149. |
| 7 | .350 | 150. | 7.3 | 156. |
| 8 | .320 | 137. | 6.7 | 210. |
| 9 | .360 | 155. | 6.6 | 201. |
| 10 | .330 | 142. | 6.4 | 215. |
| 11 | .300 | 129. | 6.0 | 242. |
| 12 | .280 | 120. | 5.6 | 271. |
| 13 | .290 | 125. | 5.8 | 259. |
| 14 | .300 | 129. | 5.9 | 249. |
| 15 | .290 | 125. | 6.0 | 228. |
| 16 | .300 | 129. | 6.2 | 218. |
| 17 | .310 | 133. | 6.2 | 232. |
| 18 | .320 | 137. | 5.8 | 265. |
| 19 | .340 | 146. | 5.5 | 304. |
| 20 | .320 | 137. | 5.5 | 308. |
| 21 | .310 | 133. | 5.5 | 305. |
| 22 | .280 | 120. | 5.7 | 267. |
| 23 | .280 | 120. | 5.9 | 253. |
| 24 | .320 | 137. | 6.5 | 204. |

DAY = 42

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.6 | 201. |
| 2 | .290 | 125. | 6.3 | 227. |

| | | | | |
|---|---|---|---|---|
| 3 | .300 | 129. | 6.0 | 251. |
| 4 | .280 | 120. | 5.9 | 251. |
| 5 | .280 | 120. | 5.8 | 256. |
| 6 | .300 | 129. | 5.7 | 273. |
| 7 | .320 | 137. | 5.6 | 297. |
| 8 | .320 | 137. | 5.6 | 312. |
| 9 | .330 | 142. | 5.8 | 310. |
| 10 | .420 | 180. | 5.8 | 316. |
| 11 | .410 | 176. | 5.7 | 317. |
| 12 | .440 | 189. | 5.8 | 309. |
| 13 | .440 | 189. | 5.7 | 275. |
| 14 | .420 | 180. | 5.7 | 310. |
| 15 | .340 | 146. | 5.8 | 281. |
| 16 | .300 | 129. | 6.0 | 254. |
| 17 | .310 | 133. | 6.1 | 248. |
| 18 | .390 | 168. | 5.9 | 275. |
| 19 | .470 | 202. | 5.7 | 317. |
| 20 | .440 | 189. | 5.7 | 315. |
| 21 | .410 | 176. | 5.8 | 296. |
| 22 | .350 | 150. | 5.7 | 282. |
| 23 | .410 | 176. | 5.7 | 294. |
| 24 | .310 | 133. | 5.7 | 285. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 5.7 | 283. |
| 2 | .360 | 155. | 5.8 | 308. |
| 3 | .350 | 150. | 5.9 | 298. |
| 4 | .330 | 142. | 6.3 | 239. |
| 5 | .310 | 133. | 6.7 | 198. |
| 6 | .320 | 137. | 6.9 | 197. |
| 7 | .340 | 146. | 6.9 | 206. |
| 8 | .350 | 150. | 6.0 | 285. |
| 9 | .310 | 133. | 6.0 | 259. |
| 10 | .300 | 129. | 5.9 | 263. |
| 11 | .300 | 129. | 5.9 | 264. |
| 12 | .300 | 129. | 5.9 | 257. |
| 13 | .300 | 129. | 6.4 | 210. |
| 14 | .300 | 129. | 6.7 | 189. |
| 15 | .320 | 137. | 6.9 | 180. |
| 16 | .370 | 159. | 6.5 | 209. |
| 17 | .360 | 155. | 7.0 | 176. |
| 18 | .350 | 150. | 6.8 | 188. |
| 19 | .350 | 150. | 6.9 | 197. |
| 20 | .340 | 146. | 6.5 | 216. |
| 21 | .320 | 137. | 6.2 | 226. |
| 22 | .310 | 133. | 6.3 | 218. |
| 23 | .330 | 142. | 6.5 | 208. |
| 24 | .350 | 150. | 6.6 | 198. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 6.9 | 184. |

| | | | | |
|---|---|---|---|---|
| 2 | .330 | 142. | 7.2 | 169. |
| 3 | .360 | 155. | 7.2 | 168. |
| 4 | .330 | 142. | 7.2 | 169. |
| 5 | .350 | 150. | 7.2 | 161. |
| 6 | .390 | 168. | 7.6 | 150. |
| 7 | .330 | 142. | 7.1 | 178. |
| 8 | .350 | 150. | 6.3 | 230. |
| 9 | .350 | 150. | 6.3 | 218. |
| 10 | .340 | 146. | 6.4 | 221. |
| 11 | .350 | 150. | 6.6 | 213. |
| 12 | .300 | 129. | 6.6 | 176. |
| 13 | .350 | 150. | 7.2 | 164. |
| 14 | .340 | 146. | 7.3 | 164. |
| 15 | .330 | 142. | 7.0 | 180. |
| 16 | .330 | 142. | 7.2 | 178. |
| 17 | .370 | 159. | 7.3 | 166. |
| 18 | .380 | 163. | 7.4 | 156. |
| 19 | .340 | 146. | 6.7 | 183. |
| 20 | .360 | 155. | 6.4 | 230. |
| 21 | .370 | 159. | 6.6 | 209. |
| 22 | .330 | 142. | 6.5 | 203. |
| 23 | .360 | 155. | 7.2 | 172. |
| 24 | .390 | 168. | 7.6 | 153. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 7.5 | 149. |
| 2 | .390 | 168. | 7.5 | 149. |
| 3 | .340 | 146. | 7.3 | 148. |
| 4 | .280 | 120. | 7.4 | 149. |
| 5 | .270 | 116. | 7.5 | 149. |
| 6 | .270 | 116. | 7.6 | 149. |
| 7 | .270 | 116. | 7.5 | 151. |
| 8 | .360 | 155. | 7.0 | 189. |
| 9 | .370 | 159. | 6.6 | 209. |
| 10 | .430 | 185. | 6.3 | 248. |
| 11 | .420 | 180. | 5.8 | 270. |
| 12 | .410 | 176. | 5.9 | 263. |
| 13 | .350 | 150. | 6.2 | 223. |
| 14 | .330 | 142. | 6.3 | 213. |
| 15 | .340 | 146. | 7.0 | 178. |
| 16 | .270 | 116. | 7.3 | 149. |
| 17 | .270 | 116. | 7.5 | 148. |
| 18 | .270 | 116. | 7.4 | 150. |
| 19 | .310 | 133. | 6.8 | 190. |
| 20 | .350 | 150. | 6.2 | 225. |
| 21 | .350 | 150. | 6.7 | 190. |
| 22 | .340 | 146. | 7.1 | 178. |
| 23 | .310 | 133. | 7.1 | 161. |
| 24 | .250 | 107. | 7.4 | 152. |

DAY = 46

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .230 | 99. | 7.5 | 148. |
| 2 | .250 | 107. | 7.4 | 148. |
| 3 | .250 | 107. | 7.3 | 149. |
| 4 | .260 | 112. | 7.4 | 148. |
| 5 | .260 | 112. | 7.3 | 149. |
| 6 | .260 | 112. | 7.2 | 149. |
| 7 | .270 | 116. | 7.3 | 157. |
| 8 | .320 | 137. | 7.4 | 163. |
| 9 | .290 | 125. | 7.0 | 174. |
| 10 | .360 | 155. | 7.1 | 173. |
| 11 | .350 | 150. | 7.3 | 166. |
| 12 | .290 | 125. | 7.2 | 167. |
| 13 | .290 | 125. | 7.3 | 160. |
| 14 | .350 | 150. | 7.5 | 153. |
| 15 | .250 | 107. | 7.3 | 149. |
| 16 | .260 | 112. | 7.5 | 150. |
| 17 | .250 | 107. | 7.2 | 156. |
| 18 | .250 | 107. | 7.3 | 157. |
| 19 | .270 | 116. | 7.5 | 151. |
| 20 | .270 | 116. | 7.6 | 153. |
| 21 | .270 | 116. | 7.6 | 149. |
| 22 | .280 | 120. | 7.5 | 149. |
| 23 | .290 | 125. | 7.6 | 149. |
| 24 | .270 | 116. | 7.5 | 149. |

DAY # 47

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 7.7 | 149. |
| 2 | .280 | 120. | 7.6 | 149. |
| 3 | .280 | 120. | 7.6 | 149. |
| 4 | .260 | 112. | 7.6 | 149. |
| 5 | .250 | 107. | 7.4 | 149. |
| 6 | .270 | 116. | 7.7 | 149. |
| 7 | .300 | 129. | 7.6 | 155. |
| 8 | .360 | 155. | 7.4 | 160. |
| 9 | .350 | 150. | 7.5 | 155. |
| 10 | .330 | 142. | 7.3 | 166. |
| 11 | .280 | 120. | 6.8 | 198. |
| 12 | .320 | 137. | 6.2 | 242. |
| 13 | .330 | 142. | 6.4 | 224. |
| 14 | .320 | 137. | 6.2 | 220. |
| 15 | .320 | 137. | 6.4 | 223. |
| 16 | .330 | 142. | 6.3 | 217. |
| 17 | .330 | 142. | 6.3 | 210. |
| 18 | .350 | 150. | 6.4 | 207. |
| 19 | .330 | 142. | 6.3 | 210. |
| 20 | .300 | 129. | 5.8 | 252. |
| 21 | .300 | 129. | 5.9 | 252. |
| 22 | .320 | 137. | 6.2 | 223. |
| 23 | .320 | 137. | 6.4 | 203. |
| 24 | .360 | 155. | 7.3 | 157. |

DAY # 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .330 | 142. | 7.2 | 174. |
| 2 | .310 | 133. | 7.1 | 163. |
| 3 | .350 | 150. | 7.3 | 169. |
| 4 | .350 | 150. | 7.4 | 161. |
| 5 | .370 | 159. | 7.6 | 161. |
| 6 | .360 | 155. | 7.5 | 164. |
| 7 | .420 | 180. | 7.9 | 148. |
| 8 | .340 | 146. | 7.4 | 174. |
| 9 | .450 | 193. | 6.7 | 227. |
| 10 | .490 | 210. | 6.3 | 248. |
| 11 | .490 | 210. | 6.3 | 243. |
| 12 | .500 | 215. | 6.4 | 241. |
| 13 | .510 | 219. | 6.5 | 216. |
| 14 | .520 | 223. | 6.9 | 196. |
| 15 | .510 | 219. | 7.1 | 178. |
| 16 | .480 | 206. | 7.3 | 167. |
| 17 | .480 | 206. | 7.2 | 176. |
| 18 | .490 | 210. | 7.0 | 194. |
| 19 | .480 | 206. | 7.0 | 205. |
| 20 | .480 | 206. | 6.9 | 195. |
| 21 | .460 | 198. | 7.1 | 179. |
| 22 | .450 | 193. | 6.9 | 192. |
| 23 | .470 | 202. | 7.1 | 176. |
| 24 | .440 | 189. | 7.4 | 160. |

DAY = 53

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .520 | 223. | 7.3 | 167. |
| 2 | .500 | 215. | 7.2 | 165. |
| 3 | .520 | 223. | 7.5 | 163. |
| 4 | .490 | 210. | 7.4 | 166. |
| 5 | .480 | 206. | 7.3 | 166. |
| 6 | .460 | 198. | 7.2 | 174. |
| 7 | .480 | 206. | 7.3 | 164. |
| 8 | .460 | 198. | 7.3 | 177. |
| 9 | .480 | 206. | 6.8 | 209. |
| 10 | .430 | 185. | 6.4 | 226. |
| 11 | .420 | 180. | 6.4 | 210. |
| 12 | .450 | 193. | 6.8 | 196. |
| 13 | .440 | 189. | 6.8 | 197. |
| 14 | .440 | 189. | 7.0 | 181. |
| 15 | .480 | 206. | 7.3 | 170. |
| 16 | .410 | 176. | 7.3 | 157. |
| 17 | .400 | 172. | 7.5 | 161. |
| 18 | .440 | 189. | 7.1 | 176. |
| 19 | .420 | 180. | 7.1 | 173. |
| 20 | .410 | 176. | 6.7 | 199. |
| 21 | .400 | 172. | 6.9 | 190. |
| 22 | .400 | 172. | 7.2 | 175. |
| 23 | .370 | 159. | 7.2 | 175. |
| 24 | .330 | 142. | 7.3 | 169. |

DAY = 54

| | NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 7.3 | 166. |
| 2 | .340 | 146. | 7.1 | 173. |
| 3 | .340 | 146. | 7.3 | 168. |
| 4 | .330 | 142. | 7.1 | 172. |
| 5 | .350 | 150. | 7.1 | 176. |
| 6 | .420 | 180. | 7.4 | 162. |
| 7 | .370 | 159. | 7.0 | 187. |
| 8 | .500 | 215. | 6.7 | 211. |
| 9 | .400 | 172. | 6.5 | 234. |
| 10 | .350 | 150. | 6.1 | 245. |
| 11 | .370 | 159. | 5.7 | 256. |
| 12 | .440 | 189. | 5.9 | 258. |
| 13 | .450 | 193. | 6.0 | 237. |
| 14 | .460 | 198. | 6.0 | 237. |
| 15 | .430 | 185. | 6.0 | 235. |
| 16 | .450 | 193. | 6.1 | 226. |
| 17 | .440 | 189. | 6.4 | 201. |
| 18 | .450 | 193. | 6.5 | 201. |
| 19 | .450 | 193. | 6.6 | 203. |
| 20 | .430 | 185. | 6.0 | 233. |
| 21 | .500 | 215. | 6.5 | 210. |
| 22 | .450 | 193. | 6.2 | 226. |
| 23 | .400 | 172. | 6.3 | 206. |
| 24 | .410 | 176. | 6.9 | 176. |

DAY = 55

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 7.1 | 161. |
| 2 | .420 | 180. | 7.1 | 176. |
| 3 | .440 | 189. | 7.1 | 172. |
| 4 | .450 | 193. | 7.1 | 179. |
| 5 | .430 | 185. | 7.1 | 177. |
| 6 | .470 | 202. | 7.3 | 168. |
| 7 | .430 | 185. | 6.9 | 192. |
| 8 | .460 | 198. | 6.2 | 233. |
| 9 | .430 | 185. | 6.1 | 246. |
| 10 | .400 | 172. | 5.7 | 269. |
| 11 | .420 | 180. | 5.7 | 283. |
| 12 | .420 | 180. | 5.8 | 246. |
| 13 | .420 | 180. | 6.2 | 210. |
| 14 | .400 | 172. | 6.6 | 192. |
| 15 | .430 | 185. | 6.7 | 187. |
| 16 | .440 | 189. | 6.5 | 197. |
| 17 | .460 | 198. | 6.4 | 197. |
| 18 | .480 | 206. | 6.6 | 191. |
| 19 | .480 | 206. | 6.6 | 195. |
| 20 | .480 | 206. | 6.2 | 231. |
| 21 | .400 | 172. | 6.1 | 229. |
| 22 | .380 | 163. | 6.1 | 216. |
| 23 | .400 | 172. | 6.8 | 180. |
| 24 | .310 | 133. | 7.1 | 164. |

DAY = 56

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 6.8 | 184. |
| 2 | .430 | 185. | 6.8 | 183. |
| 3 | .430 | 185. | 6.9 | 184. |
| 4 | .420 | 180. | 6.9 | 183. |
| 5 | .400 | 172. | 6.9 | 184. |
| 6 | .410 | 176. | 6.9 | 183. |
| 7 | .380 | 163. | 6.9 | 184. |
| 8 | .350 | 150. | 6.7 | 196. |
| 9 | .390 | 168. | 6.6 | 204. |
| 10 | .370 | 159. | 6.6 | 202. |
| 11 | .410 | 176. | 6.4 | 203. |
| 12 | .380 | 163. | 6.4 | 204. |
| 13 | .370 | 159. | 6.9 | 205. |
| 14 | .470 | 202. | 7.3 | 173. |
| 15 | .440 | 189. | 6.8 | 193. |
| 16 | .430 | 185. | 6.7 | 194. |
| 17 | .420 | 180. | 7.1 | 185. |
| 18 | .400 | 172. | 6.7 | 188. |
| 19 | .360 | 155. | 7.2 | 172. |
| 20 | .410 | 176. | 6.8 | 177. |
| 21 | .410 | 176. | 6.7 | 185. |
| 22 | .460 | 198. | 6.8 | 180. |
| 23 | .450 | 193. | 6.9 | 179. |
| 24 | .350 | 150. | 7.1 | 163. |

DAY = 57



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 7.4 | 149. |
| 2 | .260 | 112. | 7.4 | 149. |
| 3 | .240 | 103. | 7.4 | 149. |
| 4 | .230 | 99. | 7.5 | 149. |
| 5 | .240 | 103. | 7.5 | 149. |
| 6 | .250 | 107. | 7.4 | 149. |
| 7 | .250 | 107. | 7.5 | 149. |
| 8 | .350 | 150. | 7.2 | 174. |
| 9 | .440 | 189. | 6.6 | 206. |
| 10 | .490 | 210. | 6.1 | 248. |
| 11 | .460 | 198. | 6.1 | 248. |
| 12 | .400 | 172. | 5.8 | 248. |
| 13 | .350 | 150. | 6.0 | 230. |
| 14 | .330 | 142. | 6.1 | 223. |
| 15 | .310 | 133. | 6.1 | 223. |
| 16 | .380 | 163. | 6.1 | 236. |
| 17 | .410 | 176. | 5.9 | 248. |
| 18 | .410 | 176. | 5.7 | 262. |
| 19 | .440 | 189. | 5.6 | 284. |
| 20 | .480 | 206. | 5.3 | 334. |
| 21 | .510 | 219. | 5.4 | 339. |
| 22 | .480 | 206. | 5.4 | 333. |
| 23 | .450 | 193. | 5.4 | 320. |
| 24 | .470 | 202. | 5.5 | 302. |

DAY = 58

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 5.8 | 242. |
| 2 | .410 | 176. | 6.0 | 228. |
| 3 | .340 | 146. | 6.4 | 201. |
| 4 | .350 | 150. | 6.5 | 198. |
| 5 | .380 | 163. | 6.6 | 199. |
| 6 | .420 | 180. | 6.4 | 226. |
| 7 | .390 | 168. | 5.8 | 261. |
| 8 | .440 | 189. | 5.6 | 287. |
| 9 | .380 | 163. | 5.4 | 314. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .480 | 206. | 5.5 | 339. |
| 12 | .460 | 198. | 5.5 | 336. |
| 13 | .460 | 198. | 5.4 | 335. |
| 14 | .450 | 193. | 5.5 | 336. |
| 15 | .440 | 189. | 5.4 | 335. |
| 16 | .440 | 189. | 5.4 | 335. |
| 17 | .450 | 193. | 5.5 | 336. |
| 18 | .460 | 198. | 5.4 | 335. |
| 19 | .450 | 193. | 5.4 | 334. |
| 20 | .450 | 193. | 5.5 | 336. |
| 21 | .460 | 198. | 5.5 | 334. |
| 22 | .290 | 125. | 5.7 | 271. |
| 23 | .290 | 125. | 6.6 | 216. |
| 24 | .330 | 142. | 7.2 | 193. |

DAY = 59



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .310 | 133. | 7.8 | 149. |
| 2 | .220 | 95. | 7.5 | 149. |
| 3 | .250 | 107. | 7.5 | 149. |
| 4 | .270 | 116. | 7.4 | 149. |
| 5 | .280 | 120. | 7.4 | 149. |
| 6 | .270 | 116. | 7.5 | 149. |
| 7 | .380 | 163. | 7.1 | 194. |
| 8 | .480 | 206. | 6.6 | 246. |
| 9 | .490 | 210. | 6.4 | 267. |
| 10 | .510 | 219. | 6.1 | 303. |
| 11 | .560 | 241. | 6.0 | 323. |
| 12 | .550 | 236. | 6.1 | 324. |
| 13 | .510 | 219. | 5.9 | 324. |
| 14 | .520 | 223. | 6.0 | 324. |
| 15 | .550 | 236. | 6.0 | 323. |
| 16 | .530 | 228. | 5.9 | 324. |
| 17 | .490 | 210. | 5.6 | 304. |
| 18 | .430 | 185. | 5.5 | 299. |
| 19 | .510 | 219. | 5.5 | 336. |
| 20 | .530 | 228. | 5.6 | 339. |
| 21 | .490 | 210. | 5.7 | 310. |
| 22 | .270 | 116. | 6.2 | 221. |
| 23 | .190 | 82. | 7.0 | 169. |
| 24 | .170 | 73. | 7.1 | 168. |

DAY = 60

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .210 | 90. | 7.0 | 169. |
| 2 | .210 | 90. | 7.0 | 169. |
| 3 | .260 | 112. | 6.8 | 199. |
| 4 | .250 | 107. | 6.4 | 218. |
| 5 | .250 | 107. | 6.5 | 218. |
| 6 | .270 | 116. | 6.4 | 218. |
| 7 | .270 | 116. | 6.4 | 218. |
| 8 | .320 | 137. | 6.4 | 224. |
| 9 | .350 | 150. | 6.2 | 230. |
| 10 | .370 | 159. | 6.0 | 244. |
| 11 | .330 | 142. | 6.0 | 248. |
| 12 | .310 | 133. | 6.0 | 248. |
| 13 | .300 | 129. | 5.9 | 247. |
| 14 | .380 | 163. | 5.7 | 279. |
| 15 | .440 | 189. | 5.6 | 323. |
| 16 | .430 | 185. | 5.6 | 317. |
| 17 | .450 | 193. | 5.6 | 296. |
| 18 | .430 | 185. | 5.5 | 288. |
| 19 | .410 | 176. | 5.7 | 273. |
| 20 | .390 | 168. | 5.7 | 273. |
| 21 | .390 | 168. | 5.7 | 273. |
| 22 | .370 | 159. | 5.8 | 255. |
| 23 | .370 | 159. | 6.8 | 189. |
| 24 | .280 | 120. | 7.4 | 149. |

DAY = 61



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .250 | 107. | 7.4 | 148. |
| 2 | .290 | 125. | 7.4 | 149. |
| 3 | .280 | 120. | 7.4 | 149. |
| 4 | .300 | 129. | 7.3 | 149. |
| 5 | .320 | 137. | 7.4 | 148. |
| 6 | .310 | 133. | 7.4 | 149. |
| 7 | .300 | 129. | 7.4 | 149. |
| 8 | .390 | 168. | 7.1 | 189. |
| 9 | .380 | 163. | 5.9 | 283. |
| 10 | .350 | 150. | 5.7 | 298. |
| 11 | .360 | 155. | 5.9 | 299. |
| 12 | .340 | 146. | 5.7 | 298. |
| 13 | .430 | 185. | 5.6 | 298. |
| 14 | .390 | 168. | 5.6 | 298. |
| 15 | .410 | 176. | 5.6 | 298. |
| 16 | .410 | 176. | 5.6 | 298. |
| 17 | .430 | 185. | 5.6 | 298. |
| 18 | .380 | 163. | 5.6 | 299. |
| 19 | .390 | 168. | 5.6 | 304. |
| 20 | .410 | 176. | 5.6 | 322. |
| 21 | .400 | 172. | 5.6 | 318. |
| 22 | .270 | 116. | 5.6 | 273. |
| 23 | .260 | 112. | 5.6 | 276. |
| 24 | .290 | 125. | 6.6 | 205. |

DAY = 62

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 7.0 | 183. |
| 2 | .300 | 129. | 6.9 | 184. |
| 3 | .280 | 120. | 6.8 | 183. |
| 4 | -1.000 | -430. | -1.0 | -1. |
| 5 | -1.000 | -430. | -1.0 | -1. |
| 6 | -1.000 | -430. | -1.0 | -1. |
| 7 | -1.000 | -430. | -1.0 | -1. |
| 8 | .290 | 125. | 6.1 | 198. |
| 9 | .350 | 150. | 6.6 | 207. |
| 10 | .300 | 129. | 5.7 | 279. |
| 11 | .290 | 125. | 5.5 | 298. |
| 12 | .290 | 125. | 5.4 | 298. |
| 13 | .280 | 120. | 5.4 | 298. |
| 14 | .300 | 129. | 5.5 | 298. |
| 15 | .330 | 142. | 5.4 | 298. |
| 16 | .300 | 129. | 5.4 | 299. |
| 17 | .330 | 142. | 5.5 | 283. |
| 18 | .340 | 146. | 5.5 | 278. |
| 19 | .350 | 150. | 5.4 | 298. |
| 20 | .390 | 168. | 5.4 | 315. |
| 21 | .360 | 155. | 5.4 | 319. |
| 22 | .330 | 142. | 5.4 | 316. |
| 23 | .330 | 142. | 5.6 | 312. |
| 24 | .270 | 116. | 6.1 | 237. |

DAY = 63



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .260 | 112. | 6.3 | 218. |
| 2 | .250 | 107. | 7.1 | 168. |
| 3 | .260 | 112. | 7.0 | 169. |
| 4 | .250 | 107. | 7.1 | 169. |
| 5 | .250 | 107. | 7.1 | 168. |
| 6 | .260 | 112. | 6.9 | 177. |
| 7 | .300 | 129. | 6.2 | 228. |
| 8 | .360 | 155. | 5.5 | 293. |
| 9 | .380 | 163. | 5.5 | 298. |
| 10 | .440 | 189. | 5.5 | 298. |
| 11 | .440 | 189. | 5.4 | 298. |
| 12 | .430 | 185. | 5.5 | 298. |
| 13 | .390 | 168. | 5.7 | 270. |
| 14 | .350 | 150. | 5.9 | 248. |
| 15 | .370 | 159. | 5.8 | 248. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .400 | 172. | 5.7 | 256. |
| 18 | .430 | 185. | 5.6 | 273. |
| 19 | .440 | 189. | 5.5 | 284. |
| 20 | .420 | 180. | 5.3 | 299. |
| 21 | .420 | 180. | 5.4 | 298. |
| 22 | .490 | 210. | 5.6 | 298. |
| 23 | .410 | 176. | 5.8 | 278. |
| 24 | .370 | 159. | 6.0 | 245. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.3 | 206. |
| 2 | .320 | 137. | 7.1 | 167. |
| 3 | .320 | 137. | 7.2 | 159. |
| 4 | .330 | 142. | 7.4 | 159. |
| 5 | .310 | 133. | 7.3 | 158. |
| 6 | .300 | 129. | 7.3 | 159. |
| 7 | .300 | 129. | 7.0 | 177. |
| 8 | .320 | 137. | 6.2 | 250. |
| 9 | .380 | 163. | 5.7 | 286. |
| 10 | .460 | 198. | 5.8 | 294. |
| 11 | .460 | 198. | 5.7 | 273. |
| 12 | .460 | 198. | 5.8 | 263. |
| 13 | .460 | 198. | 5.9 | 260. |
| 14 | .410 | 176. | 6.0 | 238. |
| 15 | .360 | 155. | 6.1 | 238. |
| 16 | .370 | 159. | 6.1 | 238. |
| 17 | .380 | 163. | 6.0 | 238. |
| 18 | .440 | 189. | 6.0 | 249. |
| 19 | .390 | 168. | 5.7 | 273. |
| 20 | .490 | 210. | 5.6 | 294. |
| 21 | .490 | 210. | 5.7 | 298. |
| 22 | .420 | 180. | 5.6 | 298. |
| 23 | .390 | 168. | 6.0 | 250. |
| 24 | .340 | 146. | 6.9 | 175. |

DAY = 65



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 7.1 | 173. |
| 2 | .300 | 129. | 7.1 | 174. |
| 3 | .320 | 137. | 7.2 | 174. |
| 4 | .350 | 150. | 7.1 | 173. |
| 5 | .350 | 150. | 6.9 | 174. |
| 6 | .350 | 150. | 7.1 | 174. |
| 7 | .360 | 155. | 7.1 | 178. |
| 8 | .450 | 193. | 6.2 | 251. |
| 9 | .430 | 185. | 5.8 | 272. |
| 10 | .420 | 180. | 5.8 | 275. |
| 11 | .510 | 219. | 5.8 | 275. |
| 12 | .490 | 210. | 5.9 | 276. |
| 13 | .460 | 198. | 5.7 | 275. |
| 14 | .490 | 210. | 5.8 | 275. |
| 15 | .540 | 232. | 5.8 | 275. |
| 16 | .520 | 223. | 5.8 | 276. |
| 17 | .520 | 223. | 5.8 | 275. |
| 18 | .520 | 223. | 5.8 | 275. |
| 19 | .510 | 219. | 5.8 | 282. |
| 20 | .560 | 241. | 5.5 | 315. |
| 21 | .480 | 206. | 5.6 | 290. |
| 22 | .460 | 198. | 5.7 | 273. |
| 23 | .410 | 176. | 6.1 | 248. |
| 24 | .360 | 155. | 6.8 | 187. |

DAY = 66

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 7.0 | 173. |
| 2 | .370 | 159. | 7.2 | 174. |
| 3 | .270 | 116. | 7.4 | 152. |
| 4 | .280 | 120. | 7.5 | 149. |
| 5 | .300 | 129. | 7.5 | 149. |
| 6 | .350 | 150. | 7.5 | 154. |
| 7 | .390 | 168. | 7.1 | 168. |
| 8 | .420 | 180. | 7.0 | 190. |
| 9 | .460 | 198. | 5.9 | 269. |
| 10 | .450 | 193. | 5.5 | 324. |
| 11 | .550 | 236. | 5.6 | 329. |
| 12 | .500 | 215. | 5.5 | 329. |
| 13 | .460 | 198. | 5.4 | 305. |
| 14 | .450 | 193. | 5.5 | 294. |
| 15 | .450 | 193. | 5.8 | 257. |
| 16 | .480 | 206. | 6.0 | 248. |
| 17 | .460 | 198. | 6.0 | 248. |
| 18 | .470 | 202. | 6.0 | 248. |
| 19 | .460 | 198. | 5.8 | 266. |
| 20 | .450 | 193. | 5.8 | 273. |
| 21 | .440 | 189. | 5.8 | 272. |
| 22 | .440 | 189. | 5.8 | 273. |
| 23 | .400 | 172. | 5.9 | 256. |
| 24 | .420 | 180. | 6.6 | 215. |

DAY = 67



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 7.5 | 156. |
| 2 | .420 | 180. | 7.7 | 149. |
| 3 | .420 | 180. | 7.5 | 149. |
| 4 | .450 | 193. | 7.7 | 148. |
| 5 | .450 | 193. | 7.8 | 149. |
| 6 | .420 | 180. | 7.7 | 152. |
| 7 | .380 | 163. | 7.2 | 183. |
| 8 | .360 | 155. | 6.9 | 201. |
| 9 | .430 | 185. | 6.4 | 241. |
| 10 | .450 | 193. | 5.8 | 295. |
| 11 | .460 | 198. | 5.7 | 322. |
| 12 | .460 | 198. | 5.7 | 322. |
| 13 | .430 | 185. | 5.5 | 322. |
| 14 | .480 | 206. | 5.6 | 309. |
| 15 | .450 | 193. | 5.7 | 284. |
| 16 | .400 | 172. | 5.7 | 262. |
| 17 | .380 | 163. | 6.0 | 248. |
| 18 | .380 | 163. | 6.0 | 247. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .390 | 168. | 5.7 | 273. |
| 22 | .400 | 172. | 5.8 | 272. |
| 23 | .380 | 163. | 6.0 | 255. |
| 24 | .350 | 150. | 6.8 | 189. |

DAY = 68

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 7.7 | 156. |
| 2 | .250 | 107. | 7.3 | 148. |
| 3 | .280 | 120. | 7.6 | 149. |
| 4 | .270 | 116. | 7.6 | 149. |
| 5 | .270 | 116. | 7.6 | 149. |
| 6 | .340 | 146. | 7.4 | 165. |
| 7 | .370 | 159. | 6.8 | 210. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | .360 | 155. | 5.9 | 262. |
| 10 | .370 | 159. | 5.6 | 320. |
| 11 | .420 | 180. | 5.5 | 204. |
| 12 | .440 | 189. | 5.4 | 73. |
| 13 | .430 | 185. | 5.5 | 296. |
| 14 | .430 | 185. | 5.5 | 249. |
| 15 | .460 | 198. | 5.5 | 298. |
| 16 | .480 | 206. | 5.4 | 298. |
| 17 | .460 | 198. | 5.4 | 298. |
| 18 | .460 | 198. | 5.4 | 298. |
| 19 | .510 | 219. | 5.5 | 298. |
| 20 | .480 | 206. | 5.4 | 299. |
| 21 | .440 | 189. | 5.4 | 298. |
| 22 | .400 | 172. | 5.4 | 298. |
| 23 | .390 | 168. | 5.7 | 273. |
| 24 | .340 | 146. | 6.3 | 213. |

DAY = 69



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 7.4 | 155. |
| 2 | .240 | 103. | 7.4 | 153. |
| 3 | .310 | 133. | 7.5 | 162. |
| 4 | .330 | 142. | 7.1 | 177. |
| 5 | .270 | 116. | 6.9 | 187. |
| 6 | .340 | 146. | 6.9 | 188. |
| 7 | .270 | 116. | 6.9 | 189. |
| 8 | .320 | 137. | 7.0 | 188. |
| 9 | .260 | 112. | 6.9 | 189. |
| 10 | .340 | 146. | 6.9 | 195. |
| 11 | .360 | 155. | 5.7 | 264. |
| 12 | .370 | 159. | 5.7 | 276. |
| 13 | .370 | 159. | 6.1 | 132. |
| 14 | .370 | 159. | 6.4 | 142. |
| 15 | .360 | 155. | 6.3 | 225. |
| 16 | .370 | 159. | 6.3 | 225. |
| 17 | .370 | 159. | 6.3 | 225. |
| 18 | .370 | 159. | 6.4 | 225. |
| 19 | .440 | 189. | 6.0 | 256. |
| 20 | .460 | 198. | 5.5 | 292. |
| 21 | .460 | 198. | 5.5 | 300. |
| 22 | .460 | 198. | 5.6 | 301. |
| 23 | .460 | 198. | 5.6 | 300. |
| 24 | .480 | 206. | 5.6 | 299. |

DAY = 71

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 6.0 | 252. |
| 2 | .300 | 129. | 6.1 | 229. |
| 3 | .340 | 146. | 6.2 | 235. |
| 4 | .340 | 146. | 6.2 | 234. |
| 5 | .350 | 150. | 6.6 | 202. |
| 6 | .370 | 159. | 7.1 | 175. |
| 7 | .360 | 155. | 7.2 | 175. |
| 8 | .360 | 155. | 7.0 | 191. |
| 9 | .360 | 155. | 6.8 | 199. |
| 10 | .370 | 159. | 6.8 | 200. |
| 11 | .340 | 146. | 6.6 | 201. |
| 12 | .350 | 150. | 6.3 | 226. |
| 13 | .340 | 146. | 6.1 | 232. |
| 14 | .340 | 146. | 6.1 | 229. |
| 15 | .330 | 142. | 6.3 | 221. |
| 16 | .300 | 129. | 5.9 | 239. |
| 17 | .300 | 129. | 5.6 | 251. |
| 18 | .280 | 120. | 5.5 | 250. |
| 19 | .290 | 125. | 5.4 | 265. |
| 20 | .340 | 146. | 5.4 | 299. |
| 21 | .470 | 202. | 5.5 | 313. |
| 22 | .480 | 206. | 5.4 | 328. |
| 23 | .380 | 163. | 5.4 | 326. |
| 24 | .320 | 137. | 6.1 | 254. |

DAY = 73



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .240 | 103. | 7.3 | 150. |
| 2 | .270 | 116. | 7.4 | 151. |
| 3 | .310 | 133. | 7.4 | 156. |
| 4 | .340 | 146. | 6.6 | 219. |
| 5 | .330 | 142. | 6.2 | 241. |
| 6 | .310 | 133. | 6.0 | 245. |
| 7 | .300 | 129. | 6.0 | 246. |
| 8 | .290 | 125. | 5.6 | 280. |
| 9 | .400 | 172. | 5.6 | 318. |
| 10 | .410 | 176. | 5.4 | 326. |
| 11 | .410 | 176. | 5.3 | 326. |
| 12 | .380 | 163. | 5.3 | 324. |
| 13 | .380 | 163. | 5.1 | 318. |
| 14 | .350 | 150. | 5.1 | 313. |
| 15 | .340 | 146. | 5.2 | 294. |
| 16 | .310 | 133. | 5.3 | 265. |
| 17 | .340 | 146. | 5.3 | 264. |
| 18 | .350 | 150. | 5.3 | 273. |
| 19 | .340 | 146. | 5.2 | 281. |
| 20 | .400 | 172. | 5.1 | 295. |
| 21 | .360 | 155. | 5.2 | 284. |
| 22 | .330 | 142. | 5.3 | 271. |
| 23 | .360 | 155. | 5.4 | 268. |
| 24 | .310 | 133. | 5.7 | 242. |

DAY = 74

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .270 | 116. | 6.1 | 211. |
| 2 | .310 | 133. | 6.7 | 189. |
| 3 | .320 | 137. | 7.1 | 175. |
| 4 | .330 | 142. | 7.3 | 165. |
| 5 | .350 | 150. | 7.3 | 159. |
| 6 | .260 | 112. | 7.4 | 154. |
| 7 | .310 | 133. | 7.1 | 177. |
| 8 | .290 | 125. | 6.6 | 207. |
| 9 | .290 | 125. | 5.8 | 247. |
| 10 | .260 | 112. | 5.6 | 255. |
| 11 | .250 | 107. | 5.5 | 259. |
| 12 | .250 | 107. | 5.7 | 244. |
| 13 | .250 | 107. | 5.7 | 237. |
| 14 | .270 | 116. | 5.9 | 225. |
| 15 | .290 | 125. | 6.2 | 206. |
| 16 | .310 | 133. | 6.4 | 200. |
| 17 | .280 | 120. | 6.2 | 204. |
| 18 | .300 | 129. | 6.2 | 223. |
| 19 | .270 | 116. | 5.6 | 246. |
| 20 | .300 | 129. | 4.9 | 311. |
| 21 | .290 | 125. | 4.8 | 315. |
| 22 | .280 | 120. | 4.8 | 297. |
| 23 | .310 | 133. | 5.5 | 239. |
| 24 | .260 | 112. | 7.0 | 168. |

DAY = 75

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .230 | 99. | 7.3 | 150. |
| 2 | .260 | 112. | 7.4 | 151. |
| 3 | .260 | 112. | 7.5 | 150. |
| 4 | .250 | 107. | 7.3 | 150. |
| 5 | .250 | 107. | 7.4 | 150. |
| 6 | .250 | 107. | 7.5 | 152. |
| 7 | .280 | 120. | 7.5 | 158. |
| 8 | .280 | 120. | 6.2 | 231. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .330 | 142. | 5.5 | 326. |
| 12 | .470 | 202. | 5.3 | 328. |
| 13 | .450 | 193. | 5.0 | 326. |
| 14 | .540 | 232. | 5.1 | 326. |
| 15 | .560 | 241. | 5.1 | 324. |
| 16 | .550 | 236. | 5.1 | 325. |
| 17 | .540 | 232. | 4.9 | 320. |
| 18 | .540 | 232. | 4.8 | 319. |
| 19 | .530 | 228. | 4.7 | 328. |
| 20 | .500 | 215. | 4.7 | 327. |
| 21 | .460 | 198. | 4.8 | 325. |
| 22 | .480 | 206. | 4.7 | 323. |
| 23 | .460 | 198. | 4.8 | 297. |
| 24 | .420 | 180. | 5.2 | 243. |

DAY = 76

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 5.3 | 245. |
| 2 | .400 | 172. | 6.1 | 208. |
| 3 | .360 | 155. | 7.0 | 151. |
| 4 | .340 | 146. | 7.1 | 150. |
| 5 | .400 | 172. | 7.0 | 159. |
| 6 | .400 | 172. | 6.5 | 188. |
| 7 | .350 | 150. | 5.4 | 261. |
| 8 | .410 | 176. | 4.8 | 305. |
| 9 | .440 | 189. | 4.9 | 300. |
| 10 | .470 | 202. | 5.1 | 282. |
| 11 | .370 | 159. | 4.9 | 298. |
| 12 | .420 | 180. | 4.7 | 324. |
| 13 | .440 | 189. | 4.8 | 311. |
| 14 | .400 | 172. | 5.0 | 284. |
| 15 | .410 | 176. | 5.1 | 269. |
| 16 | .410 | 176. | 5.3 | 259. |
| 17 | .380 | 163. | 5.4 | 239. |
| 18 | .410 | 176. | 5.7 | 248. |
| 19 | .440 | 189. | 5.3 | 271. |
| 20 | .500 | 215. | 5.1 | 296. |
| 21 | .470 | 202. | 5.0 | 294. |
| 22 | .470 | 202. | 5.2 | 286. |
| 23 | .420 | 180. | 5.3 | 270. |
| 24 | .340 | 146. | 5.8 | 224. |

DAY = 77



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .340 | 146. | 6.3 | 202. |
| 2 | .330 | 142. | 6.6 | 190. |
| 3 | .330 | 142. | 7.0 | 186. |
| 4 | .310 | 133. | 7.0 | 184. |
| 5 | .320 | 137. | 7.0 | 183. |
| 6 | .300 | 129. | 6.7 | 197. |
| 7 | .380 | 163. | 6.3 | 225. |
| 8 | .390 | 168. | 5.6 | 273. |
| 9 | .560 | 241. | 5.7 | 319. |
| 10 | .630 | 271. | 5.9 | 327. |
| 11 | .580 | 249. | 5.8 | 326. |
| 12 | .540 | 232. | 5.7 | 325. |
| 13 | .520 | 223. | 5.7 | 299. |
| 14 | .530 | 228. | 5.7 | 291. |
| 15 | .570 | 245. | 6.0 | 296. |
| 16 | .580 | 249. | 5.4 | 312. |
| 17 | .540 | 232. | 5.3 | 319. |
| 18 | .510 | 219. | 5.3 | 320. |
| 19 | .520 | 223. | 5.2 | 320. |
| 20 | .550 | 236. | 5.1 | 326. |
| 21 | .490 | 210. | 5.1 | 324. |
| 22 | .480 | 206. | 5.2 | 321. |
| 23 | .460 | 198. | 5.4 | 305. |
| 24 | .440 | 189. | 5.4 | 275. |

DAY = 78

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 6.1 | 230. |
| 2 | .400 | 172. | 6.5 | 213. |
| 3 | .380 | 163. | 6.6 | 216. |
| 4 | .390 | 168. | 6.6 | 219. |
| 5 | .390 | 168. | 6.5 | 215. |
| 6 | .480 | 206. | 6.4 | 236. |
| 7 | .430 | 185. | 6.3 | 232. |
| 8 | .550 | 236. | 5.7 | 296. |
| 9 | .670 | 288. | 5.3 | 326. |
| 10 | .660 | 284. | 5.2 | 326. |
| 11 | .620 | 266. | 5.1 | 327. |
| 12 | .610 | 262. | 5.1 | 326. |
| 13 | .600 | 258. | 5.1 | 324. |
| 14 | .620 | 266. | 5.1 | 326. |
| 15 | .600 | 258. | 5.5 | 326. |
| 16 | .590 | 253. | 5.8 | 324. |
| 17 | .680 | 292. | 5.7 | 321. |
| 18 | .740 | 318. | 5.7 | 316. |
| 19 | .690 | 296. | 5.6 | 322. |
| 20 | .710 | 305. | 5.6 | 328. |
| 21 | .650 | 279. | 5.7 | 325. |
| 22 | .680 | 292. | 5.8 | 321. |
| 23 | .630 | 271. | 5.8 | 315. |
| 24 | .560 | 241. | 6.2 | 274. |

DAY = 80



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .570 | 245. | 6.7 | 212. |
| 2 | .460 | 198. | 7.4 | 175. |
| 3 | .440 | 189. | 7.4 | 176. |
| 4 | .460 | 198. | 7.4 | 175. |
| 5 | .440 | 189. | 7.2 | 179. |
| 6 | .440 | 189. | 6.9 | 209. |
| 7 | .520 | 223. | 6.7 | 227. |
| 8 | .590 | 253. | 6.2 | 272. |
| 9 | .650 | 279. | 6.1 | 313. |
| 10 | .620 | 266. | 6.0 | 325. |
| 11 | .670 | 288. | 6.0 | 326. |
| 12 | .680 | 292. | 6.1 | 325. |
| 13 | .660 | 284. | 6.0 | 325. |
| 14 | .630 | 271. | 6.1 | 326. |
| 15 | .660 | 284. | 6.1 | 325. |
| 16 | .620 | 266. | 6.1 | 325. |
| 17 | .600 | 258. | 6.0 | 326. |
| 18 | .680 | 292. | 6.2 | 327. |
| 19 | .640 | 275. | 6.1 | 327. |
| 20 | .650 | 279. | 6.1 | 326. |
| 21 | .570 | 245. | 5.6 | 324. |
| 22 | .630 | 271. | 5.6 | 327. |
| 23 | .630 | 271. | 5.6 | 319. |
| 24 | .450 | 193. | 5.9 | 239. |

DAY = 81

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.4 | 200. |
| 2 | .330 | 142. | 6.3 | 210. |
| 3 | .350 | 150. | 6.3 | 219. |
| 4 | .350 | 150. | 6.4 | 209. |
| 5 | .330 | 142. | 6.5 | 202. |
| 6 | .330 | 142. | 6.5 | 209. |
| 7 | .400 | 172. | 6.4 | 224. |
| 8 | .470 | 202. | 6.0 | 256. |
| 9 | .610 | 262. | 5.9 | 314. |
| 10 | .590 | 253. | 6.0 | 325. |
| 11 | .600 | 258. | 5.9 | 324. |
| 12 | .590 | 253. | 6.0 | 324. |
| 13 | .590 | 253. | 5.9 | 322. |
| 14 | .580 | 249. | 5.8 | 324. |
| 15 | .580 | 249. | 5.9 | 324. |
| 16 | .550 | 236. | 5.9 | 316. |
| 17 | .560 | 241. | 5.9 | 307. |
| 18 | .620 | 266. | 5.8 | 322. |
| 19 | .620 | 266. | 5.8 | 326. |
| 20 | .630 | 271. | 5.8 | 326. |
| 21 | .600 | 258. | 5.9 | 324. |
| 22 | .610 | 262. | 5.9 | 323. |
| 23 | .630 | 271. | 5.8 | 322. |
| 24 | .540 | 232. | 6.1 | 278. |

DAY = 82



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 6.8 | 187. |
| 2 | .280 | 120. | 7.8 | 151. |
| 3 | .280 | 120. | 7.5 | 150. |
| 4 | .270 | 116. | 7.5 | 150. |
| 5 | .270 | 116. | 7.7 | 150. |
| 6 | .330 | 142. | 7.6 | 166. |
| 7 | .500 | 215. | 6.2 | 290. |
| 8 | .600 | 258. | 5.9 | 326. |
| 9 | .550 | 236. | 6.0 | 300. |
| 10 | .500 | 215. | 5.7 | 333. |
| 11 | .500 | 215. | 5.8 | 335. |
| 12 | .580 | 249. | 5.9 | 334. |
| 13 | .500 | 215. | 6.0 | 328. |
| 14 | .480 | 206. | 6.0 | 326. |
| 15 | .490 | 210. | 5.9 | 326. |
| 16 | .490 | 210. | 5.9 | 326. |
| 17 | .530 | 228. | 5.9 | 327. |
| 18 | .520 | 223. | 5.8 | 326. |
| 19 | .530 | 228. | 5.9 | 323. |
| 20 | .600 | 258. | 5.8 | 332. |
| 21 | .560 | 241. | 5.9 | 323. |
| 22 | .560 | 241. | 5.9 | 329. |
| 23 | .600 | 258. | 5.9 | 324. |
| 24 | .570 | 245. | 5.9 | 324. |

DAY = 83

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .580 | 249. | 5.9 | 326. |
| 2 | .580 | 249. | 5.9 | 326. |
| 3 | .540 | 232. | 6.0 | 325. |
| 4 | .500 | 215. | 5.9 | 326. |
| 5 | .630 | 271. | 6.0 | 326. |
| 6 | .650 | 279. | 6.0 | 327. |
| 7 | .620 | 266. | 6.0 | 325. |
| 8 | .610 | 262. | 5.9 | 323. |
| 9 | .570 | 245. | 6.0 | 320. |
| 10 | .570 | 245. | 5.9 | 323. |
| 11 | .590 | 253. | 5.9 | 327. |
| 12 | .580 | 249. | 5.8 | 326. |
| 13 | .570 | 245. | 5.8 | 326. |
| 14 | .500 | 215. | 5.9 | 326. |
| 15 | .460 | 198. | 5.8 | 326. |
| 16 | .510 | 219. | 5.9 | 326. |
| 17 | .580 | 249. | 5.9 | 326. |
| 18 | .550 | 236. | 5.8 | 327. |
| 19 | .530 | 228. | 5.8 | 326. |
| 20 | .590 | 253. | 5.9 | 327. |
| 21 | .610 | 262. | 5.8 | 325. |
| 22 | .590 | 253. | 5.8 | 315. |
| 23 | .600 | 258. | 5.8 | 184. |
| 24 | .620 | 266. | 5.9 | 231. |

DAY = 84



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .630 | 271. | 5.8 | 61. |
| 2 | .590 | 253. | 5.8 | 183. |
| 3 | .630 | 271. | 5.8 | 126. |
| 4 | .630 | 271. | 5.8 | 187. |
| 5 | .620 | 266. | 5.9 | 146. |
| 6 | .620 | 266. | 5.9 | 214. |
| 7 | .490 | 210. | 3.1 | 150. |
| 8 | .660 | 284. | 6.0 | 137. |
| 9 | .640 | 275. | 6.0 | 325. |
| 10 | .640 | 275. | 5.9 | 329. |
| 11 | .680 | 292. | 5.5 | 350. |
| 12 | .580 | 249. | 5.1 | 348. |
| 13 | .590 | 253. | 5.6 | 344. |
| 14 | .630 | 271. | 5.8 | 342. |
| 15 | .620 | 266. | 5.5 | 340. |
| 16 | .560 | 241. | 5.5 | 339. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .530 | 228. | 5.5 | 344. |
| 21 | .580 | 249. | 5.4 | 339. |
| 22 | .670 | 288. | 5.4 | 322. |
| 23 | .570 | 245. | 5.4 | 330. |
| 24 | .480 | 206. | 5.8 | 291. |

DAY = 86

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .320 | 137. | 6.8 | 168. |
| 2 | .400 | 172. | 5.9 | 243. |
| 3 | .480 | 206. | 5.5 | 308. |
| 4 | .500 | 215. | 5.4 | 325. |
| 5 | .480 | 206. | 5.4 | 326. |
| 6 | .490 | 210. | 5.4 | 327. |
| 7 | .500 | 215. | 5.4 | 329. |
| 8 | .510 | 219. | 5.4 | 329. |
| 9 | .510 | 219. | 5.4 | 326. |
| 10 | .510 | 219. | 5.4 | 327. |
| 11 | .460 | 198. | 5.6 | 326. |
| 12 | .480 | 206. | 5.6 | 326. |
| 13 | .480 | 206. | 5.2 | 320. |
| 14 | .430 | 185. | 5.1 | 328. |
| 15 | .420 | 180. | 5.3 | 327. |
| 16 | .430 | 185. | 5.4 | 326. |
| 17 | .470 | 202. | 5.4 | 326. |
| 18 | .510 | 219. | 5.4 | 327. |
| 19 | .490 | 210. | 5.3 | 326. |
| 20 | .490 | 210. | 5.3 | 327. |
| 21 | .490 | 210. | 5.4 | 325. |
| 22 | .420 | 180. | 5.4 | 324. |
| 23 | .420 | 180. | 5.4 | 325. |
| 24 | .440 | 189. | 5.5 | 326. |

DAY = 87



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 5.5 | 316. |
| 2 | .420 | 180. | 5.6 | 302. |
| 3 | .340 | 146. | 5.7 | 250. |
| 4 | .340 | 146. | 6.6 | 203. |
| 5 | .340 | 146. | 6.6 | 200. |
| 6 | .390 | 168. | 6.2 | 243. |
| 7 | .410 | 176. | 5.7 | 310. |
| 8 | .430 | 185. | 5.6 | 317. |
| 9 | .480 | 206. | 5.6 | 320. |
| 10 | .540 | 232. | 5.5 | 327. |
| 11 | .520 | 223. | 5.5 | 325. |
| 12 | .560 | 241. | 5.6 | 326. |
| 13 | .570 | 245. | 5.6 | 324. |
| 14 | .520 | 223. | 5.5 | 325. |
| 15 | .510 | 219. | 5.5 | 324. |
| 16 | .540 | 232. | 5.6 | 324. |
| 17 | .560 | 241. | 5.6 | 326. |
| 18 | .600 | 258. | 5.6 | 326. |
| 19 | .620 | 266. | 5.5 | 325. |
| 20 | .570 | 245. | 5.5 | 326. |
| 21 | .530 | 228. | 5.6 | 324. |
| 22 | .540 | 232. | 5.6 | 326. |
| 23 | .540 | 232. | 5.6 | 324. |
| 24 | .520 | 223. | 5.8 | 310. |

DAY = 88

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 6.7 | 242. |
| 2 | .390 | 168. | 6.7 | 217. |
| 3 | .390 | 168. | 7.5 | 170. |
| 4 | .360 | 155. | 7.5 | 177. |
| 5 | .350 | 150. | 7.2 | 199. |
| 6 | .390 | 168. | 7.0 | 229. |
| 7 | .350 | 150. | 6.5 | 253. |
| 8 | .430 | 185. | 6.2 | 296. |
| 9 | .440 | 189. | 6.1 | 308. |
| 10 | .440 | 189. | 6.1 | 316. |
| 11 | .470 | 202. | 6.0 | 316. |
| 12 | .430 | 185. | 6.0 | 316. |
| 13 | .420 | 180. | 5.9 | 316. |
| 14 | .420 | 180. | 5.9 | 315. |
| 15 | .430 | 185. | 5.8 | 315. |
| 16 | .440 | 189. | 5.9 | 316. |
| 17 | .440 | 189. | 6.0 | 316. |
| 18 | .470 | 202. | 6.0 | 316. |
| 19 | .470 | 202. | 6.0 | 316. |
| 20 | .490 | 210. | 6.0 | 319. |
| 21 | .500 | 215. | 6.1 | 315. |
| 22 | .470 | 202. | 6.0 | 316. |
| 23 | .440 | 189. | 6.0 | 315. |
| 24 | .430 | 185. | 6.0 | 309. |

DAY = 89



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 6.2 | 269. |
| 2 | .370 | 159. | 6.6 | 247. |
| 3 | .400 | 172. | 6.7 | 238. |
| 4 | .370 | 159. | 6.8 | 235. |
| 5 | .390 | 168. | 6.6 | 244. |
| 6 | .370 | 159. | 6.5 | 251. |
| 7 | .380 | 163. | 6.5 | 252. |
| 8 | .370 | 159. | 6.1 | 312. |
| 9 | .510 | 219. | 6.0 | 335. |
| 10 | .550 | 236. | 6.0 | 325. |
| 11 | .490 | 210. | 5.9 | 325. |
| 12 | .550 | 236. | 6.0 | 333. |
| 13 | .510 | 219. | 5.9 | 337. |
| 14 | .600 | 258. | 5.9 | 338. |
| 15 | .630 | 271. | 5.9 | 338. |
| 16 | .610 | 262. | 5.9 | 337. |
| 17 | .590 | 253. | 5.8 | 336. |
| 18 | .630 | 271. | 5.9 | 335. |
| 19 | .600 | 258. | 5.9 | 335. |
| 20 | .600 | 258. | 5.9 | 336. |
| 21 | .580 | 249. | 4.9 | 335. |
| 22 | .600 | 258. | 6.0 | 335. |
| 23 | .580 | 249. | 5.9 | 335. |
| 24 | .600 | 258. | 5.9 | 336. |

DAY = 90

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .650 | 279. | 5.9 | 335. |
| 2 | .690 | 296. | 5.9 | 335. |
| 3 | .700 | 301. | 6.0 | 335. |
| 4 | .590 | 253. | 6.0 | 336. |
| 5 | .560 | 241. | 6.0 | 335. |
| 6 | .570 | 245. | 6.1 | 337. |
| 7 | .620 | 266. | 6.0 | 337. |
| 8 | .620 | 266. | 6.0 | 337. |
| 9 | .600 | 258. | 6.1 | 337. |
| 10 | .700 | 301. | 6.1 | 337. |
| 11 | .720 | 309. | 6.0 | 343. |
| 12 | .720 | 309. | 5.7 | 347. |
| 13 | .630 | 271. | 5.1 | 341. |
| 14 | .590 | 253. | 5.2 | 343. |
| 15 | .560 | 241. | 5.2 | 342. |
| 16 | .580 | 249. | 5.1 | 343. |
| 17 | .590 | 253. | 5.2 | 342. |
| 18 | .620 | 266. | 5.1 | 344. |
| 19 | .570 | 245. | 5.2 | 344. |
| 20 | .610 | 262. | 5.1 | 344. |
| 21 | .600 | 258. | 5.0 | 345. |
| 22 | .640 | 275. | 5.1 | 344. |
| 23 | .570 | 245. | 5.1 | 344. |
| 24 | .540 | 232. | 5.1 | 344. |

APPENDIX M

PUBLIC SERVICE COMPANY OF NEW MEXICO

SAN JUAN PLANT

UNIT 1

Input Data

**PULVERIZED COAL-FIRED UTILITY BOILER NOX EMISSION MONITORING**

PUB. SERV. NEW MEXICO SAN JUAN PLANT UNIT 1

FOSTER WHEELER BOILER -OVERFIRE AIR AND DUAL REG. BRNS 360 MWE GROSS

PERFORM. NOX=0.627 LB/10**6BTU (270 NG/J). REDUCED TO 0.35 LB/10**6BTU

(151 NG/J) FOR STATE COMPLIANCE. SUBBITUMINOUS COAL

NOX MONITOR RELATIVE ACCURACY = 10.5 PC

DAY 1 = 1 JANUARY 1981

**INPUT DATA**

DAY = 1

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 9.8 | 217. |
| 2 | .290 | 125. | 11.3 | 209. |
| 3 | .290 | 125. | 11.3 | 206. |
| 4 | .270 | 116. | 9.7 | 214. |
| 5 | .330 | 142. | 8.8 | 229. |
| 6 | .550 | 236. | 9.3 | 235. |
| 7 | .480 | 206. | 10.1 | 236. |
| 8 | .290 | 125. | 9.9 | 242. |
| 9 | .350 | 150. | 9.7 | 270. |
| 10 | .340 | 146. | 9.6 | 272. |
| 11 | .340 | 146. | 9.5 | 272. |
| 12 | .350 | 150. | 9.3 | 285. |
| 13 | .350 | 150. | 8.4 | 291. |
| 14 | .350 | 150. | 7.1 | 291. |
| 15 | .350 | 150. | 7.1 | 294. |
| 16 | .360 | 155. | 7.1 | 291. |
| 17 | .340 | 146. | 7.0 | 292. |
| 18 | .350 | 150. | 6.9 | 301. |
| 19 | .380 | 163. | 6.9 | 331. |
| 20 | .390 | 168. | 7.0 | 331. |
| 21 | .380 | 163. | 7.0 | 332. |
| 22 | .380 | 163. | 7.0 | 332. |
| 23 | .380 | 163. | 7.0 | 329. |
| 24 | .400 | 172. | 7.9 | 279. |

DAY = 2

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 8.2 | 250. |
| 2 | .400 | 172. | 8.2 | 250. |
| 3 | .400 | 172. | 8.2 | 249. |
| 4 | .430 | 185. | 8.1 | 250. |
| 5 | .380 | 163. | 7.9 | 253. |
| 6 | .370 | 159. | 7.9 | 259. |
| 7 | .400 | 172. | 8.9 | 319. |
| 8 | .390 | 168. | 8.8 | 342. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .380 | 163. | 9.1 | 340. |
| 11 | .370 | 159. | 9.0 | 337. |
| 12 | .410 | 176. | 9.0 | 338. |
| 13 | .420 | 180. | 9.1 | 332. |
| 14 | .430 | 185. | 9.6 | 329. |
| 15 | .410 | 176. | 9.5 | 330. |
| 16 | .430 | 185. | 9.5 | 326. |
| 17 | .410 | 176. | 9.5 | 327. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | .410 | 176. | 9.7 | 324. |
| 20 | .410 | 176. | 9.6 | 325. |

| | | | | |
|---|---|---|---|---|
| 21 | .420 | 180. | 9.7 | 321. |
| 22 | .450 | 193. | 10.0 | 285. |
| 23 | .380 | 163. | 11.1 | 202. |
| 24 | .390 | 168. | 15.7 | 73. |

DAY = 4

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 9.5 | 361. |
| 2 | .420 | 180. | 9.8 | 362. |
| 3 | .430 | 185. | 9.8 | 365. |
| 4 | .430 | 185. | 9.9 | 363. |
| 5 | .410 | 176. | 10.0 | 361. |
| 6 | .410 | 176. | 10.0 | 362. |
| 7 | .420 | 180. | 10.1 | 362. |
| 8 | .420 | 180. | 10.1 | 362. |
| 9 | .430 | 185. | 9.7 | 360. |
| 10 | .420 | 180. | 9.5 | 361. |
| 11 | .420 | 180. | 9.4 | 361. |
| 12 | .410 | 176. | 9.4 | 362. |
| 13 | .420 | 180. | 9.3 | 361. |
| 14 | .420 | 180. | 9.2 | 362. |
| 15 | .410 | 176. | 8.9 | 362. |
| 16 | .400 | 172. | 8.3 | 362. |
| 17 | .410 | 176. | 8.4 | 361. |
| 18 | .410 | 176. | 8.2 | 361. |
| 19 | .410 | 176. | 8.6 | 359. |
| 20 | .400 | 172. | 8.5 | 359. |
| 21 | .400 | 172. | 8.5 | 359. |
| 22 | .400 | 172. | 8.5 | 361. |
| 23 | .410 | 176. | 8.6 | 360. |
| 24 | .410 | 176. | 8.5 | 362. |

DAY = 5

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 8.6 | 364. |
| 2 | .400 | 172. | 8.6 | 363. |
| 3 | .400 | 172. | 8.7 | 362. |
| 4 | .400 | 172. | 7.6 | 359. |
| 5 | .400 | 172. | 7.3 | 360. |
| 6 | .390 | 168. | 8.2 | 360. |
| 7 | .390 | 168. | 8.9 | 360. |
| 8 | .400 | 172. | 9.1 | 362. |
| 9 | .410 | 176. | 9.4 | 361. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .420 | 180. | 9.3 | 361. |
| 12 | .430 | 185. | 9.2 | 361. |
| 13 | .460 | 198. | 9.3 | 364. |
| 14 | .450 | 193. | 9.3 | 364. |
| 15 | .430 | 185. | 9.2 | 362. |
| 16 | .440 | 189. | 9.2 | 362. |
| 17 | .450 | 193. | 9.4 | 360. |
| 18 | .450 | 193. | 9.4 | 363. |
| 19 | .450 | 193. | 9.5 | 362. |

| | | | | |
|---|---|---|---|---|
| 20 | .450 | 193. | 9.6 | 361. |
| 21 | .420 | 180. | 9.5 | 362. |
| 22 | .420 | 180. | 9.5 | 362. |
| 23 | .440 | 189. | 9.5 | 357. |
| 24 | .430 | 185. | 9.4 | 345. |

DAY = 6

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 9.1 | 353. |
| 2 | .430 | 185. | 9.2 | 362. |
| 3 | .450 | 193. | 9.3 | 362. |
| 4 | .450 | 193. | 9.3 | 361. |
| 5 | .480 | 206. | 9.4 | 361. |
| 6 | .470 | 202. | 9.4 | 364. |
| 7 | .430 | 185. | 9.1 | 364. |
| 8 | .450 | 193. | 9.3 | 363. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .500 | 215. | 9.3 | 363. |
| 11 | .490 | 210. | 9.3 | 362. |
| 12 | .490 | 210. | 9.2 | 360. |
| 13 | .490 | 210. | 9.2 | 361. |
| 14 | .490 | 210. | 9.1 | 361. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .480 | 206. | 9.3 | 362. |
| 17 | .500 | 215. | 9.4 | 362. |
| 18 | .490 | 210. | 9.4 | 362. |
| 19 | .490 | 210. | 9.3 | 361. |
| 20 | .490 | 210. | 9.4 | 360. |
| 21 | .490 | 210. | 9.3 | 362. |
| 22 | .480 | 206. | 9.3 | 362. |
| 23 | .500 | 215. | 9.5 | 359. |
| 24 | .470 | 202. | 9.7 | 351. |

DAY = 7

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 9.5 | 356. |
| 2 | .390 | 168. | 9.7 | 346. |
| 3 | .410 | 176. | 10.2 | 298. |
| 4 | .390 | 168. | 10.0 | 296. |
| 5 | .390 | 168. | 10.0 | 303. |
| 6 | .450 | 193. | 9.6 | 354. |
| 7 | .480 | 206. | 9.1 | 360. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .470 | 202. | 9.3 | 332. |
| 11 | .430 | 185. | 9.2 | 331. |
| 12 | .430 | 185. | 9.2 | 330. |
| 13 | .440 | 189. | 9.2 | 329. |
| 14 | .500 | 215. | 8.9 | 343. |
| 15 | .530 | 228. | 8.5 | 359. |
| 16 | .520 | 223. | 8.4 | 363. |
| 17 | .520 | 223. | 8.5 | 363. |
| 18 | .480 | 206. | 8.6 | 362. |

| | | | | |
|---|---|---|---|---|
| 19 | .450 | 193. | 8.5 | 361. |
| 20 | .470 | 202. | 8.5 | 360. |
| 21 | .470 | 202. | 8.6 | 358. |
| 22 | .470 | 202. | 8.6 | 359. |
| 23 | .450 | 193. | 8.6 | 359. |
| 24 | .440 | 189. | 8.5 | 360. |

DAY = 8

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 8.5 | 363. |
| 2 | .440 | 189. | 8.5 | 363. |
| 3 | .430 | 185. | 8.5 | 363. |
| 4 | .430 | 185. | 8.8 | 345. |
| 5 | .430 | 185. | 8.9 | 338. |
| 6 | .420 | 180. | 8.5 | 362. |
| 7 | .420 | 180. | 8.6 | 361. |
| 8 | .410 | 176. | 8.5 | 361. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .420 | 180. | 8.6 | 361. |
| 11 | .450 | 193. | 8.5 | 360. |
| 12 | .430 | 185. | 8.4 | 360. |
| 13 | .430 | 185. | 8.3 | 360. |
| 14 | .440 | 189. | 8.3 | 359. |
| 15 | .450 | 193. | 8.2 | 358. |
| 16 | .460 | 198. | 8.2 | 357. |
| 17 | .470 | 202. | 8.2 | 358. |
| 18 | .430 | 185. | 8.2 | 358. |
| 19 | .420 | 180. | 8.1 | 360. |
| 20 | .420 | 180. | 8.1 | 361. |
| 21 | .450 | 193. | 5.9 | 361. |
| 22 | .440 | 189. | 5.9 | 360. |
| 23 | .420 | 180. | 5.9 | 363. |
| 24 | .450 | 193. | 6.2 | 360. |

DAY = 9

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 6.1 | 362. |
| 2 | .450 | 193. | 6.4 | 356. |
| 3 | .460 | 198. | 8.7 | 336. |
| 4 | .470 | 202. | 9.0 | 334. |
| 5 | .460 | 198. | 9.0 | 336. |
| 6 | .460 | 198. | 8.8 | 350. |
| 7 | .440 | 189. | 8.6 | 362. |
| 8 | .440 | 189. | 8.5 | 362. |
| 9 | .440 | 189. | 8.4 | 364. |
| 10 | .470 | 202. | 8.4 | 362. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .470 | 202. | 8.5 | 360. |
| 13 | .470 | 202. | 8.4 | 361. |
| 14 | .480 | 206. | 8.4 | 360. |
| 15 | .490 | 210. | 8.3 | 359. |
| 16 | .480 | 206. | 7.8 | 360. |
| 17 | -1.000 | -430. | -1.0 | -1. |

| | | | | |
|---|---|---|---|---|
| 18 | .460 | 198. | 8.8 | 362. |
| 19 | .450 | 193. | 8.8 | 364. |
| 20 | .450 | 193. | 9.0 | 363. |
| 21 | .430 | 185. | 9.0 | 360. |
| 22 | .450 | 193. | 9.0 | 362. |
| 23 | .460 | 198. | 9.1 | 363. |
| 24 | .450 | 193. | 9.1 | 362. |

DAY = 10

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 9.1 | 361. |
| 2 | .450 | 193. | 9.2 | 360. |
| 3 | .430 | 185. | 9.1 | 363. |
| 4 | .430 | 185. | 9.1 | 361. |
| 5 | .420 | 180. | 9.0 | 364. |
| 6 | .430 | 185. | 9.1 | 363. |
| 7 | .420 | 180. | 9.1 | 363. |
| 8 | .420 | 180. | 9.1 | 362. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .640 | 275. | 17.5 | 40. |
| 14 | .580 | 249. | 13.6 | 110. |
| 15 | .700 | 301. | 10.9 | 193. |
| 16 | .720 | 309. | 11.4 | 192. |
| 17 | .650 | 279. | 10.9 | 195. |
| 18 | .620 | 266. | 10.7 | 196. |
| 19 | .560 | 241. | 10.5 | 199. |
| 20 | .480 | 206. | 10.5 | 199. |
| 21 | .520 | 223. | 10.9 | 192. |
| 22 | .540 | 232. | 10.6 | 197. |
| 23 | .540 | 232. | 10.7 | 196. |
| 24 | .520 | 223. | 10.7 | 33. |

DAY = 11

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .470 | 202. | 10.7 | 199. |
| 2 | .440 | 189. | 10.4 | 197. |
| 3 | .450 | 193. | 10.4 | 198. |
| 4 | .460 | 198. | 10.4 | 192. |
| 5 | .460 | 198. | 10.3 | 196. |
| 6 | .370 | 159. | 9.6 | 212. |
| 7 | .350 | 150. | 9.7 | 214. |
| 8 | .340 | 146. | 9.5 | 218. |
| 9 | .330 | 142. | 9.5 | 220. |
| 10 | .350 | 150. | 9.6 | 217. |
| 11 | .360 | 155. | 9.6 | 215. |
| 12 | .350 | 150. | 9.5 | 216. |
| 13 | .340 | 146. | 9.3 | 216. |
| 14 | .350 | 150. | 9.3 | 217. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .370 | 159. | 7.5 | 311. |

| | | | | |
|---|---|---|---|---|
| 17 | .380 | 163. | 7.6 | 312. |
| 18 | .370 | 159. | 9.6 | 309. |
| 19 | .380 | 163. | 10.2 | 312. |
| 20 | .380 | 163. | 10.3 | 313. |
| 21 | .370 | 159. | 10.1 | 314. |
| 22 | .370 | 159. | 10.2 | 313. |
| 23 | .380 | 163. | 10.3 | 313. |
| 24 | .410 | 176. | 10.3 | 315. |

DAY = 12

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 10.3 | 317. |
| 2 | .420 | 180. | 10.3 | 314. |
| 3 | .430 | 185. | 10.8 | 276. |
| 4 | .420 | 180. | 10.7 | 275. |
| 5 | .420 | 180. | 10.7 | 275. |
| 6 | .420 | 180. | 10.6 | 279. |
| 7 | .420 | 180. | 10.4 | 297. |
| 8 | .400 | 172. | 10.3 | 309. |
| 9 | .410 | 176. | 10.3 | 311. |
| 10 | .400 | 172. | 10.4 | 313. |
| 11 | .350 | 150. | 10.5 | 314. |
| 12 | .370 | 159. | 10.6 | 310. |
| 13 | .380 | 163. | 10.4 | 301. |
| 14 | .360 | 155. | 10.5 | 308. |
| 15 | .400 | 172. | 10.3 | 303. |
| 16 | .360 | 155. | 8.2 | 310. |
| 17 | .400 | 172. | 7.6 | 328. |
| 18 | .390 | 168. | 7.7 | 327. |
| 19 | .330 | 142. | 7.8 | 327. |
| 20 | .330 | 142. | 7.9 | 322. |
| 21 | .360 | 155. | 7.9 | 320. |
| 22 | .350 | 150. | 7.8 | 319. |
| 23 | .350 | 150. | 7.7 | 325. |
| 24 | .360 | 155. | 7.6 | 49. |

DAY = 13

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 7.6 | 292. |
| 2 | .400 | 172. | 7.6 | 292. |
| 3 | -1.000 | -430. | -1.0 | -1. |
| 4 | .410 | 176. | 7.5 | 327. |
| 5 | .400 | 172. | 8.0 | 326. |
| 6 | .400 | 172. | 9.9 | 326. |
| 7 | .400 | 172. | 9.9 | 327. |
| 8 | .390 | 168. | 9.9 | 328. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .380 | 163. | 10.0 | 329. |
| 11 | .390 | 168. | 10.1 | 325. |
| 12 | .400 | 172. | 10.2 | 306. |
| 13 | .340 | 146. | 10.2 | 314. |
| 14 | .340 | 146. | 10.2 | 317. |
| 15 | .370 | 159. | 9.8 | 327. |

| | | | | |
|---|---|---|---|---|
| 16 | .390 | 163. | 9.7 | 326. |
| 17 | .330 | 142. | 9.8 | 326. |
| 18 | .400 | 172. | 9.9 | 326. |
| 19 | .400 | 172. | 9.9 | 322. |
| 20 | .410 | 176. | 10.0 | 324. |
| 21 | .420 | 180. | 9.9 | 324. |
| 22 | .420 | 180. | 10.2 | 321. |
| 23 | .420 | 180. | 10.0 | 319. |
| 24 | .420 | 180. | 10.2 | 311. |

DAY = 14

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 10.7 | 267. |
| 2 | .440 | 189. | 10.7 | 267. |
| 3 | .430 | 185. | 10.7 | 267. |
| 4 | .420 | 180. | 10.7 | 266. |
| 5 | .410 | 176. | 10.6 | 268. |
| 6 | .420 | 180. | 10.2 | 310. |
| 7 | .410 | 176. | 10.2 | 315. |
| 8 | .420 | 180. | 10.1 | 323. |
| 9 | .420 | 180. | 10.2 | 322. |
| 10 | .400 | 172. | 9.5 | 325. |
| 11 | .410 | 176. | 10.2 | 323. |
| 12 | .400 | 172. | 10.1 | 323. |
| 13 | .400 | 172. | 10.0 | 325. |
| 14 | .400 | 172. | 10.0 | 326. |
| 15 | .390 | 168. | 9.9 | 323. |
| 16 | .390 | 168. | 10.2 | 297. |
| 17 | .380 | 163. | 10.6 | 294. |
| 18 | .370 | 159. | 10.6 | 298. |
| 19 | .390 | 168. | 10.5 | 322. |
| 20 | .410 | 176. | 10.7 | 320. |
| 21 | .410 | 176. | 10.7 | 322. |
| 22 | .400 | 172. | 10.7 | 322. |
| 23 | .410 | 176. | 10.7 | 322. |
| 24 | .410 | 176. | 10.9 | 315. |

DAY = 15

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 11.2 | 265. |
| 2 | .390 | 168. | 11.2 | 261. |
| 3 | .430 | 185. | 11.5 | 246. |
| 4 | .480 | 206. | 11.7 | 243. |
| 5 | .480 | 206. | 11.7 | 241. |
| 6 | .390 | 168. | 11.2 | 281. |
| 7 | .410 | 176. | 10.8 | 320. |
| 8 | .420 | 180. | 10.9 | 327. |
| 9 | .430 | 185. | 10.9 | 327. |
| 10 | .430 | 185. | 10.8 | 324. |
| 11 | .410 | 176. | 10.6 | 325. |
| 12 | .410 | 176. | 10.6 | 325. |
| 13 | .410 | 176. | 10.5 | 324. |
| 14 | .400 | 172. | 10.4 | 327. |

| | | | | |
|---|---|---|---|---|
| 15 | .390 | 168. | 10.2 | 333. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .440 | 189. | 10.7 | 318. |
| 18 | .430 | 185. | 10.7 | 318. |
| 19 | .430 | 185. | 10.5 | 328. |
| 20 | .410 | 176. | 10.4 | 328. |
| 21 | .430 | 185. | 10.5 | 329. |
| 22 | .430 | 185. | 10.5 | 329. |
| 23 | .410 | 176. | 10.8 | 301. |
| 24 | .390 | 168. | 10.9 | 43. |

DAY = 16

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 11.4 | 245. |
| 2 | .450 | 193. | 11.4 | 234. |
| 3 | .410 | 176. | 11.1 | 255. |
| 4 | .410 | 176. | 11.1 | 255. |
| 5 | .450 | 193. | 11.5 | 250. |
| 6 | .420 | 180. | 13.1 | 204. |
| 7 | .430 | 185. | 11.8 | 256. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | .410 | 176. | 10.7 | 324. |
| 10 | .410 | 176. | 10.8 | 319. |
| 11 | .410 | 176. | 10.8 | 317. |
| 12 | .390 | 168. | 10.6 | 319. |
| 13 | .430 | 185. | 11.0 | 312. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .420 | 180. | 9.2 | 322. |
| 18 | .400 | 172. | 9.1 | 319. |
| 19 | .400 | 172. | 10.1 | 317. |
| 20 | .380 | 163. | 10.1 | 318. |
| 21 | .390 | 168. | 10.2 | 318. |
| 22 | .380 | 163. | 9.7 | 319. |
| 23 | .390 | 168. | 9.1 | 319. |
| 24 | .400 | 172. | 9.5 | 322. |

DAY = 17

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.4 | 322. |
| 2 | .380 | 163. | 10.3 | 321. |
| 3 | .380 | 163. | 10.0 | 322. |
| 4 | .380 | 163. | 10.2 | 323. |
| 5 | .380 | 163. | 10.2 | 323. |
| 6 | .380 | 163. | 10.2 | 323. |
| 7 | .380 | 163. | 10.3 | 321. |
| 8 | .390 | 168. | 10.4 | 320. |
| 9 | .380 | 163. | 10.3 | 322. |
| 10 | .390 | 168. | 10.3 | 320. |
| 11 | .400 | 172. | 10.4 | 322. |
| 12 | .400 | 172. | 10.2 | 323. |
| 13 | .390 | 168. | 10.2 | 324. |

| | | | | |
|---|---|---|---|---|
| 14 | .390 | 168. | 10.2 | 323. |
| 15 | .400 | 172. | 10.2 | 323. |
| 16 | .390 | 168. | 10.2 | 323. |
| 17 | .390 | 168. | 10.4 | 323. |
| 18 | .400 | 172. | 9.2 | 322. |
| 19 | .420 | 180. | 10.3 | 322. |
| 20 | .430 | 185. | 10.7 | 322. |
| 21 | .430 | 185. | 10.7 | 322. |
| 22 | .430 | 185. | 10.6 | 324. |
| 23 | .430 | 185. | 10.7 | 321. |
| 24 | .440 | 189. | 10.6 | 53. |

DAY = 18

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 10.8 | 319. |
| 2 | .440 | 189. | 10.7 | 321. |
| 3 | .440 | 189. | 10.6 | 321. |
| 4 | .430 | 185. | 10.6 | 316. |
| 5 | .420 | 180. | 10.5 | 316. |
| 6 | .420 | 180. | 10.5 | 318. |
| 7 | .410 | 176. | 10.5 | 319. |
| 8 | .420 | 180. | 10.5 | 323. |
| 9 | .420 | 180. | 10.7 | 323. |
| 10 | .420 | 180. | 10.7 | 323. |
| 11 | .420 | 180. | 10.5 | 323. |
| 12 | .420 | 180. | 10.5 | 322. |
| 13 | .420 | 180. | 10.4 | 324. |
| 14 | .420 | 180. | 10.4 | 322. |
| 15 | .420 | 180. | 10.4 | 321. |
| 16 | .410 | 176. | 10.5 | 322. |
| 17 | .410 | 176. | 10.6 | 323. |
| 18 | .410 | 176. | 10.6 | 321. |
| 19 | .400 | 172. | 10.4 | 321. |
| 20 | .400 | 172. | 10.3 | 321. |
| 21 | .390 | 168. | 10.3 | 321. |
| 22 | .390 | 168. | 10.2 | 322. |
| 23 | .380 | 163. | 10.2 | 321. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 19

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.4 | 321. |
| 2 | .390 | 168. | 10.3 | 322. |
| 3 | .380 | 163. | 10.3 | 324. |
| 4 | .380 | 163. | 10.3 | 323. |
| 5 | .370 | 159. | 10.3 | 322. |
| 6 | .380 | 163. | 10.4 | 322. |
| 7 | .390 | 168. | 10.6 | 322. |
| 8 | .390 | 168. | 10.5 | 318. |
| 9 | .400 | 172. | 10.7 | 319. |
| 10 | .400 | 172. | 10.6 | 323. |
| 11 | .400 | 172. | 10.3 | 324. |
| 12 | .410 | 176. | 10.5 | 322. |

| | | | | |
|---|---|---|---|---|
| 13 | .430 | 185. | 10.5 | 321. |
| 14 | .420 | 180. | 10.3 | 319. |
| 15 | .410 | 176. | 10.3 | 318. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .400 | 172. | 10.3 | 321. |
| 18 | .410 | 176. | 10.3 | 323. |
| 19 | .400 | 172. | 10.0 | 322. |
| 20 | .400 | 172. | 9.9 | 322. |
| 21 | .410 | 176. | 9.9 | 321. |
| 22 | .400 | 172. | 9.8 | 322. |
| 23 | .380 | 163. | 9.9 | 324. |
| 24 | .390 | 168. | 10.3 | 325. |

DAY = 20

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.4 | 325. |
| 2 | .390 | 168. | 10.3 | 326. |
| 3 | .370 | 159. | 10.2 | 324. |
| 4 | .350 | 150. | 10.0 | 322. |
| 5 | .340 | 146. | 9.9 | 324. |
| 6 | .340 | 146. | 10.0 | 325. |
| 7 | .360 | 155. | 10.1 | 324. |
| 8 | .370 | 159. | 10.2 | 323. |
| 9 | .370 | 159. | 10.4 | 323. |
| 10 | .380 | 163. | 10.5 | 322. |
| 11 | .390 | 168. | 10.7 | 323. |
| 12 | .400 | 172. | 10.8 | 325. |
| 13 | .400 | 172. | 10.7 | 323. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .400 | 172. | 10.8 | 328. |
| 16 | .390 | 168. | 10.5 | 331. |
| 17 | .380 | 163. | 10.6 | 332. |
| 18 | .380 | 163. | 10.4 | 333. |
| 19 | .380 | 163. | 10.3 | 334. |
| 20 | .400 | 172. | 10.5 | 340. |
| 21 | .410 | 176. | 10.7 | 340. |
| 22 | .410 | 176. | 10.8 | 339. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | .410 | 176. | 10.8 | 337. |

DAY = 21

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 11.0 | 328. |
| 2 | .400 | 172. | 10.9 | 326. |
| 3 | .400 | 172. | 10.9 | 318. |
| 4 | .400 | 172. | 10.9 | 315. |
| 5 | .380 | 163. | 10.9 | 313. |
| 6 | .410 | 176. | 10.9 | 326. |
| 7 | .400 | 172. | 10.9 | 327. |
| 8 | .430 | 185. | 11.0 | 328. |
| 9 | .440 | 189. | 11.0 | 329. |
| 10 | .430 | 185. | 11.0 | 330. |
| 11 | .430 | 185. | 10.9 | 332. |

| | | | | |
|---|---|---|---|---|
| 12 | .430 | 185. | 10.8 | 331. |
| 13 | .430 | 185. | 10.8 | 332. |
| 14 | .420 | 180. | 10.7 | 333. |
| 15 | .420 | 180. | 10.8 | 332. |
| 16 | .410 | 176. | 10.7 | 331. |
| 17 | .410 | 176. | 10.7 | 332. |
| 18 | .410 | 176. | 10.7 | 331. |
| 19 | .390 | 168. | 10.7 | 330. |
| 20 | .380 | 163. | 10.6 | 331. |
| 21 | .390 | 168. | 10.8 | 331. |
| 22 | .390 | 168. | 10.7 | 329. |
| 23 | .390 | 168. | 10.8 | 331. |
| 24 | .390 | 168. | 10.8 | 331. |

DAY = 22

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.8 | 331. |
| 2 | .390 | 168. | 10.8 | 331. |
| 3 | .390 | 168. | 10.8 | 330. |
| 4 | .370 | 159. | 10.7 | 330. |
| 5 | .380 | 163. | 10.8 | 331. |
| 6 | .400 | 172. | 11.0 | 331. |
| 7 | .400 | 172. | 10.9 | 331. |
| 8 | .390 | 168. | 10.8 | 331. |
| 9 | .400 | 172. | 11.2 | 332. |
| 10 | .410 | 176. | 11.2 | 330. |
| 11 | .410 | 176. | 11.0 | 329. |
| 12 | .410 | 176. | 11.0 | 330. |
| 13 | .410 | 176. | 10.9 | 330. |
| 14 | .410 | 176. | 10.9 | 328. |
| 15 | .390 | 168. | 10.8 | 327. |
| 16 | .410 | 176. | 10.8 | 331. |
| 17 | .420 | 180. | 10.9 | 333. |
| 18 | .410 | 176. | 10.9 | 334. |
| 19 | .410 | 176. | 10.9 | 334. |
| 20 | .420 | 180. | 11.0 | 333. |
| 21 | .420 | 180. | 11.0 | 328. |
| 22 | .430 | 185. | 11.0 | 330. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | .420 | 180. | 11.1 | 55. |

DAY = 23

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT Mw |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.9 | 332. |
| 2 | .410 | 176. | 10.8 | 330. |
| 3 | .390 | 168. | 10.9 | 310. |
| 4 | .370 | 159. | 10.8 | 311. |
| 5 | .380 | 163. | 10.8 | 310. |
| 6 | .360 | 155. | 8.4 | 312. |
| 7 | .380 | 163. | 8.2 | 328. |
| 8 | .390 | 168. | 8.3 | 333. |
| 9 | .390 | 168. | 8.5 | 331. |
| 10 | .400 | 172. | 8.4 | 331. |

| | | | | |
|---|---|---|---|---|
| 11 | .400 | 172. | 8.4 | 330. |
| 12 | .390 | 168. | 8.3 | 330. |
| 13 | .380 | 163. | 8.1 | 330. |
| 14 | .360 | 155. | 7.9 | 330. |
| 15 | .370 | 159. | 8.0 | 331. |
| 16 | .370 | 159. | 7.9 | 332. |
| 17 | .360 | 155. | 7.7 | 337. |
| 18 | .350 | 150. | 7.5 | 340. |
| 19 | .350 | 150. | 7.3 | 340. |
| 20 | .340 | 146. | 7.3 | 338. |
| 21 | .360 | 155. | 9.6 | 336. |
| 22 | .360 | 155. | 10.0 | 336. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | .360 | 155. | 10.1 | 337. |

DAY = 24

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.2 | 336. |
| 2 | .380 | 163. | 10.2 | 336. |
| 3 | .380 | 163. | 10.2 | 336. |
| 4 | .350 | 150. | 9.6 | 337. |
| 5 | .360 | 155. | 8.5 | 337. |
| 6 | .390 | 168. | 8.0 | 336. |
| 7 | .390 | 168. | 8.5 | 335. |
| 8 | .380 | 163. | 8.5 | 335. |
| 9 | .380 | 163. | 8.6 | 333. |
| 10 | .400 | 172. | 10.3 | 334. |
| 11 | .410 | 176. | 10.6 | 335. |
| 12 | .400 | 172. | 10.4 | 336. |
| 13 | .400 | 172. | 10.3 | 336. |
| 14 | .390 | 168. | 10.1 | 335. |
| 15 | .390 | 168. | 10.0 | 335. |
| 16 | .390 | 168. | 10.0 | 335. |
| 17 | .410 | 176. | 10.2 | 335. |
| 18 | .390 | 168. | 10.1 | 335. |
| 19 | .390 | 168. | 10.0 | 337. |
| 20 | .390 | 168. | 10.1 | 336. |
| 21 | .390 | 168. | 10.1 | 335. |
| 22 | .380 | 163. | 10.1 | 334. |
| 23 | .380 | 163. | 10.1 | 333. |
| 24 | .380 | 163. | 10.2 | 306. |

DAY = 25

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 10.3 | 285. |
| 2 | .380 | 163. | 10.2 | 287. |
| 3 | .400 | 172. | 10.1 | 287. |
| 4 | .390 | 168. | 10.1 | 287. |
| 5 | .390 | 168. | 10.4 | 287. |
| 6 | .380 | 163. | 10.6 | 287. |
| 7 | .380 | 163. | 10.8 | 285. |
| 8 | .380 | 163. | 10.9 | 287. |
| 9 | .370 | 159. | 10.9 | 303. |

| | | | | |
|---|---|---|---|---|
| 10 | .370 | 159. | 10.5 | 327. |
| 11 | .370 | 159. | 10.4 | 341. |
| 12 | .370 | 159. | 10.3 | 340. |
| 13 | .380 | 163. | 10.3 | 339. |
| 14 | .380 | 163. | 10.5 | 333. |
| 15 | .400 | 172. | 10.8 | 326. |
| 16 | .400 | 172. | 11.1 | 286. |
| 17 | .380 | 163. | 10.8 | 292. |
| 18 | .360 | 155. | 10.6 | 302. |
| 19 | .370 | 159. | 10.4 | 323. |
| 20 | .390 | 168. | 10.5 | 331. |
| 21 | .400 | 172. | 10.5 | 335. |
| 22 | .380 | 163. | 10.4 | 336. |
| 23 | .380 | 163. | 10.4 | 337. |
| 24 | .380 | 163. | 10.2 | 47. |

DAY = 26

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.8 | 283. |
| 2 | .390 | 168. | 10.9 | 283. |
| 3 | .390 | 168. | 10.8 | 283. |
| 4 | .400 | 172. | 10.4 | 328. |
| 5 | .420 | 180. | 10.4 | 336. |
| 6 | .410 | 176. | 10.3 | 336. |
| 7 | .410 | 176. | 10.4 | 336. |
| 8 | .390 | 168. | 9.5 | 336. |
| 9 | .390 | 168. | 9.9 | 337. |
| 10 | .390 | 168. | 10.6 | 334. |
| 11 | .410 | 176. | 10.7 | 334. |
| 12 | .400 | 172. | 10.6 | 333. |
| 13 | .420 | 180. | 10.6 | 335. |
| 14 | .380 | 163. | 8.7 | 336. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .260 | 112. | 10.8 | 330. |
| 17 | .380 | 163. | 10.7 | 331. |
| 18 | .380 | 163. | 10.7 | 332. |
| 19 | .400 | 172. | 10.9 | 327. |
| 20 | .390 | 168. | 10.7 | 326. |
| 21 | .380 | 163. | 10.6 | 325. |
| 22 | .370 | 159. | 10.6 | 325. |
| 23 | .380 | 163. | 10.7 | 324. |
| 24 | .390 | 168. | 10.8 | 313. |

DAY = 27

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 10.9 | 301. |
| 2 | .390 | 168. | 10.9 | 302. |
| 3 | .390 | 168. | 10.9 | 302. |
| 4 | .400 | 172. | 11.0 | 301. |
| 5 | .400 | 172. | 11.1 | 302. |
| 6 | .410 | 176. | 11.1 | 305. |
| 7 | .370 | 159. | 10.7 | 330. |
| 8 | .400 | 172. | 11.0 | 330. |

| | | | | |
|---|---|---|---|---|
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | .190 | 82. | 5.4 | 328. |
| 15 | .380 | 163. | 10.6 | 329. |
| 16 | .360 | 155. | 10.6 | 331. |
| 17 | .350 | 150. | 10.4 | 332. |
| 18 | .340 | 146. | 10.3 | 331. |
| 19 | .360 | 155. | 10.4 | 330. |
| 20 | .380 | 163. | 10.5 | 330. |
| 21 | .400 | 172. | 10.6 | 328. |
| 22 | .400 | 172. | 10.6 | 330. |
| 23 | .400 | 172. | 10.6 | 330. |
| 24 | .410 | 176. | 11.0 | 307. |

DAY = 28

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 11.1 | 285. |
| 2 | .400 | 172. | 11.1 | 284. |
| 3 | .400 | 172. | 11.1 | 285. |
| 4 | .400 | 172. | 11.0 | 284. |
| 5 | .400 | 172. | 10.0 | 288. |
| 6 | .390 | 168. | 10.0 | 301. |
| 7 | .380 | 163. | 9.9 | 322. |
| 8 | .380 | 163. | 10.4 | 331. |
| 9 | .380 | 163. | 10.5 | 331. |
| 10 | .380 | 163. | 10.3 | 332. |
| 11 | .380 | 163. | 10.3 | 333. |
| 12 | .370 | 159. | 10.3 | 334. |
| 13 | .380 | 163. | 10.3 | 333. |
| 14 | .380 | 163. | 10.4 | 331. |
| 15 | .390 | 168. | 10.5 | 333. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .400 | 172. | 10.7 | 331. |
| 18 | .400 | 172. | 10.6 | 331. |
| 19 | .400 | 172. | 10.6 | 332. |
| 20 | -1.000 | -430. | -1.0 | -1. |
| 21 | .400 | 172. | 10.6 | 331. |
| 22 | .410 | 176. | 10.7 | 324. |
| 23 | .390 | 168. | 10.5 | 328. |
| 24 | .390 | 168. | 9.9 | 47. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | .370 | 159. | 8.7 | 282. |
| 3 | .370 | 159. | 8.8 | 281. |
| 4 | .370 | 159. | 8.7 | 282. |
| 5 | .380 | 163. | 9.1 | 285. |
| 6 | .360 | 155. | 9.0 | 312. |
| 7 | .370 | 159. | 8.6 | 329. |

| | | | | |
|---|---|---|---|---|
| 8 | .380 | 163. | 10.0 | 337. |
| 9 | .390 | 168. | 9.8 | 340. |
| 10 | .370 | 159. | 9.6 | 343. |
| 11 | .380 | 163. | 9.7 | 340. |
| 12 | .380 | 163. | 9.6 | 341. |
| 13 | .390 | 168. | 9.7 | 341. |
| 14 | .400 | 172. | 9.7 | 338. |
| 15 | .390 | 168. | 9.6 | 339. |
| 16 | .400 | 172. | 9.7 | 341. |
| 17 | .390 | 168. | 9.4 | 340. |
| 18 | .400 | 172. | 10.0 | 339. |
| 19 | -1.000 | -430. | -1.0 | -1. |
| 20 | .410 | 176. | 10.2 | 337. |
| 21 | .400 | 172. | 10.1 | 337. |
| 22 | .390 | 168. | 10.1 | 337. |
| 23 | .400 | 172. | 10.1 | 338. |
| 24 | .410 | 176. | 10.3 | 339. |

DAY = 30

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 10.4 | 337. |
| 2 | .410 | 176. | 10.7 | 336. |
| 3 | .420 | 180. | 10.7 | 335. |
| 4 | .400 | 172. | 10.6 | 335. |
| 5 | .400 | 172. | 10.6 | 335. |
| 6 | .390 | 168. | 10.7 | 323. |
| 7 | .400 | 172. | 10.6 | 331. |
| 8 | .380 | 163. | 10.5 | 335. |
| 9 | .380 | 163. | 10.5 | 332. |
| 10 | .370 | 159. | 10.3 | 336. |
| 11 | .360 | 155. | 10.2 | 337. |
| 12 | .370 | 159. | 10.1 | 338. |
| 13 | .350 | 150. | 10.0 | 339. |
| 14 | .360 | 155. | 9.7 | 336. |
| 15 | .350 | 150. | 9.6 | 338. |
| 16 | .380 | 163. | 10.0 | 338. |
| 17 | .380 | 163. | 10.0 | 338. |
| 18 | .380 | 163. | 10.0 | 337. |
| 19 | .370 | 159. | 9.7 | 336. |
| 20 | .380 | 163. | 10.3 | 337. |
| 21 | .380 | 163. | 10.1 | 337. |
| 22 | .380 | 163. | 10.0 | 337. |
| 23 | .370 | 159. | 10.0 | 336. |
| 24 | .380 | 163. | 10.1 | 335. |

DAY = 31

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 10.0 | 335. |
| 2 | .370 | 159. | 10.1 | 335. |
| 3 | .350 | 150. | 10.4 | 302. |
| 4 | .350 | 150. | 10.4 | 299. |
| 5 | .360 | 155. | 10.5 | 299. |
| 6 | .370 | 159. | 10.8 | 299. |

| | | | | |
|---|---|---|---|---|
| 7 | .360 | 155. | 10.8 | 298. |
| 8 | .360 | 155. | 10.9 | 301. |
| 9 | .360 | 155. | 10.6 | 332. |
| 10 | .370 | 159. | 10.4 | 337. |
| 11 | .370 | 159. | 10.4 | 337. |
| 12 | .370 | 159. | 10.4 | 337. |
| 13 | .390 | 168. | 10.3 | 339. |
| 14 | .390 | 168. | 9.3 | 305. |
| 15 | .390 | 168. | 10.0 | 265. |
| 16 | .390 | 168. | 10.3 | 279. |
| 17 | .360 | 155. | 10.0 | 309. |
| 18 | .380 | 163. | 10.5 | 318. |
| 19 | .420 | 180. | 10.7 | 341. |
| 20 | .440 | 189. | 10.8 | 339. |
| 21 | .430 | 185. | 10.8 | 339. |
| 22 | .430 | 185. | 10.9 | 340. |
| 23 | .430 | 185. | 10.9 | 340. |
| 24 | .410 | 176. | 10.8 | 338. |

DAY = 33

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 11.1 | 333. |
| 2 | .390 | 168. | 11.0 | 332. |
| 3 | .380 | 163. | 10.9 | 332. |
| 4 | .380 | 163. | 10.9 | 327. |
| 5 | .450 | 193. | 11.7 | 301. |
| 6 | .390 | 168. | 11.4 | 305. |
| 7 | .400 | 172. | 11.0 | 327. |
| 8 | .410 | 176. | 11.0 | 334. |
| 9 | .390 | 168. | 11.9 | 339. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .400 | 172. | 10.8 | 338. |
| 12 | .390 | 168. | 10.6 | 339. |
| 13 | .380 | 163. | 10.6 | 337. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .380 | 163. | 9.6 | 332. |
| 16 | .390 | 168. | 9.7 | 331. |
| 17 | .400 | 172. | 9.5 | 333. |
| 18 | .400 | 172. | 9.7 | 330. |
| 19 | .400 | 172. | 9.9 | 331. |
| 20 | .410 | 176. | 10.0 | 332. |
| 21 | .410 | 176. | 10.2 | 332. |
| 22 | .410 | 176. | 9.9 | 333. |
| 23 | .420 | 180. | 9.4 | 330. |
| 24 | .410 | 176. | 10.4 | 330. |

DAY = 34

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.4 | 330. |
| 2 | .440 | 189. | 10.7 | 330. |
| 3 | .450 | 193. | 10.9 | 330. |
| 4 | .440 | 189. | 10.7 | 330. |
| 5 | .4 0 | 189. | 10.6 | 328. |

| | | | | |
|---|---|---|---|---|
| 6 | .440 | 189. | 10.5 | 329. |
| 7 | .440 | 189. | 10.9 | 329. |
| 8 | .420 | 180. | 10.9 | 330. |
| 9 | .410 | 176. | 10.8 | 330. |
| 10 | .420 | 180. | 11.0 | 329. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .400 | 172. | 10.8 | 330. |
| 14 | .390 | 168. | 10.6 | 329. |
| 15 | .390 | 168. | 10.6 | 328. |
| 16 | .380 | 163. | 10.6 | 329. |
| 17 | .390 | 168. | 10.6 | 327. |
| 18 | .380 | 163. | 10.5 | 328. |
| 19 | .370 | 159. | 10.5 | 328. |
| 20 | .370 | 159. | 10.5 | 328. |
| 21 | .380 | 163. | 10.7 | 328. |
| 22 | .390 | 168. | 10.7 | 328. |
| 23 | .380 | 163. | 10.7 | 329. |
| 24 | .380 | 163. | 10.8 | 329. |

DAY = 35

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 11.0 | 328. |
| 2 | .400 | 172. | 11.0 | 328. |
| 3 | .380 | 163. | 11.0 | 328. |
| 4 | .380 | 163. | 11.4 | 330. |
| 5 | .410 | 176. | 11.8 | 330. |
| 6 | .410 | 176. | 11.3 | 330. |
| 7 | .420 | 180. | 11.2 | 330. |
| 8 | .420 | 180. | 11.2 | 330. |
| 9 | .420 | 180. | 11.3 | 328. |
| 10 | .420 | 180. | 11.1 | 332. |
| 11 | .430 | 185. | 11.1 | 332. |
| 12 | .420 | 180. | 11.0 | 331. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | .410 | 176. | 10.6 | 329. |
| 15 | .420 | 180. | 10.6 | 329. |
| 16 | .420 | 180. | 10.7 | 329. |
| 17 | .400 | 172. | 10.5 | 329. |
| 18 | .400 | 172. | 10.5 | 331. |
| 19 | .400 | 172. | 10.6 | 329. |
| 20 | .410 | 176. | 10.6 | 329. |
| 21 | -1.000 | -430. | -1.0 | -1. |
| 22 | .380 | 163. | 9.8 | 327. |
| 23 | .390 | 168. | 9.6 | 327. |
| 24 | .410 | 176. | 9.8 | 329. |

DAY = 36

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 10.5 | 327. |
| 2 | .380 | 163. | 10.4 | 324. |
| 3 | .390 | 168. | 10.5 | 323. |
| 4 | .390 | 168. | 10.8 | 322. |

| | | | | |
|---|---|---|---|---|
| 5 | .390 | 168. | 10.3 | 322. |
| 6 | .390 | 168. | 10.1 | 324. |
| 7 | .390 | 168. | 10.0 | 328. |
| 8 | .380 | 163. | 10.0 | 327. |
| 9 | .380 | 163. | 10.0 | 324. |
| 10 | .380 | 163. | 9.9 | 328. |
| 11 | .390 | 168. | 10.0 | 322. |
| 12 | .380 | 163. | 10.0 | 321. |
| 13 | .370 | 159. | 10.1 | 320. |
| 14 | .380 | 163. | 10.1 | 329. |
| 15 | .390 | 168. | 10.2 | 334. |
| 16 | .400 | 172. | 10.3 | 335. |
| 17 | .400 | 172. | 10.2 | 336. |
| 18 | .400 | 172. | 10.2 | 337. |
| 19 | .420 | 180. | 10.4 | 330. |
| 20 | .410 | 176. | 10.4 | 330. |
| 21 | -1.000 | -430. | -1.0 | -1. |
| 22 | .410 | 176. | 10.3 | 329. |
| 23 | .390 | 168. | 10.3 | 331. |
| 24 | .390 | 168. | 10.3 | 333. |

DAY = 38

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | .430 | 185. | 12.7 | 211. |
| 3 | .440 | 189. | 12.9 | 212. |
| 4 | .420 | 180. | 12.9 | 210. |
| 5 | .450 | 193. | 12.9 | 212. |
| 6 | .430 | 185. | 12.8 | 199. |
| 7 | .420 | 180. | 13.0 | 199. |
| 8 | .410 | 176. | 12.9 | 197. |
| 9 | .480 | 206. | 13.5 | 184. |
| 10 | .390 | 168. | 16.7 | 104. |
| 11 | .380 | 163. | 16.1 | 105. |
| 12 | .340 | 146. | 15.6 | 117. |
| 13 | .350 | 150. | 15.7 | 112. |
| 14 | .360 | 155. | 15.7 | 110. |
| 15 | .330 | 142. | 15.4 | 116. |
| 16 | .390 | 168. | 15.7 | 114. |
| 17 | .440 | 189. | 15.8 | 112. |
| 18 | .440 | 189. | 15.8 | 113. |
| 19 | .400 | 172. | 15.7 | 109. |
| 20 | .370 | 159. | 15.7 | 112. |
| 21 | -1.000 | -430. | -1.0 | -1. |
| 22 | .440 | 189. | 15.5 | 108. |
| 23 | .090 | 39. | 10.9 | 28. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 42

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 9.4 | 265. |
| 2 | .480 | 206. | 9.6 | 262. |
| 3 | .500 | 215. | 9.7 | 261. |

| | | | | |
|---|---|---|---|---|
| 4 | .510 | 219. | 9.8 | 269. |
| 5 | .470 | 202. | 9.6 | 280. |
| 6 | .440 | 189. | 9.6 | 280. |
| 7 | .440 | 189. | 9.7 | 284. |
| 8 | .420 | 180. | 9.5 | 293. |
| 9 | .420 | 180. | 9.5 | 291. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .420 | 180. | 9.4 | 292. |
| 12 | .430 | 185. | 9.3 | 290. |
| 13 | .430 | 185. | 9.2 | 288. |
| 14 | .440 | 189. | 9.2 | 290. |
| 15 | .440 | 189. | 9.2 | 294. |
| 16 | .430 | 185. | 9.0 | 300. |
| 17 | .420 | 180. | 8.9 | 301. |
| 18 | .410 | 176. | 8.9 | 310. |
| 19 | .390 | 168. | 8.7 | 314. |
| 20 | .390 | 168. | 8.8 | 308. |
| 21 | .430 | 185. | 9.1 | 298. |
| 22 | .450 | 193. | 9.3 | 291. |
| 23 | .450 | 193. | 9.3 | 292. |
| 24 | .430 | 185. | 9.3 | 49. |

DAY = 43

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .450 | 193. | 9.5 | 290. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .440 | 189. | 9.5 | 284. |
| 4 | .400 | 172. | 9.2 | 290. |
| 5 | .410 | 176. | 9.2 | 291. |
| 6 | .400 | 172. | 9.2 | 291. |
| 7 | .400 | 172. | 9.5 | 287. |
| 8 | .430 | 185. | 9.3 | 289. |
| 9 | .420 | 180. | 9.3 | 291. |
| 10 | .450 | 193. | 9.7 | 286. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .410 | 176. | 9.0 | 291. |
| 14 | .420 | 180. | 9.0 | 289. |
| 15 | .420 | 180. | 8.9 | 291. |
| 16 | .390 | 168. | 8.7 | 296. |
| 17 | .380 | 163. | 8.6 | 297. |
| 18 | -1.000 | -430. | -1.0 | -1. |
| 19 | .420 | 180. | 9.3 | 277. |
| 20 | .430 | 185. | 9.4 | 274. |
| 21 | .370 | 159. | 8.9 | 289. |
| 22 | .410 | 176. | 9.1 | 284. |
| 23 | .450 | 193. | 9.6 | 271. |
| 24 | .400 | 172. | 9.1 | 282. |

DAY = 44

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .370 | 159. | 8.7 | 295. |
| 2 | .370 | 159. | 8.8 | 295. |

| | | | | |
|---|---|---|---|---|
| 3 | .360 | 155. | 8.6 | 297. |
| 4 | .360 | 155. | 8.6 | 297. |
| 5 | .370 | 159. | 8.7 | 298. |
| 6 | .350 | 150. | 8.5 | 303. |
| 7 | .340 | 146. | 8.4 | 307. |
| 8 | .310 | 133. | 7.9 | 311. |
| 9 | .310 | 133. | 7.9 | 310. |
| 10 | .320 | 137. | 8.1 | 296. |
| 11 | .300 | 129. | 7.7 | 312. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | .300 | 129. | 7.7 | 322. |
| 16 | .310 | 133. | 7.9 | 321. |
| 17 | .330 | 142. | 8.1 | 323. |
| 18 | .320 | 137. | 8.0 | 326. |
| 19 | .320 | 137. | 8.0 | 327. |
| 20 | .320 | 137. | 8.0 | 326. |
| 21 | .310 | 133. | 8.1 | 330. |
| 22 | -1.000 | -430. | -1.0 | -1. |
| 23 | .320 | 137. | 8.1 | 332. |
| 24 | .310 | 133. | 8.2 | 55. |

DAY = 45

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .290 | 125. | 8.2 | 329. |
| 2 | .290 | 125. | 8.2 | 328. |
| 3 | .350 | 150. | 10.3 | 264. |
| 4 | .430 | 185. | 12.0 | 217. |
| 5 | .420 | 180. | 12.0 | 217. |
| 6 | .420 | 180. | 12.1 | 217. |
| 7 | .410 | 176. | 12.1 | 216. |
| 8 | .410 | 176. | 12.1 | 215. |
| 9 | .410 | 176. | 12.0 | 213. |
| 10 | .360 | 155. | 11.3 | 211. |
| 11 | .360 | 155. | 11.2 | 210. |
| 12 | .350 | 150. | 11.0 | 212. |
| 13 | .430 | 185. | 11.3 | 205. |
| 14 | .390 | 168. | 11.1 | 210. |
| 15 | .370 | 159. | 11.1 | 211. |
| 16 | .340 | 146. | 10.8 | 216. |
| 17 | .330 | 142. | 10.8 | 214. |
| 18 | .330 | 142. | 10.7 | 218. |
| 19 | .290 | 125. | 9.9 | 227. |
| 20 | .310 | 133. | 10.1 | 221. |
| 21 | -1.000 | -430. | -1.0 | -1. |
| 22 | -1.000 | -430. | -1.0 | -1. |
| 23 | .330 | 142. | 8.5 | 323. |
| 24 | .330 | 142. | 8.6 | 319. |

DAY = 46

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .300 | 129. | 8.3 | 327. |

| | | | | |
|---|---|---|---|---|
| 2 | .340 | 146. | 8.8 | 322. |
| 3 | .340 | 146. | 8.7 | 322. |
| 4 | .300 | 129. | 8.5 | 321. |
| 5 | .220 | 95. | 7.8 | 319. |
| 6 | .220 | 95. | 7.4 | 317. |
| 7 | .260 | 112. | 10.1 | 256. |
| 8 | .280 | 120. | 11.7 | 201. |
| 9 | .300 | 129. | 12.7 | 173. |
| 10 | .210 | 90. | 10.5 | 199. |
| 11 | .250 | 107. | 10.6 | 175. |
| 12 | .210 | 90. | 9.4 | 176. |
| 13 | .240 | 103. | 9.4 | 187. |
| 14 | .260 | 112. | 10.1 | 190. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .430 | 185. | 8.1 | 273. |
| 19 | .430 | 185. | 8.3 | 269. |
| 20 | .360 | 155. | 7.8 | 282. |
| 21 | .390 | 168. | 8.0 | 280. |
| 22 | .380 | 163. | 7.9 | 279. |
| 23 | .370 | 159. | 7.9 | 280. |
| 24 | .400 | 172. | 8.2 | 46. |

DAY = 07

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 8.8 | 276. |
| 2 | .440 | 189. | 8.8 | 274. |
| 3 | .380 | 163. | 8.1 | 280. |
| 4 | .360 | 155. | 8.2 | 286. |
| 5 | .350 | 150. | 7.7 | 297. |
| 6 | .350 | 150. | 7.8 | 301. |
| 7 | .350 | 150. | 8.2 | 304. |
| 8 | .350 | 150. | 8.1 | 300. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .360 | 155. | 8.4 | 307. |
| 12 | .450 | 193. | 10.6 | 303. |
| 13 | .490 | 210. | 11.4 | 303. |
| 14 | .570 | 245. | 10.7 | 304. |
| 15 | .300 | 129. | 5.7 | 304. |
| 16 | .300 | 129. | 5.6 | 304. |
| 17 | .290 | 125. | 5.5 | 308. |
| 18 | .300 | 129. | 5.5 | 309. |
| 19 | .320 | 137. | 5.8 | 303. |
| 20 | .330 | 142. | 5.8 | 302. |
| 21 | .310 | 133. | 5.5 | 306. |
| 22 | .300 | 129. | 5.6 | 307. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 08

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .460 | 198. | 10.4 | 213. |
| 2 | .480 | 206. | 10.4 | 208. |
| 3 | .410 | 176. | 10.2 | 210. |
| 4 | .420 | 180. | 10.2 | 209. |
| 5 | .410 | 176. | 10.0 | 212. |
| 6 | .350 | 150. | 9.7 | 217. |
| 7 | .330 | 142. | 9.6 | 222. |
| 8 | .350 | 150. | 10.0 | 217. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .370 | 159. | 9.8 | 213. |
| 12 | .370 | 159. | 9.7 | 220. |
| 13 | .400 | 172. | 9.8 | 202. |
| 14 | .380 | 163. | 9.6 | 202. |
| 15 | .350 | 150. | 10.1 | 215. |
| 16 | .500 | 215. | 13.8 | 227. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .340 | 146. | 10.2 | 301. |
| 19 | .370 | 159. | 8.6 | 296. |
| 20 | .360 | 155. | 8.4 | 289. |
| 21 | .340 | 146. | 8.8 | 292. |
| 22 | .400 | 172. | 11.2 | 282. |
| 23 | .400 | 172. | 11.5 | 272. |
| 24 | .380 | 163. | 11.2 | 274. |

DAY = 49

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .440 | 189. | 11.9 | 263. |
| 2 | .500 | 215. | 10.9 | 223. |
| 3 | .520 | 223. | 11.7 | 216. |
| 4 | .500 | 215. | 12.1 | 217. |
| 5 | .460 | 198. | 10.1 | 244. |
| 6 | .380 | 163. | 11.1 | 260. |
| 7 | .350 | 150. | 10.9 | 270. |
| 8 | .350 | 150. | 10.9 | 273. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .440 | 189. | 11.0 | 279. |
| 11 | .480 | 206. | 10.9 | 278. |
| 12 | .430 | 185. | 10.7 | 279. |
| 13 | .410 | 176. | 10.5 | 282. |
| 14 | .470 | 202. | 10.8 | 272. |
| 15 | .590 | 253. | 11.4 | 256. |
| 16 | .570 | 245. | 11.5 | 258. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .610 | 262. | 11.9 | 248. |
| 19 | .580 | 249. | 11.8 | 250. |
| 20 | .580 | 249. | 12.0 | 249. |
| 21 | .560 | 241. | 12.0 | 253. |
| 22 | -1.000 | -430. | -1.0 | -1. |
| 23 | -1.000 | -430. | -1.0 | -1. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 51

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|

| | | | | |
|---|---|---|---|---|
| 1 | .380 | 163. | 11.1 | 208. |
| 2 | .380 | 163. | 11.2 | 213. |
| 3 | .350 | 150. | 11.3 | 207. |
| 4 | .450 | 193. | 12.0 | 208. |
| 5 | .710 | 305. | 15.6 | 196. |
| 6 | .610 | 262. | 14.8 | 200. |
| 7 | .360 | 155. | 11.1 | 204. |
| 8 | .380 | 163. | 11.7 | 201. |
| 9 | .400 | 172. | 11.9 | 194. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .490 | 210. | 10.5 | 195. |
| 12 | .430 | 185. | 10.2 | 192. |
| 13 | .420 | 180. | 10.0 | 193. |
| 14 | .420 | 180. | 9.9 | 194. |
| 15 | .430 | 185. | 10.2 | 195. |
| 16 | .520 | 223. | 14.3 | 117. |
| 17 | .480 | 206. | 13.8 | 127. |
| 18 | .450 | 193. | 13.7 | 132. |
| 19 | .450 | 193. | 12.0 | 182. |
| 20 | .450 | 193. | 11.0 | 208. |
| 21 | .460 | 198. | 10.2 | 221. |
| 22 | .540 | 232. | 7.7 | 273. |
| 23 | .500 | 215. | 8.1 | 269. |
| 24 | .470 | 202. | 7.6 | 46. |

DAY = 52

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | .480 | 206. | 8.5 | 275. |
| 3 | .430 | 185. | 7.7 | 285. |
| 4 | .460 | 198. | 8.5 | 289. |
| 5 | .470 | 202. | 9.0 | 289. |
| 6 | .540 | 232. | 9.2 | 259. |
| 7 | .460 | 198. | 8.0 | 257. |
| 8 | .450 | 193. | 7.5 | 257. |
| 9 | .480 | 206. | 7.5 | 255. |
| 10 | .460 | 198. | 7.4 | 256. |
| 11 | .460 | 198. | 7.5 | 256. |
| 12 | .470 | 202. | 7.9 | 253. |
| 13 | .450 | 193. | 7.9 | 252. |
| 14 | .420 | 180. | 7.6 | 255. |
| 15 | .360 | 155. | 5.3 | 255. |
| 16 | .390 | 168. | 5.6 | 256. |
| 17 | .380 | 163. | 5.6 | 256. |
| 18 | .390 | 168. | 5.8 | 256. |
| 19 | .380 | 163. | 5.8 | 267. |
| 20 | .410 | 176. | 6.7 | 285. |
| 21 | .470 | 202. | 9.3 | 289. |
| 22 | .430 | 185. | 11.1 | 279. |
| 23 | .420 | 180. | 11.1 | 283. |
| 24 | -1.000 | -430. | -1.0 | -1. |

DAY = 53

| | NOX | NOX | O2 | GROSS OUTPUT |
|---|---|---|---|---|

| HOUR | LB/10**6 BTU | NG/J | PERCENT | MW |
|---|---|---|---|---|
| 1 | .380 | 163. | 7.6 | 289. |
| 2 | .420 | 180. | 8.5 | 293. |
| 3 | .410 | 176. | 7.8 | 292. |
| 4 | .500 | 215. | 9.9 | 288. |
| 5 | .400 | 172. | 7.8 | 286. |
| 6 | .400 | 172. | 7.4 | 287. |
| 7 | .340 | 146. | 5.5 | 283. |
| 8 | .340 | 146. | 5.7 | 265. |
| 9 | .310 | 133. | 5.7 | 266. |
| 10 | .310 | 133. | 5.6 | 267. |
| 11 | .320 | 137. | 5.6 | 266. |
| 12 | .380 | 163. | 6.6 | 262. |
| 13 | .440 | 189. | 7.8 | 261. |
| 14 | .440 | 189. | 7.8 | 259. |
| 15 | .450 | 193. | 7.7 | 259. |
| 16 | .480 | 206. | 7.8 | 259. |
| 17 | .450 | 193. | 7.7 | 258. |
| 18 | .470 | 202. | 8.6 | 260. |
| 19 | .410 | 176. | 7.6 | 273. |
| 20 | .410 | 176. | 7.9 | 311. |
| 21 | .480 | 206. | 8.9 | 360. |
| 22 | .410 | 176. | 7.2 | 359. |
| 23 | .430 | 185. | 7.2 | 357. |
| 24 | .440 | 189. | 7.4 | 358. |

DAY = 58



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 7.2 | 361. |
| 2 | .430 | 185. | 7.4 | 361. |
| 3 | .450 | 193. | 7.5 | 361. |
| 4 | .430 | 185. | 7.4 | 361. |
| 5 | .430 | 185. | 7.3 | 361. |
| 6 | .430 | 185. | 7.1 | 361. |
| 7 | .410 | 176. | 7.1 | 361. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | .440 | 189. | 7.2 | 361. |
| 10 | .440 | 189. | 7.1 | 360. |
| 11 | .440 | 189. | 7.1 | 360. |
| 12 | .440 | 189. | 7.0 | 361. |
| 13 | .430 | 185. | 7.1 | 362. |
| 14 | .430 | 185. | 7.2 | 362. |
| 15 | .430 | 185. | 7.1 | 362. |
| 16 | .420 | 180. | 7.0 | 363. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .400 | 172. | 7.1 | 361. |
| 19 | .410 | 176. | 7.1 | 362. |
| 20 | .420 | 180. | 7.2 | 363. |
| 21 | .420 | 180. | 7.4 | 362. |
| 22 | .420 | 180. | 7.3 | 358. |
| 23 | .420 | 180. | 7.3 | 358. |
| 24 | .420 | 180. | 7.3 | 361. |

DAY = 59

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .410 | 176. | 7.3 | 362. |
| 2 | .420 | 180. | 7.2 | 364. |
| 3 | .410 | 176. | 7.2 | 364. |
| 4 | .400 | 172. | 7.2 | 363. |
| 5 | .390 | 168. | 7.2 | 362. |
| 6 | .380 | 163. | 7.0 | 363. |
| 7 | .370 | 159. | 7.1 | 363. |
| 8 | .350 | 150. | 7.2 | 363. |
| 9 | .370 | 159. | 7.1 | 362. |
| 10 | .410 | 176. | 7.0 | 363. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .420 | 180. | 7.1 | 360. |
| 14 | .410 | 176. | 7.0 | 361. |
| 15 | .320 | 137. | 7.3 | 317. |
| 16 | .350 | 150. | 7.1 | 333. |
| 17 | .400 | 172. | 6.9 | 367. |
| 18 | .410 | 176. | 7.0 | 364. |
| 19 | .400 | 172. | 7.0 | 363. |
| 20 | .420 | 180. | 7.2 | 362. |
| 21 | .410 | 176. | 7.4 | 362. |
| 22 | .410 | 176. | 7.3 | 362. |
| 23 | .390 | 168. | 7.0 | 363. |
| 24 | .360 | 155. | 7.2 | 52. |

DAY = 60



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | -1.000 | -430. | -1.0 | -1. |
| 2 | .310 | 133. | 7.3 | 313. |
| 3 | .330 | 142. | 7.9 | 288. |
| 4 | .330 | 142. | 8.0 | 280. |
| 5 | .330 | 142. | 7.7 | 305. |
| 6 | .310 | 133. | 7.5 | 312. |
| 7 | .320 | 137. | 7.6 | 312. |
| 8 | .310 | 133. | 7.4 | 331. |
| 9 | .310 | 133. | 7.4 | 333. |
| 10 | .310 | 133. | 7.4 | 334. |
| 11 | .320 | 137. | 7.4 | 340. |
| 12 | .340 | 146. | 7.5 | 339. |
| 13 | .350 | 150. | 7.6 | 340. |
| 14 | .410 | 176. | 7.0 | 364. |
| 15 | .400 | 172. | 7.0 | 363. |
| 16 | .400 | 172. | 6.9 | 363. |
| 17 | .400 | 172. | 6.9 | 364. |
| 18 | .400 | 172. | 6.9 | 364. |
| 19 | .390 | 168. | 6.7 | 363. |
| 20 | .390 | 168. | 6.8 | 362. |
| 21 | .380 | 163. | 6.8 | 363. |
| 22 | .390 | 168. | 6.8 | 362. |
| 23 | .390 | 168. | 6.9 | 361. |
| 24 | .410 | 176. | 7.2 | 361. |

DAY = 61

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 7.3 | 352. |
| 2 | .360 | 155. | 8.1 | 332. |
| 3 | .350 | 150. | 8.2 | 320. |
| 4 | .350 | 150. | 8.1 | 323. |
| 5 | .360 | 155. | 8.2 | 323. |
| 6 | .380 | 163. | 8.0 | 332. |
| 7 | .450 | 193. | 7.4 | 352. |
| 8 | .480 | 206. | 7.2 | 361. |
| 9 | .440 | 189. | 7.1 | 364. |
| 10 | .430 | 185. | 7.1 | 365. |
| 11 | .430 | 185. | 7.0 | 362. |
| 12 | .460 | 198. | 7.1 | 362. |
| 13 | .440 | 189. | 7.1 | 363. |
| 14 | .440 | 189. | 6.9 | 359. |
| 15 | .420 | 180. | 6.8 | 360. |
| 16 | .430 | 185. | 6.8 | 360. |
| 17 | .420 | 180. | 6.9 | 363. |
| 18 | .430 | 185. | 6.8 | 364. |
| 19 | .430 | 185. | 6.9 | 363. |
| 20 | .430 | 185. | 6.8 | 363. |
| 21 | .440 | 189. | 7.0 | 363. |
| 22 | .440 | 189. | 7.1 | 363. |
| 23 | .440 | 189. | 7.1 | 354. |
| 24 | .410 | 176. | 8.3 | 202. |

DAY = 62



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .390 | 168. | 8.1 | 303. |
| 2 | .400 | 172. | 8.2 | 302. |
| 3 | .380 | 163. | 8.0 | 300. |
| 4 | .420 | 180. | 8.4 | 269. |
| 5 | .420 | 180. | 8.5 | 248. |
| 6 | .410 | 176. | 8.2 | 271. |
| 7 | .460 | 198. | 7.5 | 349. |
| 8 | .490 | 210. | 7.5 | 363. |
| 9 | .410 | 176. | 3.8 | 360. |
| 10 | -1.000 | -430. | -1.0 | -1. |
| 11 | .560 | 241. | 7.5 | 357. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | -1.000 | -430. | -1.0 | -1. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .450 | 193. | 7.4 | 363. |
| 17 | .450 | 193. | 7.3 | 361. |
| 18 | .480 | 206. | 7.3 | 361. |
| 19 | .470 | 202. | 7.4 | 360. |
| 20 | .490 | 210. | 7.5 | 360. |
| 21 | .480 | 206. | 7.5 | 359. |
| 22 | .480 | 206. | 7.5 | 359. |
| 23 | .480 | 206. | 7.4 | 360. |
| 24 | .410 | 176. | 8.6 | 318. |

DAY = 63

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .460 | 198. | 8.6 | 280. |
| 2 | .440 | 189. | 8.1 | 272. |
| 3 | .440 | 189. | 8.2 | 273. |
| 4 | .440 | 189. | 8.0 | 272. |
| 5 | .420 | 180. | 7.6 | 289. |
| 6 | .410 | 176. | 7.5 | 290. |
| 7 | .410 | 176. | 7.3 | 325. |
| 8 | -1.000 | -430. | -1.0 | -1. |
| 9 | .400 | 172. | 5.9 | 363. |
| 10 | .410 | 176. | 6.8 | 365. |
| 11 | .420 | 180. | 6.9 | 367. |
| 12 | .420 | 180. | 6.9 | 365. |
| 13 | .410 | 176. | 6.8 | 361. |
| 14 | -1.000 | -430. | -1.0 | -1. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | -1.000 | -430. | -1.0 | -1. |
| 17 | .380 | 163. | 7.5 | 329. |
| 18 | .390 | 168. | 7.5 | 328. |
| 19 | .380 | 163. | 7.5 | 336. |
| 20 | .400 | 172. | 7.7 | 334. |
| 21 | .380 | 163. | 8.0 | 299. |
| 22 | .360 | 155. | 8.0 | 268. |
| 23 | .370 | 159. | 8.0 | 267. |
| 24 | .350 | 150. | 8.0 | 45. |

DAY = 64

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .350 | 150. | 7.7 | 266. |
| 2 | .350 | 150. | 7.8 | 256. |
| 3 | .360 | 155. | 7.8 | 257. |
| 4 | .360 | 155. | 7.9 | 255. |
| 5 | .360 | 155. | 8.0 | 254. |
| 6 | .350 | 150. | 7.9 | 256. |
| 7 | .360 | 155. | 7.8 | 269. |
| 8 | .350 | 150. | 7.9 | 315. |
| 9 | .350 | 150. | 7.8 | 312. |
| 10 | .290 | 125. | 7.6 | 313. |
| 11 | .380 | 163. | 7.7 | 337. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .420 | 180. | 7.5 | 366. |
| 14 | .420 | 180. | 9.1 | 364. |
| 15 | -1.000 | -430. | -1.0 | -1. |
| 16 | .440 | 189. | 10.8 | 363. |
| 17 | .430 | 185. | 10.8 | 362. |
| 18 | .440 | 189. | 10.6 | 360. |
| 19 | .430 | 185. | 10.9 | 357. |
| 20 | .440 | 189. | 11.0 | 312. |
| 21 | -1.000 | -430. | -1.0 | -1. |
| 22 | .440 | 189. | 11.1 | 362. |
| 23 | .370 | 159. | 11.6 | 363. |
| 24 | .400 | 172. | 11.1 | 364. |

DAY = 85

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .550 | 236. | 8.7 | 255. |
| 2 | .470 | 202. | 8.4 | 288. |
| 3 | .520 | 223. | 8.2 | 279. |
| 4 | .570 | 245. | 8.4 | 274. |
| 5 | .560 | 241. | 8.1 | 279. |
| 6 | .540 | 232. | 8.1 | 276. |
| 7 | .080 | 34. | 18.5 | 25. |
| 8 | .050 | 21. | 18.0 | 12. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .310 | 133. | 12.7 | 108. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | .500 | 215. | 8.2 | 300. |
| 13 | .460 | 198. | 7.8 | 327. |
| 14 | .450 | 193. | 7.7 | 336. |
| 15 | .440 | 189. | 7.7 | 336. |
| 16 | .430 | 185. | 7.6 | 335. |
| 17 | .350 | 150. | 10.0 | 241. |
| 18 | .330 | 142. | 9.8 | 238. |
| 19 | .380 | 163. | 8.3 | 295. |
| 20 | .420 | 180. | 7.6 | 342. |
| 21 | .410 | 176. | 7.4 | 346. |
| 22 | .430 | 185. | 7.4 | 354. |
| 23 | .440 | 189. | 7.5 | 351. |
| 24 | .430 | 185. | 7.4 | 350. |

DAY = 86



| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .430 | 185. | 7.6 | 345. |
| 2 | -1.000 | -430. | -1.0 | -1. |
| 3 | .400 | 172. | 7.3 | 348. |
| 4 | .400 | 172. | 7.4 | 351. |
| 5 | -1.000 | -430. | -1.0 | -1. |
| 6 | .410 | 176. | 7.5 | 350. |
| 7 | .410 | 176. | 7.5 | 346. |
| 8 | .410 | 176. | 7.5 | 345. |
| 9 | -1.000 | -430. | -1.0 | -1. |
| 10 | .410 | 176. | 8.1 | 330. |
| 11 | -1.000 | -430. | -1.0 | -1. |
| 12 | -1.000 | -430. | -1.0 | -1. |
| 13 | .410 | 176. | 8.0 | 335. |
| 14 | .410 | 176. | 8.0 | 338. |
| 15 | .410 | 176. | 8.0 | 337. |
| 16 | .400 | 172. | 7.9 | 336. |
| 17 | -1.000 | -430. | -1.0 | -1. |
| 18 | .400 | 172. | 7.8 | 337. |
| 19 | .410 | 176. | 8.0 | 332. |
| 20 | .400 | 172. | 7.8 | 330. |
| 21 | .410 | 176. | 7.9 | 327. |
| 22 | .410 | 176. | 8.0 | 317. |
| 23 | .410 | 176. | 7.9 | 317. |
| 24 | .400 | 172. | 8.1 | 319. |

DAY = 87

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .400 | 172. | 8.1 | 321. |
| 2 | .400 | 172. | 8.1 | 321. |
| 3 | .380 | 163. | 8.1 | 322. |
| 4 | .390 | 168. | 8.1 | 322. |
| 5 | .390 | 168. | 8.1 | 322. |
| 6 | .400 | 172. | 8.0 | 325. |
| 7 | .390 | 168. | 8.0 | 328. |
| 8 | .400 | 172. | 8.0 | 328. |
| 9 | .400 | 172. | 7.9 | 326. |
| 10 | .420 | 180. | 8.1 | 324. |
| 11 | .420 | 180. | 8.2 | 325. |
| 12 | .420 | 180. | 8.1 | 325. |
| 13 | .420 | 180. | 8.1 | 322. |
| 14 | .430 | 185. | 8.2 | 321. |
| 15 | .440 | 189. | 8.2 | 323. |
| 16 | .430 | 185. | 8.2 | 320. |
| 17 | .430 | 185. | 8.2 | 322. |
| 18 | .430 | 185. | 8.1 | 324. |
| 19 | .420 | 180. | 8.1 | 323. |
| 20 | .420 | 180. | 8.2 | 317. |
| 21 | .420 | 180. | 8.3 | 314. |
| 22 | .410 | 176. | 8.2 | 316. |
| 23 | .410 | 176. | 8.2 | 318. |
| 24 | .420 | 180. | 8.2 | 317. |

DAY = 29

| HOUR | NOX LB/10**6 BTU | NOX NG/J | O2 PERCENT | GROSS OUTPUT MW |
|---|---|---|---|---|
| 1 | .420 | 180. | 8.0 | 325. |
| 2 | .420 | 180. | 8.1 | 325. |
| 3 | .430 | 185. | 8.3 | 324. |
| 4 | .430 | 185. | 8.2 | 323. |
| 5 | .440 | 189. | 8.1 | 324. |
| 6 | .430 | 185. | 8.1 | 323. |
| 7 | .430 | 185. | 7.9 | 317. |
| 8 | .430 | 185. | 7.9 | 319. |
| 9 | .430 | 185. | 8.0 | 321. |
| 10 | .430 | 185. | 8.1 | 321. |
| 11 | .420 | 180. | 8.0 | 321. |
| 12 | .420 | 180. | 8.1 | 317. |
| 13 | .420 | 180. | 8.0 | 318. |
| 14 | .420 | 180. | 8.0 | 318. |
| 15 | .400 | 172. | 9.2 | 315. |
| 16 | .380 | 163. | 10.2 | 313. |
| 17 | .390 | 168. | 10.2 | 314. |
| 18 | .380 | 163. | 10.1 | 315. |
| 19 | .390 | 168. | 10.3 | 315. |
| 20 | .400 | 172. | 10.4 | 312. |
| 21 | .400 | 172. | 10.5 | 318. |
| 22 | .390 | 168. | 10.2 | 321. |
| 23 | .390 | 168. | 10.3 | 323. |
| 24 | .400 | 172. | 10.4 | 322. |